

LOT 1 - ERIE AIR PARK REPLAT D

LOCATED IN THE NORTHWEST QUARTER OF SECTION 31, TOWNSHIP 1 NORTH RANGE 68 WEST OF THE 6TH P.M. TOWN OF ERIE, COUNTY OF WELD, STATE OF COLORADO AREA = 10.340 ACRES









Lot 1 Erie Air Park **Replat D** 2800 Airport Drive Erie, CO 80516

Date Description 1 05/22/23 Initial Submittal 2 07/28/23 SIP Submittal

Project No:	23126A
Ву:	JAS/DPA
File:	23126A-1

Site Context Map

Sheet

C-101

May 18, 2023

Mr. Chris LaRue Town of Erie 645 Holbrook Street P.O. Box 750 Erie, CO 80516

Reference: Letter of Authorization – Site Plan Review Lot 1 – Erie Air Park Replat D 2800 Airport Drive – Erie, Colorado

Dear Chris:

The undersigned has hereby authorized Mr. Donald P, Ash to act as agent and/or make application to the Town of Erie for the above referenced property for the following applications:

- PUD Rezoning
- Minor Subdivision
- Site Plan Review

Sincerely,

David S. Nassar Real Investments, LLC

[NOTARY BLOCK FOLLOWS]

ACKNOWLEDGEMENT

STATE OF COLORADO)
COUNTY OF Weld)ss.
The foregoing instrument was ac	knowledged before me this 18 day of
, 2023 by Da	vid S. Nassar, as Monager
of Real Investments, LLC.	9
(SEAL)	NOTARY PUBLIC:
LAURIE HURD	sign: Jamie Burd
NOTARY PUBLIC STATE OF COLORADO NOTARY ID 20214033179	Printed Name: Laurie Hurd
MY COMMISSION EXPIRES-08/19/2025	Commission Number: 20214033179
	Commission Expiration: 8/19/25

COLORADO DEPARTMENT OF TRANSPORTATION STATE HIGHWAY ACCESS PERMIT APPLICATION

Issuing authority application acceptance date:

 Contact the issuing a Complete this form (s Submit an application or type If you have any question 	 Please print or type Contact the issuing authority to determine what plans and other documents are required to be submitted with your application. Complete this form (some questions may not apply to you) and attach all necessary documents and Submit it to the issuing authority. Submit an application for each access affected. If you have any questions contact the issuing authority. For additional information see CDOT's Access Management website at 												

18) Check with the issuing authority to determine which of the following documents are required to complete the review of your application.

- a) Property map indicating other access, bordering roads and streets.
- b) Highway and driveway plan profile.
- c) Drainage plan showing impact to the highway right-of-way.
- d) Map and letters detailing utility locations before and after
- development in and along the right-of-way.

- e) Subdivision, zoning, or development plan.
- f) Proposed access design.
- g) Parcel and ownership maps including easements.
- h) Traffic studies.
- i) Proof of ownership.

1- It is the applicant's responsibility to contact appropriate agencies and obtain all environmental clearances that apply to their activities. Such clearances may include Corps of Engineers 404 Permits or Colorado Discharge Permit System permits, or ecological, archeological, historical or cultural resource clearances. The CDOT Environmental Clearances Information Summary presents contact information for agencies administering certain clearances, information about prohibited discharges, and may be obtained from Regional CDOT Utility/Special Use Permit offices or accessed via the CDOT Planning/Construction-Environmental-Guidance webpage: https://www.codot.gov/programs/environmental/ resources/guidance-standards/environmental-clearances-info-summary-august-2017/view

2- All workers within the State Highway right of way shall comply with their employer's safety and health policies/ procedures, and all applicable U.S. Occupational Safety and Health Administration (OSHA) regulations - including, but not limited to the applicable sections of 29 CFR Part 1910 - Occupational Safety and Health Standards and 29 CFR Part 1926

- Safety and Health Regulations for Construction.

Personal protective equipment (e.g. head protection, footwear, high visibility apparel, safety glasses, hearing protection, respirators, gloves, etc.) shall be worn as appropriate for the work being performed, and as specified in regulation. At a minimum, all workers in the State Highway right of way, except when in their vehicles, shall wear the following personal protective equipment: High visibility apparel as specified in the Traffic Control provisions of the documentation accompanying the Notice to Proceed related to this permit (at a minimum, ANSI/ISEA 107-1999, class 2); head protection that complies with the ANSI Z89.1-1997 standard; and at all construction sites or whenever there is danger of injury to feet, workers shall comply with OSHA's PPE requirements for foot protection per 29 CFR 1910.136, 1926.95, and 1926.96. If required, such footwear shall meet the requirements of ANSI Z41-1999.

Where any of the above-referenced ANSI standards have been revised, the most recent version of the standard shall apply.

3- The Permittee is responsible for complying with the Revised Guidelines that have been adopted by the Access Board under the American Disabilities Act (ADA). These guidelines define traversable slope requirements and prescribe the use of a defined pattern of truncated domes as detectable warnings at street crossings. The new Standards Plans and can be found on the Design and Construction Project Support web page at:

https://www.codot.gov/business/civilrights/ada/resources-engineers

If an access permit is issued to you, it will state the terms and conditions for its use. Any changes in the use of the permitted access not consistent with the terms and conditions listed on the permit may be considered a violation of the permit.

The applicant declares under penalty of perjury in the second degree, and any other applicable state or federal laws, that all information provided on this form and submitted attachments are to the best of their knowledge true and complete.

I understand receipt of an access permit does not constitute permission to start access construction work.

Applicant or Agent for Permittee signature	Print name Date								
If the applicant is not the owner of the property, we require this application also to be signed by the property owner or their legally authorized representative (or other acceptable written evidence). This signature shall constitute agreement with this application by all owners-of-interest unless stated in writing. If a permit is issued, the property owner, in most cases, will be listed as the permittee.									
Property owner signature	Print name	Date							

INSTRUCTIONS FOR COMPLETING APPLICATION FOR ACCESS PERMIT (CDOT FORM NO. 137) December 2018

To construct, relocate, close, or modify access(es) to a State Highway or when there are changes in use of such access point(s), an application for access permit must be submitted to the Colorado Department of Transportation (CDOT) or the local jurisdiction serving as the issuing authority for State Highway Access Permits. Contact the CDOT Regional Access Unit in which the subject property is located to determine where the application must be submitted. The following link will help you determine which CDOT Region office to contact:

https://www.codot.gov/business/permits/accesspermits/regional-offices.html

All applications are processed and access permits are issued in accordance to the requirements and procedures found in the most current version of the State Highway Access Code (Access Code). Code and the application form are also available from CDOT's web site at:

https://www.codot.gov/business/permits/accesspermits

Please complete all information requested accurately. Access permits granted based on applications found to contain false information may be revoked. An incomplete application will not be accepted. If additional information, plans and documents are required, attach them to the application. Keep a copy of your submittal for your records. Please note that only the original signed copy of the application will be accepted. Do not send or enclose any permit fee at this time. A permit fee will be collected if an access permit is issued. The following is a brief description of the information to be provided on each enumerated space on the application form (CDOT Form 137, 2010).

1. **Property Owner (Permittee):** Please provide the full name, mailing address and telephone number and the E-mail address (if available) of the legal property owner (owner of the surface rights). Please provide a telephone number where the Permittee can be reached during business hours (8:00 a.m. to 5:00 p.m.). Having a contract on the property is not a sufficient legal right to that property for purposes of this application. If the access is to be on or across an access easement, then a copy of the easement MUST accompany this application. If federal land is involved, provide the name of the relevant federal agency AND attach copy of federal authorization for property use.

2. Agent for permittee: If the applicant (person completing this application) is different than the property owner (Permittee), provide entity name (if applicable), the full name of the person serving as the Agent, mailing address, telephone number, and the E-mail address (if available). Please provide a telephone number where the Agent can be reached during business hours (8:00 a.m. to 5:00 p.m.). Joint applications such as owner/lessee may be submitted. Corporations must be licensed to do business in Colorado: All corporations serving as, or providing, an Agent as the applicant must be licensed to do business in Colorado.

3. Address of Property to be Served: Provide if property to be served has an official street address. If the access is a public road, note the name (or future name) of the road.

4. Legal Description of Property: Fill in this item to the extent it applies. This information is available at your local County Courthouse, or on your ownership deed(s). A copy of the deed may be required as part of this application in some situations. To determine applicability, check with the CDOT's Regional Access Manager or issuing authority staff.

5. State Highway: Provide the State Highway number from which the access is requested.

6. Highway Side: Mark the appropriate box to indicate what side of the highway the requested access is located.

7. Access Mile Point: Without complete information, we may not be able to locate the proposed access. To obtain the distance in feet, drive the length between the mile point and the proposed access, rounding the distance on the odometer to the nearest tenth of a mile; multiply the distance by 5,280 feet to obtain the number of feet from the mile point. Then enter the direction (i.e. north, south, east, west) from the mile point to the proposed access. Finally, enter the mile point number. It is helpful in rural or undeveloped areas if some flagging is tied to the right-of-way fence at the desired location of the access. Also, if there is a cross street or road close to the proposed access, note the distance in feet (using the same procedures noted above) from that cross street or road.

8. Access Construction Date: Fill in the date on which construction of the access is planned to begin.

9. Access Request: Mark items that apply. More than one item may be checked.

10. Existing property use: Describe how the property is currently being used. For example, common uses are Single Family Residential, Commercial or Agricultural.

11. Existing Access: Does the property have *any other legal alternatives to reach a public road* other than the access requested in this application? Note the access permit number(s) for any existing state highway access point(s) along with their issue date(s). If there are no existing access point(s), mark the "no" box.

12. Adjacent Property: Please mark the appropriate box. If the "yes" box is marked, provide a brief description of the property (location of the property in relation to the property for which this access application is being made).

13. Abutting Streets: If there are any other existing or proposed public roads or easements abutting the property, they should be shown on a map or plan attached to this application.

14. Agricultural Acres: Provide number of acres to be served.

15. Access Use: List the land uses and square footage of the site as it will be when it is fully developed. The planned land uses as they will be when the site is fully developed are used to project the amount of traffic that the site will generate, peak hour traffic levels and the type of vehicles that can be expected as a result of the planned land uses. There may be exceptional circumstances that would allow phased installation of access requirements. This is at the discretion of the CDOT Regional Access Unit or issuing authority staff.

16. Estimated Traffic Count: Provide a reasonable estimate of the traffic volume expected to use the access. Note the type of vehicles that will use the access along with the volume (number of vehicles in and out at either the peak hour or average daily rates) for each type of vehicle. A vehicle leaving the property and then returning counts as two trips. If 40 customers are expected to visit the business daily, there would be 80 trips in addition to the trips made by all employees and other visitors (such as delivery and trash removal vehicles). If the PDF on-line version of this application is being used, the fields for each type of vehicle will automatically be added together to populate the last field on the page.

17. Documents and Plans: The CDOT Regional Access Manager or issuing authority staff will determine which of these items must be provided to make the application complete. Incomplete applications will not be accepted. If an incomplete application is received via U.S. mail or through means other than in the hand of the Access Manager or issuing authority staff, it will not be processed. *It is the responsibility of the applicant to verify with the CDOT Regional Access Manager or issuing authority staff whether the application is complete at the time of submission.*

Signature: Generally, if the applicant is not the property owner, then the property owner or a legally authorized representative must sign the application. With narrow exceptions, proof of the property owner's consent is required to be submitted with the application (proof may be a power of attorney or a similar consent instrument). The CDOT Regional Access Manager or issuing authority staff will determine if the exception provided in the Access Code (2.3 (3) (b)) is applicable.

If CDOT is the issuing authority for this application, direct your questions to the CDOT Regional Access Manager or the issuing authority staff serving the subject property.

https://www.codot.gov/business/permits/accesspermits/regional-offices.html

If the application is accepted, it will be reviewed by the CDOT Regional Access Manager or the issuing authority staff. If an Access Permit is issued, be sure to read all of the attached Terms and Conditions before signing and returning the Access Permit. The Terms and Conditions may require that additional information be provided prior to issuance of the Notice to Proceed.

The CDOT Regional Access Manager (or issuing authority staff) MUST be contacted prior to commencing work on any Access Permit project. A Notice to Proceed that authorizes the Permittee to begin access related construction MUST be issued prior to working on the access in the State Highway right-of-way. The Notice to Proceed may also have Terms and Conditions that must be fulfilled before work may begin on the permitted access.

July 31, 2023



Mr. Chris LaRue Town of Erie 645 Holbrook Street P.O. Box 750 Erie, CO 80516

Reference: Traffic Conformance Letter Site Plan Review – SP-001598-2023 Lot 1 – Erie Air Park Replat D 2800 Airport Drive – Erie, Colorado SiteWorks Project No. 23126

Dear Chris:

The following conformance letter has been prepared in response to the Town of Erie completeness review comments dated June 20, 2023, for the above referenced project.

The original Traffic Impact Analysis (TIS) was prepared by LSC Transportation Consultants, Inc. dated October 9, 2019. The report was included as part of the Minor Subdivision submittal for the site, which was approved by the Town in 2022.

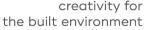
We have reviewed the updated plans with LSC and have confirmed that there are no changes required to the original TIS. All of the traffic count reports, trip generation and level of service analysis have remained unchanged since the original report.

Should you have any questions or comments concerning this letter, kindly give us a call.

Sincerely,

Donald P. Ash, P.E. Principal – SiteWorks





LSC TRANSPORTATION CONSULTANTS, INC.



1889 York Street Denver, CO 80206 (303) 333-1105 FAX (303) 333-1107 E-mail: lsc@lscdenver.com

May 20, 2024

Mr. Don Ash Site Work Studio dash@siteworkstudio.com

> Re: Erie Airpark Tract E-2 Traffic Impact Analysis Erie, CO LSC #230890

Dear Mr. Ash:

In response to your request, LSC Transportation Consultants, Inc. has prepared this updated traffic impact analysis for the proposed Erie Airpark Tract E-2 development to address Town comments. As shown on Figure 1, the site is located north of State Highway 7 on Airport Drive in Erie, Colorado.

REPORT CONTENTS

The report contains the following: the existing roadway and traffic conditions in the vicinity of the site including the lane geometries, traffic controls, posted speed limits, etc.; the existing weekday peak-hour traffic volumes; the existing daily traffic volumes in the area; the typical weekday site-generated traffic volume projections for the site; the assignment of the projected traffic volumes to the area roadways; the projected short-term and long-term background and resulting total traffic volumes on the area roadways; the site's projected traffic impacts; and any recommended roadway improvements to mitigate the site's traffic impacts.

LAND USE AND ACCESS

The site is proposed to include about 137,500 square feet of light industrial use and about 34,375 square feet of office space. Access is proposed from a full movement access to Airport Drive as shown in the conceptual site plan in Figure 2.

ROADWAY AND TRAFFIC CONDITIONS

Area Roadways

The major roadways in the site's vicinity are shown on Figure 1 and are described below.

• **E. Baseline Road (SH 7)** is an east-west, two-lane state highway south of the site and is classified as a Non-Rural Principal Highway (NR-A) by CDOT. The intersection with Airport Drive is stop-sign controlled. The posted speed limit in the vicinity of the site is 55 mph.

• **Airport Drive** is a north-south, two-lane roadway providing access to E. Baseline Road (SH 7). The intersection with E. Baseline Road (SH 7) is stop-sign controlled.

Existing Traffic Conditions

Figure 3 shows the existing lane geometries, traffic controls, posted speed limits, and traffic volumes in the site's vicinity on a typical weekday. The weekday peak-hour traffic volumes and daily traffic counts are from the attached traffic counts conducted by Counter Measures in November, 2023.

2026 and 2044 Background Traffic

Figure 4 shows the estimated 2026 background traffic. The volumes to/from Airport Drive are assumed to grow at an annual rate of two percent. The through volumes on SH 7 were factored between the volumes in Figure 3 and 5.

Figure 5 shows the estimated 2044 background traffic. The volumes to/from Airport Drive are assumed to grow from the development of future Tract E-3. The through volumes on SH 7 are consistent with the 2044 total traffic from the *Parkdale North TIA* by LSC. Figure 9a from that TIA is attached for reference.

Existing, 2026, and 2044 Background Levels of Service

Level of service (LOS) is a quantitative measure of the level of congestion or delay at an intersection. Level of service is indicated on a scale from "A" to "F." LOS A is indicative of little congestion or delay and LOS F is indicative of a high level of congestion or delay. Attached are specific level of service definitions for signalized and unsignalized intersections.

The intersections in Figures 3, 4, and 5 were analyzed as appropriate to determine the existing, 2026, and 2044 background levels of service using Synchro. Table 1 shows the level of service analysis results. The level of service reports are attached.

• **E. Baseline Road (SH 7)/Airport Drive:** All movements at this unsignalized intersection currently operate at LOS "D" or better during both morning and afternoon peak-hours with the exception of the southbound approach which operates at LOS "F" during the afternoon peak-hour. In 2026, the southbound approach is expected to operate at LOS "E" during the morning peak-hour and LOS "F" during the afternoon peak-hour with stop-sign control. The intersection is expected to be signalized by 2044 and is expected to operate at LOS "B" or better during both peak-hours.

TRIP GENERATION

Table 2 shows the estimated average weekday, morning peak-hour, and afternoon peak-hour trip generation for the proposed site based on the rates from *Trip Generation*, 11th Edition, 2021 by the Institute of Transportation Engineers (ITE) for the proposed land use.

The proposed land use is projected to generate about 1,043 one-way vehicle-trips on the average weekday, with about half entering and half exiting during a 24-hour period. During the

morning peak-hour, which generally occurs for one hour between 6:30 and 8:30 a.m., about 136 vehicles would enter and about 18 vehicles would exit the site. During the afternoon peakhour, which generally occurs for one hour between 4:00 and 6:00 p.m., about 21 vehicles would enter and about 118 vehicles would exit.

TRIP DISTRIBUTION

Figure 6 shows the estimated directional distribution of the site-generated traffic volumes on the area roadways. The estimates were based on the location of the site with respect to the regional population, employment, and activity centers; the site's proposed land use; and the existing traffic counts.

TRIP ASSIGNMENT

Figure 7 shows the estimated site-generated traffic volumes based on the directional distribution percentages (from Figure 6) and the trip generation estimate (from Table 2).

2026 AND 2044 TOTAL TRAFFIC

Figure 8 shows the 2026 total traffic which is the sum of the 2026 background traffic volumes (from Figure 4) and the site-generated traffic volumes (from Figure 7). Figure 8 also shows the recommended 2026 lane geometry and traffic control.

Figure 9 shows the 2044 total traffic which is the sum of 2044 background traffic volumes (from Figure 5) and the site-generated traffic volumes (from Figure 7). Figure 9 also shows the recommended 2044 lane geometry and traffic control.

PROJECTED LEVELS OF SERVICE

The intersections in Figures 8 and 9 were analyzed to determine the 2026 and 2044 total levels of service. Table 1 shows the level of service analysis results. The level of service reports are attached.

• **E. Baseline Road (SH 7)/Airport Drive:** All movements at this unsignalized intersection are expected to operate at LOS "C" or better during both morning and afternoon peakhours through 2044 with the exception of the southbound left-turn movement which is expected to operate at LOS "F" during both peak-hours with stop-sign control. As a signalized intersection it is expected to operate at LOS "C" or better during both peakhours through 2044.

TRAFFIC SIGNAL WARRANT

The existing posted speed limit on E. Baseline Road (SH 7) is 55 mph so the reduced 70% factor is appropriate for use in this situation. A peak-hour warrant would require one hour of side road approach trips greater than 75 vehicles per hour (vph). A four-hour warrant would require four hours of side road approach trips greater than 60 vph. The afternoon peak-hour volume for only the southbound left-turn movement is expected to be about 84 vph in 2026 with full Tract E-2 buildout and 139 vph by 2044 with full buildout of Tract E-2 and E-3. The peak-hour warrant will be met in 2026. The 2026 and 2044 total traffic volumes are plotted on a four-

hour traffic signal warrant chart in Figure 10 which suggests the four-hour warrant could also be met over time.

CONCLUSIONS AND RECOMMENDATIONS

Trip Generation

1. The proposed land use is projected to generate about 1,043 one-way vehicle-trips on the average weekday, with about half entering and half exiting during a 24-hour period. During the morning peak-hour, about 136 vehicles would enter and about 18 vehicles would exit the site. During the afternoon peak-hour, about 21 vehicles would enter and about 118 vehicles would exit.

Projected Levels of Service

2. All movements at the E. Baseline Road (SH 7)/Airport Drive intersection are expected to operate at acceptable levels of service during both morning and afternoon peak-hours through 2044 with the exception of the southbound left-turn movement which is expected to operate at LOS "F" during both peak-hours with stop-sign control. As a signalized intersection it is expected to operate at LOS "C" or better during both peak-hours through 2044. This intersection is expected to meet a traffic signal warrant by 2026 with full build-out of Tract E-2.

Conclusions

3. The impact of the Erie Airpark Tract E-2 Park development can be accommodated by the existing roadway network with the following recommendations.

Recommendations

- 4. E. Baseline Road (SH 7) will likely need to be widened to four lanes by others prior to 2044.
- 5. A southbound right-turn lane is recommended approaching E. Baseline Road (SH 7) to prevent right-turning vehicles from being blocked by left-turning queued vehicles. It will also result in more efficient utilization of the acceleration lane on E. Baseline Road (SH 7).
- 6. The westbound right-turn lane and southbound to westbound right-turn acceleration lane are deficient in length and are currently striped on the existing shoulder. These two lanes should be lengthened and/or widened as appropriate. This will likely be coordinated through the CDOT access permit process.
- 7. Traffic signal control will likely be warranted by Tract E-2 buildout by 2026 this will also likely be coordinated through the CDOT access permit process.

* * * * *

May 18, 2023



the built environment

Mr. Chris LaRue Town of Erie 645 Holbrook Street P.O. Box 750 Erie, CO 80516

Reference: Mineral Estate Notification – Site Plan Review Lot 1 – Erie Air Park Replat D 2800 Airport Drive – Erie, Colorado SiteWorks Project No. 23126

Dear Chris:

This letter has been prepared in accordance with your request to provide mineral estate notification for the above referenced project.

The sole mineral estate holder, Rocky Mountain Fuel Company, is no longer in operation. We have provided their contact information with this submittal, and they will be included in the Site Plan Review referral process. See the attached estate information and correspondence.

As a reminder, RM Fuel was notified in 2020 as part of the Minor Subdivision referral submittal. They responded that they are no longer in operation. Crestone Peak Resources, Inc. was also one of the referral agencies. There are no records showing that the mineral estate has been transferred or deeded to any other entity.

Prior discussions with RM Fuel have determined that the company still has ownership of the subsurface rights. There are no other surface right agreements or operating agreements in place.

Should you have any questions or comments concerning this letter, kindly give us a call.

Sincerely,

Donald P. Ash, P.E. Principal – SiteWorks





Subsurface Mineral Rights - Last Known Contact Information:

The Rocky Mountain Fuel Company 8020 S County Road Rd 5 #200 Fort Collins, CO 80528 (970) 207-1157

Warranty deed recorded at Weld County Assessors on August 27, 1946 at Book 1186 Page 313. See attached deed.

The surface rights to the property were sold to George E. Gouger by The Rocky Mountain Fuel Company on August 27, 1946 per document recorded at Book 1186 Page 313. A copy of this deed has been attached to the submittal. The deed grants surface rights to the grantee, George E. Gouger. But the grantor, RM Fuel, reserved all surface and subsurface mineral rights to the property. There are no other surface right agreements or operating agreements in place. RM Fuel went bankrupt in 1944, but the assets that were not liquidated were maintained by other RM Fuel entities. Notice will be sent to the former RM Fuel office in Ft. Collins, but it appears that the office is permanently closed.

From:	Warren Turner
То:	Don Ash
Subject:	Re: RM Fuel and Erie Air Park
Date:	Friday, May 22, 2020 2:03:38 PM

Awesome. With oil at record lows and the current political climate, our guess was that those minerals would never develop.

On May 22, 2020, at 2:00 PM, Don Ash <<u>ash@scottcox.com</u>> wrote:

Ok. Great. Thanks for the info.

We are subdividing one of the tracts.

From: Warren Turner <<u>tpccolorado@gmail.com</u>>
Sent: Friday, May 22, 2020 1:58:20 PM
To: Don Ash <<u>ash@scottcox.com</u>>
Subject: Re: RM Fuel and Erie Air Park

Don,

I just got off the phone with our broker. They believe Rocky Mountain Fuel still owns them and the contracts did not change the ownership of these minerals. Thanks,

Warren

On May 21, 2020, at 10:46 AM, Don Ash <<u>ash@scottcox.com</u>> wrote:

Hey Warren, this sounds good. Would there be a way for you to send me the contact person for this contract? I probably need to give them notice as well. It won't affect ownership or anything contractually between the two of you.

Thanks,

D

Donald P. Ash, P.E.

Chief Civil Engineer <image001.jpg> 1530 55th Street • Boulder, CO 80303 W 303.444.3051 • F 303.444.3387 • C 303.918.7859

<image002.png> <image003.png> <image004.png> <image005.png>

www.scottcox.com

From: Warren Turner <tpccolorado@gmail.com>
Sent: Thursday, May 21, 2020 10:14 AM
To: Don Ash <<u>ash@scottcox.com</u>>
Subject: Re: RM Fuel and Erie Air Park

Don,

Thanks for the response. There's some ambiguity as to ownership of those minerals do to an open ended contract. Thanks for reaching out. We have no comments or concerns. Best regards,

Warren Turner

On May 21, 2020, at 12:11 AM, Don Ash <<u>ash@scottcox.com</u>> wrote:

I sent you a flash drive a while back with some documents pertaining to a subdivision at the Erie Air Park. RM Fuel was listed as the mineral estate holder. Your email response was forwarded to me by Staff.

Have these assets been transferred to a different company? I can't seem to find any public records pertaining to any transfers. We are required to give the estate holders notice, but the proposed development does not affect your rights at all. So I'd like to figure out if there are any other notices required.

Let me know if there is a different owner, or we can talk about the plans. 303.918.7859.

Thanks,

D

Donald P. Ash, P.E.

Chief Civil Engineer <image001.jpg>

1530 55th Street • Boulder, CO 80303 W 303.444.3051 • F 303.444.3387 • C 303.918.7859

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www.scottcox.com

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Signed, se	aled and delivered this	lst ' day d	of August	, A. D. 1	946
Attest :			THE ROCKY MOUNTAI	I FUEL COMPANY	
-60.0	0.00	- 1	. IN. M.	Quand	60
City and	TATE OF COLORADO, County of Denver instrument was acknowled ii. M. Jones	retary. Bss. dged before me this	lst day of	√ico-Presiden August	5
, Dy	Kildred Lea		88 	Vice-Presider Secrets	
		rial commission ex Witness my han	d and official seal.	1 0.	ation.
	ETHEL G. WELLS, City and County of L	Notary Public,	Öth	Notary Pub	lis.

AMENDED REQUEST FOR NOTIFICATION OF SURFACE DEVELOPMENT

(C.R.S. § 24-65.5-101 et seq.)

STATE OF COLORADO)COUNTY OF WELD)

WHEREAS, by Request for Notification of Surface Development dated June 18, 2019, recorded June 19, 2019 at Reception No. 4498658 in the records of Weld County, Colorado,

Crestone Peak Resources Holdings LLC (CPR) is the Mineral Estate Owner (as defined in C.R.S. Section 24-65.5-102(5)) underlying the following described land located in Weld County, Colorado (the "Subject Lands"), to-wit:

Township 1 North, Range 68 West, 6th P.M. Section 30: ALL

WHEREAS, there were certain errors or omissions in the original Request and the undersigned wishes to amend the Request to correct the errors and omissions;

NOW, THEREFORE, the undersigned does hereby amend the Request for Notification of Surface Development by replacing the original document.

Pursuant to C.R.S. Section 24-65.5-103(3), CPR hereby requests written notification of any and all Applications for Development (as such term is defined in C.R.S. Section 24-65.5-102(2)) and all other proposed surface development activities on the Subject Lands in accordance with the terms of Article 24-65.5, C.R.S. Such notices should be sent to the following address:

Crestone Peak Resources Holdings LLC 1801 California Street, Suite 2500 Denver, CO 80202 Attn: DJ Surface Land Department

Executed this 15th day of July 2019.

Crestone Peak Resources Holdings LLC

By:

Name: Shea Kauffman Title: Director of Land & Business Development

>))ss.

STATE OF COLORADO

COUNTY OF DENVER

The foregoing instrument was acknowledged before me this 15th day of July 2019, by <u>Shea</u> <u>Kauffman</u>, as <u>Director of Land & Business Development</u> of <u>Crestone Peak Resources Holdings</u> <u>LLC</u>, a Delaware limited liability company.

Witness my hand and official seal.

My Commission Expires: 4118[7]

LAURA L CUSTER Notary Public State of Colorado Notary ID # 20124081516 My Commission Expires 04-18-2021

Notary Public

AMENDED REQUEST FOR NOTIFICATION OF SURFACE DEVELOPMENT

(C.R.S. § 24-65.5-101 et seq.)

STATE OF COLORADO COUNTY OF WELD

WHEREAS, by Request for Notification of Surface Development dated June 18, 2019, recorded June 19, 2019 at Reception No. 4498659 in the records of Weld County, Colorado,

)

)

Crestone Peak Resources Holdings LLC (CPR) is the Mineral Estate Owner (as defined in C.R.S. Section 24-65.5-102(5)) underlying the following described land located in Weld County, Colorado (the "Subject Lands"), to-wit:

Township 1 North, Range 68 West, 6th P.M. Section 31: ALL

WHEREAS, there were certain errors or omissions in the original Request and the undersigned wishes to amend the Request to correct the errors and omissions;

NOW, THEREFORE, the undersigned does hereby amend the Request for Notification of Surface Development by replacing the original document.

Pursuant to C.R.S. Section 24-65.5-103(3), CPR hereby requests written notification of any and all Applications for Development (as such term is defined in C.R.S. Section 24-65.5-102(2)) and all other proposed surface development activities on the Subject Lands in accordance with the terms of Article 24-65.5, C.R.S. Such notices should be sent to the following address:

Crestone Peak Resources Holdings LLC 1801 California Street, Suite 2500 Denver, CO 80202 Attn: DJ Surface Land Department

Executed this 15th day of July 2019.

Crestone Peak Resources Holdings LLC

By:

Name: Shea Kauffman Title: Director of Land & Business Development

STATE OF COLORADO

COUNTY OF DENVER

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The foregoing instrument was acknowledged before me this 15th day of July 2019, by <u>Shea</u> <u>Kauffman</u>, as <u>Director of Land & Business Development</u> of <u>Crestone Peak Resources Holdings</u> <u>LLC</u>, a Delaware limited liability company.

Witness my hand	and official	seal.
My Commission I	Expires: <u>4</u>	15/81

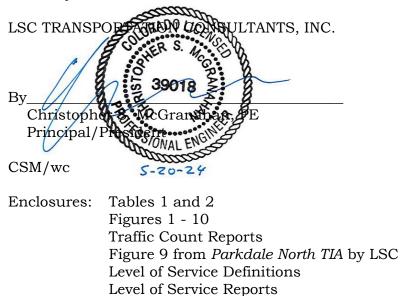
88	
RI	LAURA L CUSTER
	Notary Public
	State of Colorado
	Notary ID # 20124081516
	My Commission Expires 04-18-2021
	and the second se

Paro

Notary Public

We trust our findings will assist you in gaining approval of the proposed Erie Airpark Tract E-2 development. Please contact me if you have any questions or need further assistance.

Sincerely,

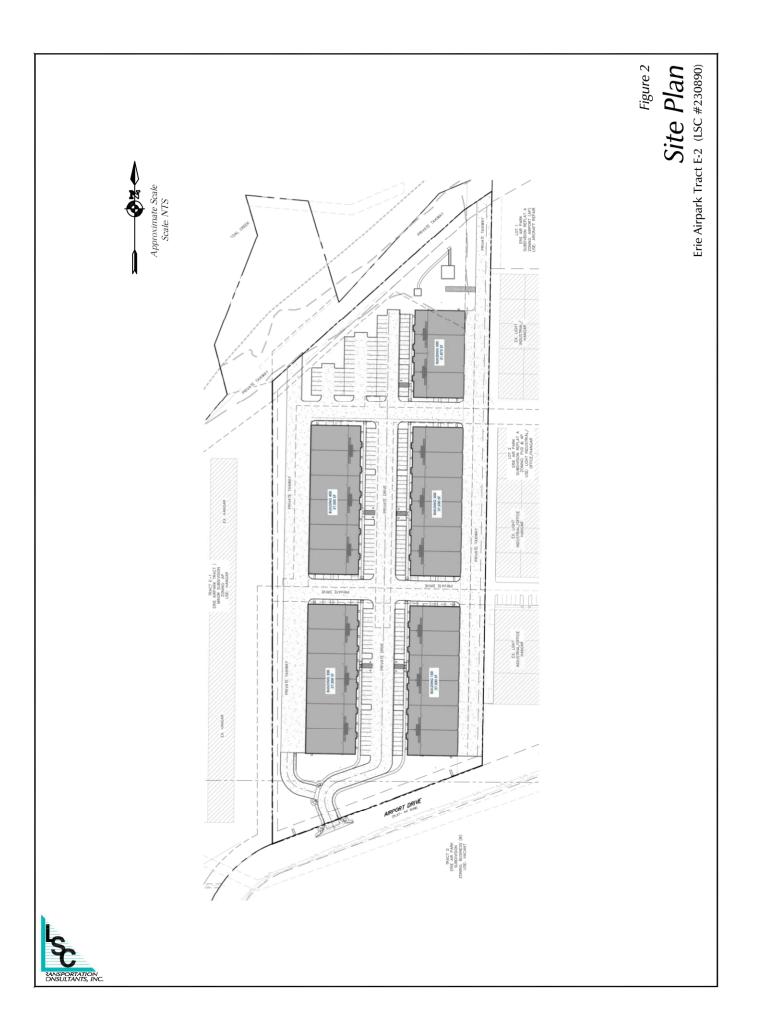


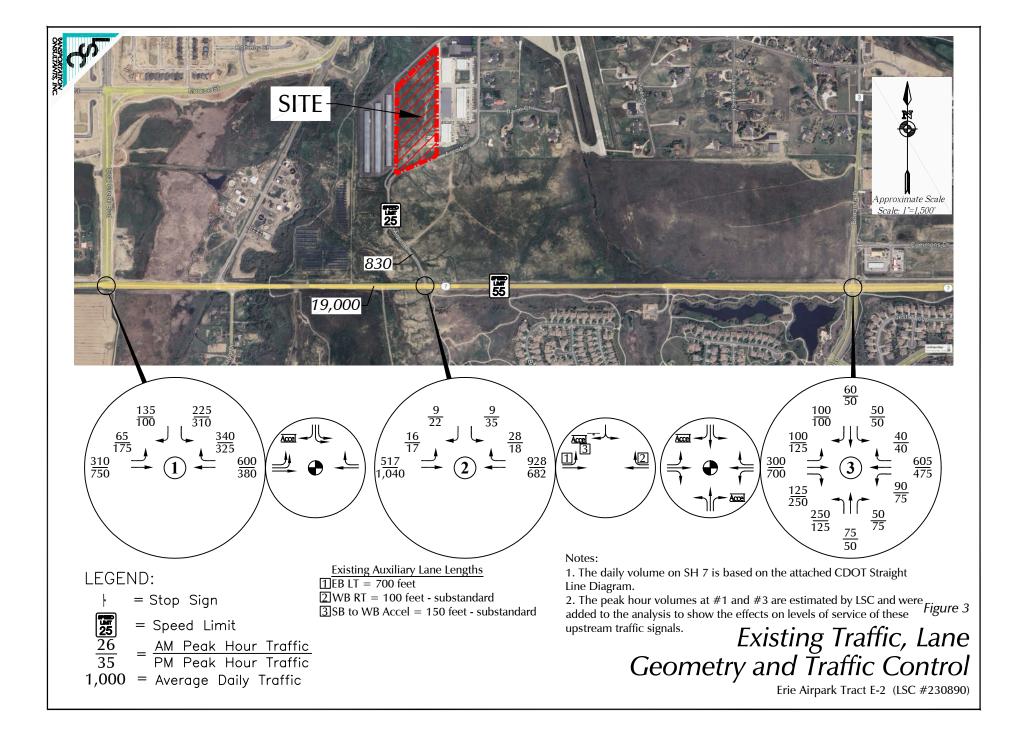
W:\LSC\Projects\2023\230890-ErieAirpark-TractE-2\Report\May-2024\ErieAirparkTract_E-2-052024.wpd

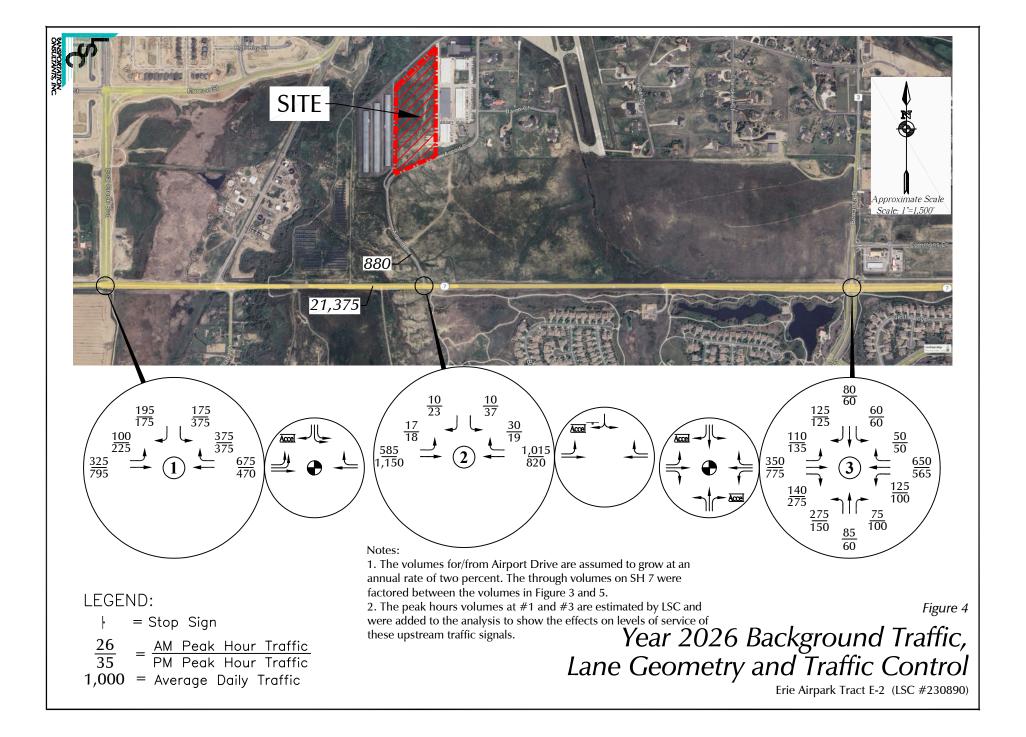
Table 1 Intersection Levels of Service Analysis Erie Airpark Tract E-2 Erie, CO LSC #230890; May, 2024											
Existing 2026 Background 2026 Total Traffic 2044 Background 2044 Total Traffi											
		Level of	Level of	Level of	Level of	Level of	Level of	Level of	Level of	Level of	Level of
	Traffic	Service	Service	Service	Service	Service	Service	Service	Service	Service	Service
Intersection Location	Control	AM	PM	AM	PM	AM	PM	AM	PM	AM	PM
<u>State Highway 7/Airport Drive</u> EB Left SB Approach SB Left SB Right Critical Movement Delay	TWSC	B D 30.1	A F 77.1	B E 37.9	A F 168.4	B F C 95.9	B F C >240	 	 	 	
Si	ignalized										
EB Left						А	Α	Α	D	С	D
EB Through						А	A	A	А	А	A
WB Through						А	A	A	В	А	С
WB Right						A	A	A	А	A	А
SB Left						E	E	E	E	E	D
SB Right						E	E	E	E	E	D
Entire Intersection Delay (sec /veh) Entire Intersection LOS						7.4 A	12.8 B	6.1 A	15.0 B	7.7 A	22.8 C

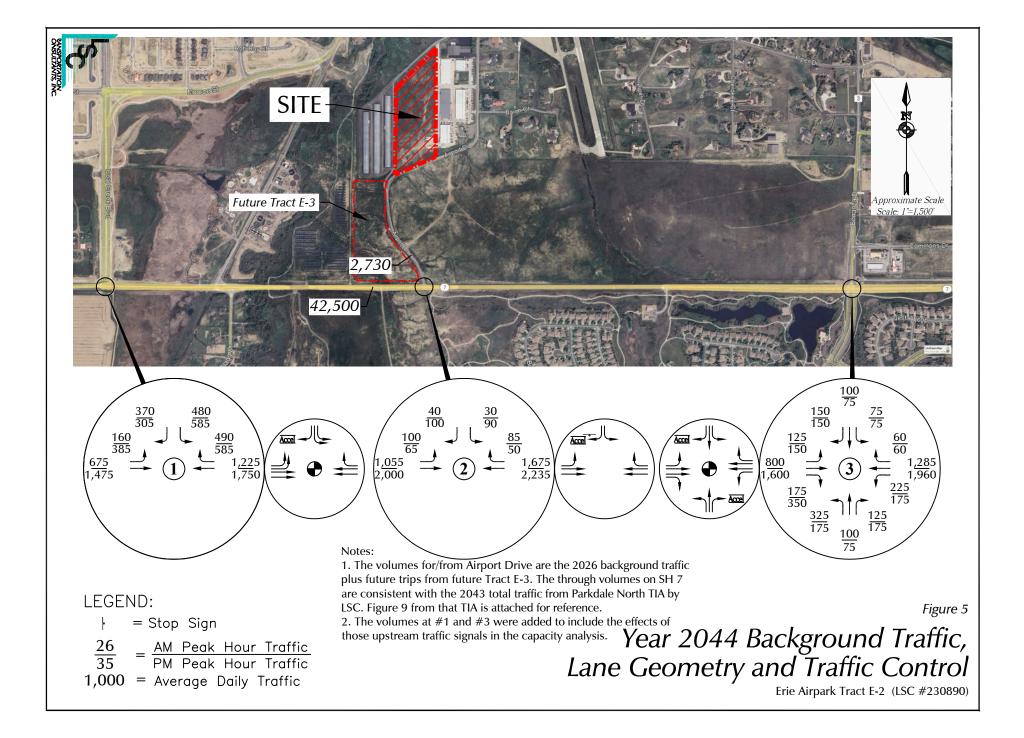
			E	oark Tra rie, CO 890; Ma		4						
			Trip Gen	eration R	ates ⁽¹⁾			Total Trip	s Gener	rated		
		Average	AM Pea	ak-Hour	PM Pe	ak-Hour	Average	AM Peak	-Hour	PM Peak	-Hour	
Trip Generating Category	Quantity	Weekday	In	Out	In	Out	Weekday	In	Out	In	Ou	
CURRENTLY PROPOSED Light Industrial ⁽²⁾ Office Space ⁽⁴⁾	LAND USE 137.500 KSF ⁽³⁾ 34.375 KSF ⁽³⁾	4.87 10.84	0.651 1.338	0.089 0.182	0.091 0.245	0.559 1.195	670 373	90 46	12 6	13 8	77 42	
						Total =	1,043	136	18	21	11	
Notes: (1) Source: <i>Trip Generatio</i>	on, Institute of Transpo	antation Enni		14h 🗖 -114	0004							

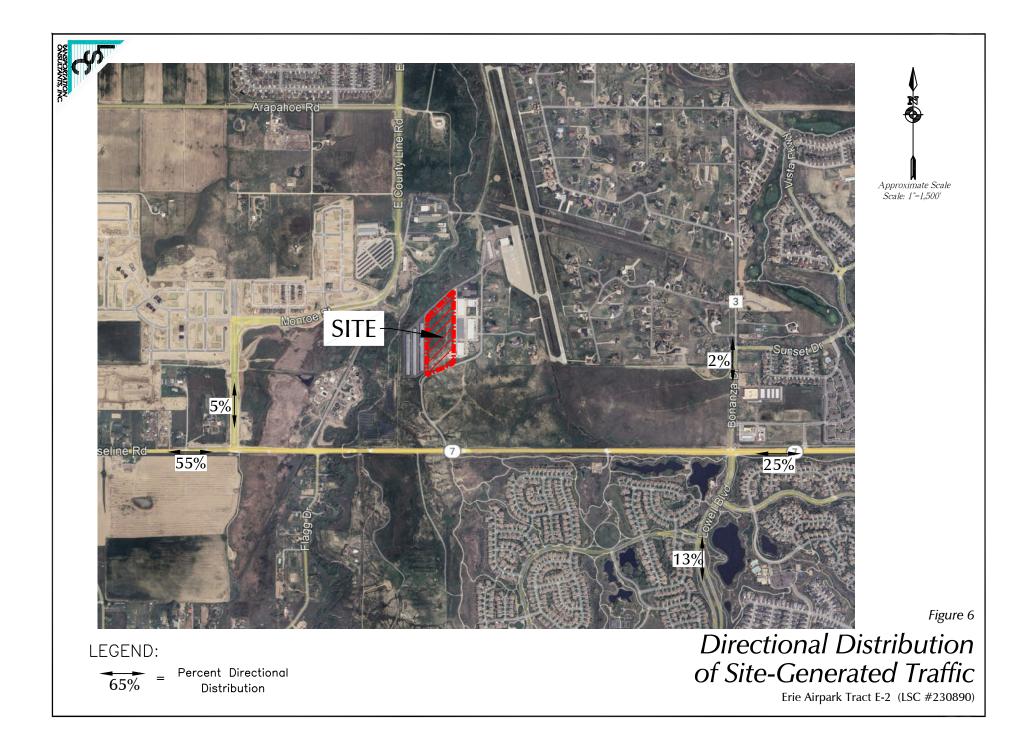


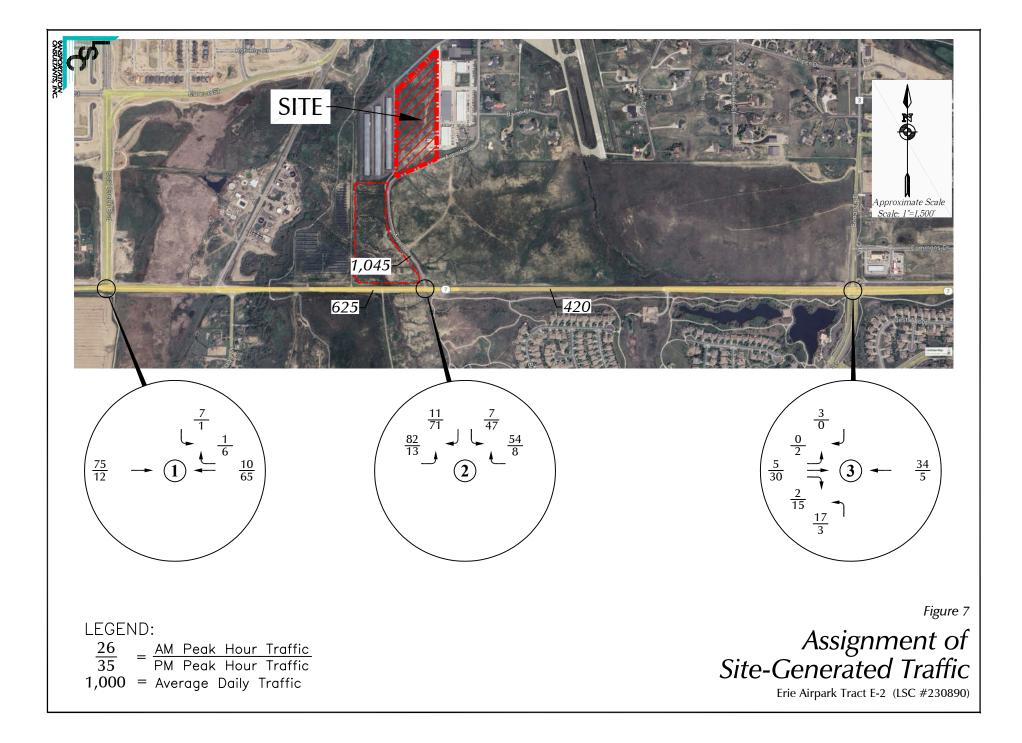


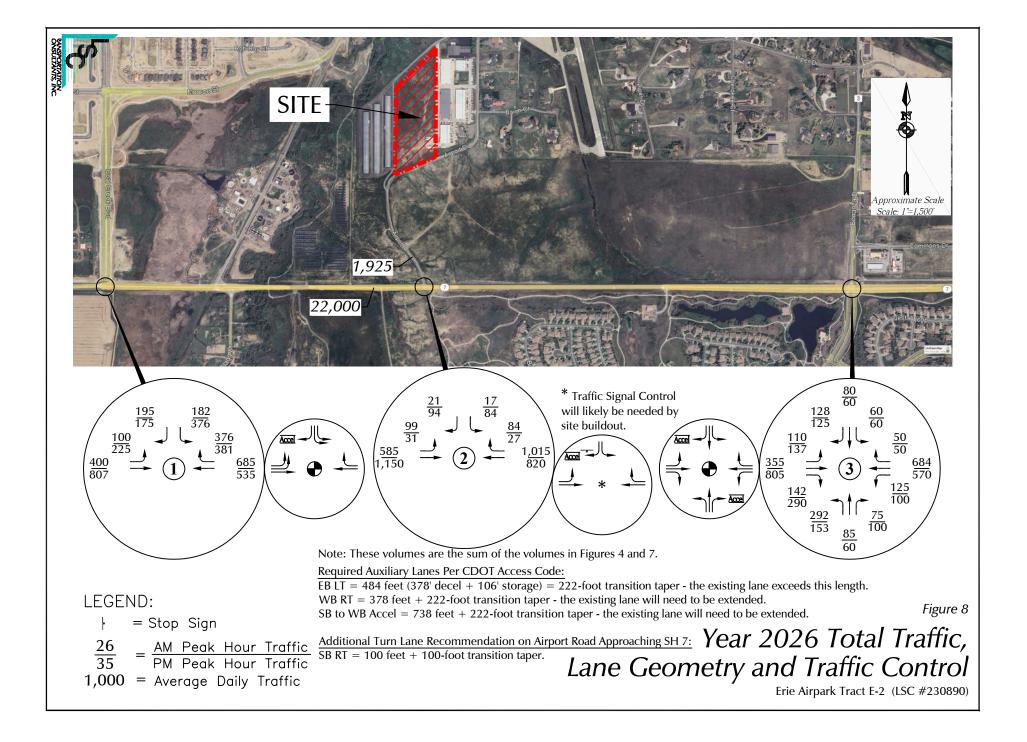


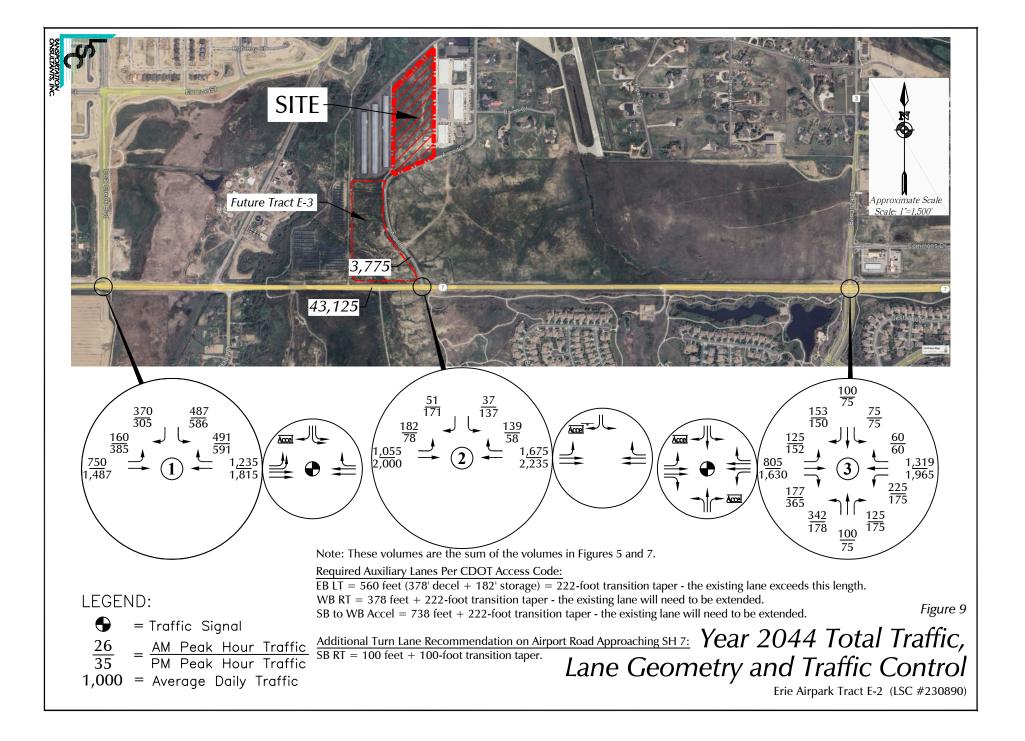


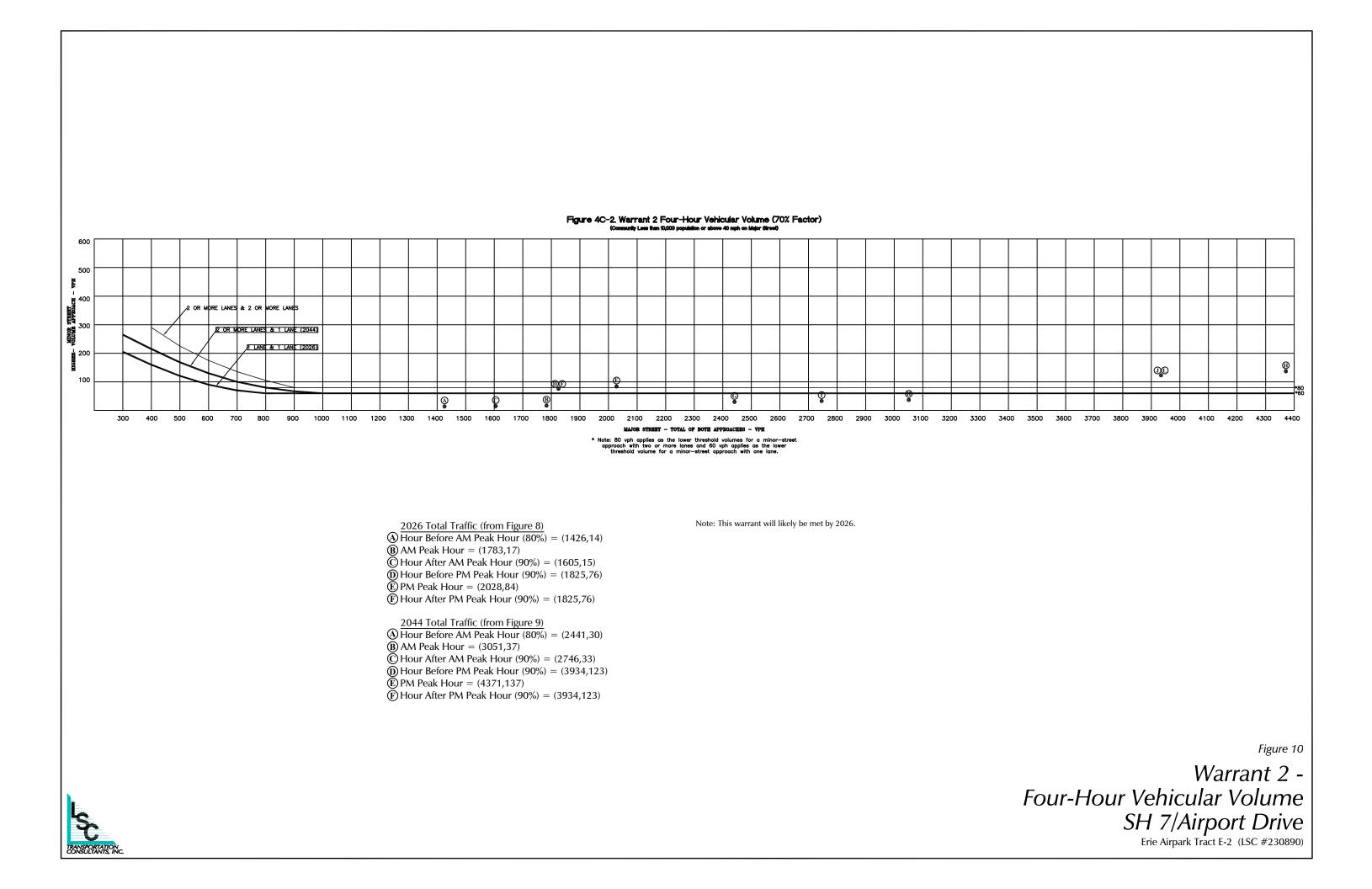


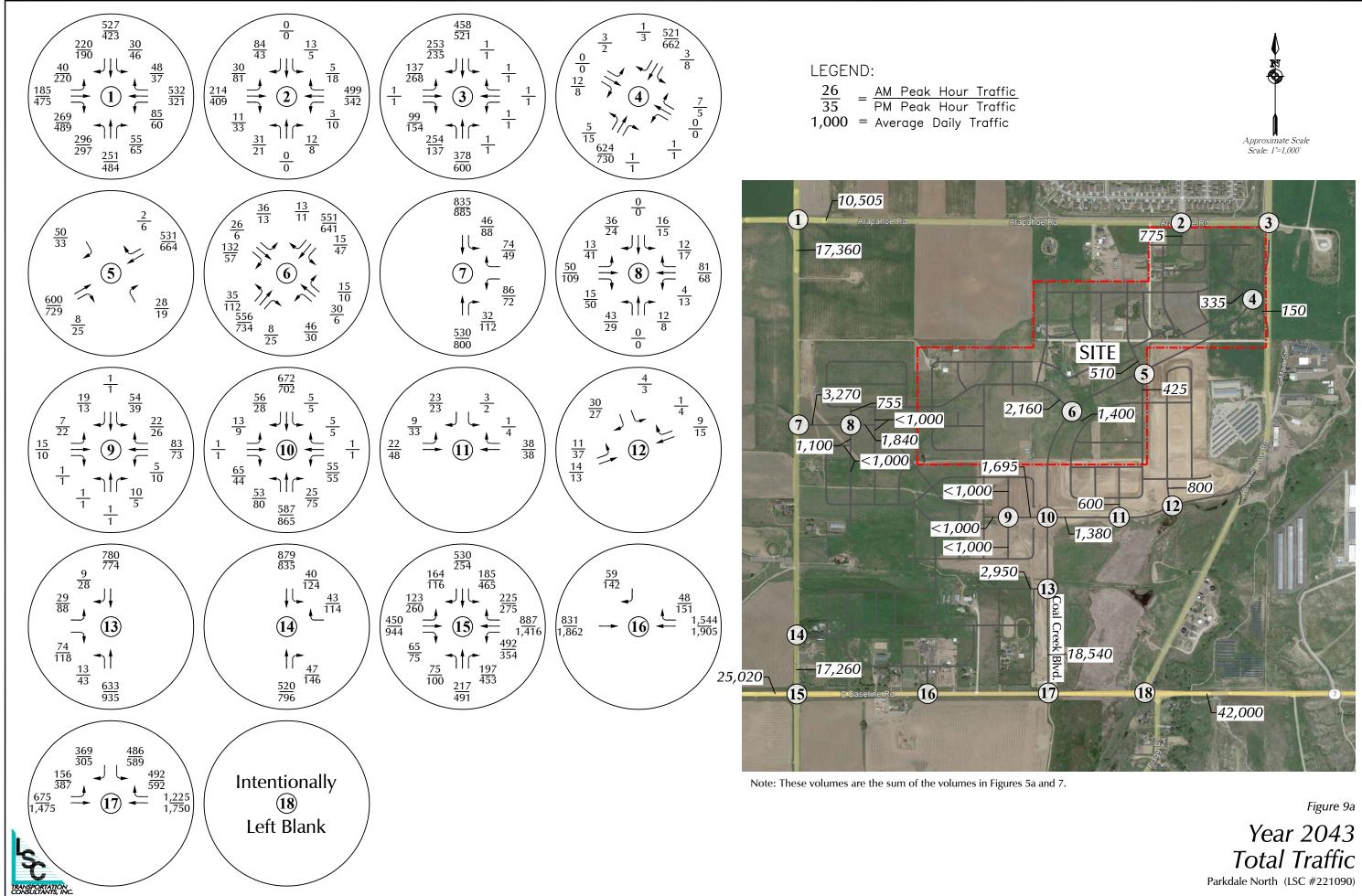












COUNTER MEASURES INC.

N/S STREET: AIRPORT DR E/W STREET: HWY 7 (E. BASELINE RD) CITY: ERIE COUNTY: BOULDER 1889 YORK STREET DENVER.COLORADO 303-333-7409

File Name : AIRPHWY7 Site Code : 00000011 Start Date : 11/2/2023 Page No : 1

COUNTY: BOU	LDER														Page I	No :1	
								Printed-	VEHIC			,					
		AIRPO			E. BAS		RD (H	NY 7)		PRIVA			E. BA		RD (H\	NY 7)	
		South	bound			West	oound			North	oound			Eastb	ound		
Start Time	Left	Thru	Right	Peds	Left	Thru	Right	Peds	Left	Thru	Right	Peds	Left	Thru	Right	Peds	Int. Total
Factor	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
06:30 AM	6	0	4	0	0	193	2	0	0	0	0	0	0	75	0	0	280
06:45 AM	1	0	1	0	0	183	1	0	0	0	0	0	2	83	0	0	271
Total	7	0	5	0	0	376	3	0	0	0	0	0	2	158	0	0	551
07:00 AM	0	0	2	0	1	174	5	0	1	0	0	0	8	107	0	0	298
07:15 AM	2	0	4	0	0	234	4	0	0	0	0	0	3	114	0	0	361
07:30 AM	1	0	2	0	0	278	9	0	0	0	0	0	0	106	0	0	396
07:45 AM	6	0	1	0	0	207	9	0	0	0	0	0	11	149	0	0	383
Total	9	0	9	0	1	893	27	0	1	0	0	0	22	476	0	0	1438
08:00 AM	0	0	2	0	0	209	6	0	0	0	0	0	2	148	0	0	367
08:15 AM	1	0	3	0	0	205	7	0	0	0	0	0	6	139	0	0	361
Total	1	0	5	0	0	414	13	0	0	0	0	0	8	287	0	0	728
04:00 PM	11	0	6	0	0	155	3	0	0	0	0	0	4	280	0	0	459
04:15 PM 04:30 PM	2 14	1 0	7 6	0 0	0 0	200 162	8	0 0	0 0	0	0 0	0 0	6 4	236	0	0	460 453
04:45 PM	8	0	3	0	0	162	2 5	0	0	0 0	0	0	4	265 259	0 0	0 0	453
Total	35	1	22	0	0	682	18	0	0	0	0	0	17	1040	0	0	1815
05:00 PM	18	0	9	0	0	157	1	0	0	0	0	0	4	249	0	0	438
05:15 PM	9	0	6	0	0	159	7	0	0	0	0	0	0	274	0	0	455
05:30 PM	8	0	10	0	0	166	2	1	0	0	0	0	6	272	0	0	465
05:45 PM	4	1	0	0	0	152	3	0	0	0	0	0	1	248	0	0	409
Total	39	1	25	0	0	634	13	1	0	0	0	0	11	1043	0	0	1767
Grand Total Apprch % Total %	91 57.2 1.4	2 1.3 0.0	66 41.5 1.0	0 0.0 0.0	1 0.0 0.0	2999 97.5 47.6	74 2.4 1.2	1 0.0 0.0	1 100.0 0.0	0 0.0 0.0	0 0.0 0.0	0 0.0 0.0	60 2.0 1.0	3004 98.0 47.7	0 0.0 0.0	0 0.0 0.0	6299

COUNTER MEASURES INC. 1889 YORK STREET DENVER.COLORADO

303-333-7409

N/S STREET: AIRPORT DR E/W STREET: HWY 7 (E. BASELINE RD) CITY: ERIE COUNTY: BOULDER

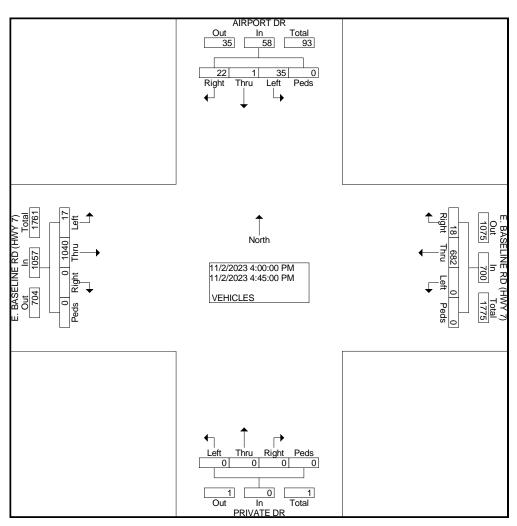
			POR outhbo			E. B		INE R estbo	D (HV und	/Y 7)			VATE			E.B		INE R	D (HV Ind	/Y 7)	
Start Time	Left	Thr u		Ped s	App. Total	Left	Thr u			App. Total	Left	Thr u		Ped s	App. Total	Left	Thr u		Ped s	App. Total	Int. Total
Peak Hour F	-rom 0			08:15	AM - Pe	eak 1 d		III	3	TOLAI		u	m	3	Total		u	III	3	Total	TOTAL
Intersecti on	07:15	AM																			
Volume	9	0	9	0	18	0	928	28	0	956	0	0	0	0	0	16	517	0	0	533	1507
Percent	50. 0	0.0	50. 0	0.0		0.0	97. 1	2.9	0.0		0.0	0.0	0.0	0.0		3.0	97. 0	0.0	0.0		
07:30 Volume Peak	1	0	2	0	3	0	278	9	0	287	0	0	0	0	0	0	106	0	0	106	396 0.951
Factor High Int. Volume Peak Factor	07:45 6	AM 0	1	0	7 0.64 3	07:30 0) AM 278	9	0	287 0.83 3	6:15:0 0	MA 00 0	0	0	0	07:45 11	5 AM 149	0	0	160 0.83 3	
									Out 44 9 Right ↓	0		otal 62 0 2°eds									
		F BASFLINE RD (HWY 7)	Out In Total 937 533 1470	Dede Didth Thru Left					11/2/2	Nort 2023 7:15 2023 8:00 CLES	5:00 AM					Thru Left	928 0	E. BASELINE RD (HWY 7) Out In Total 526 956 1482			
									0 0 0 Out	Thru 0	0 0 To	0									

COUNTER MEASURES INC.

N/S STREET: AIRPORT DR E/W STREET: HWY 7 (E. BASELINE RD) CITY: ERIE COUNTY: BOULDER 1889 YORK STREET DENVER.COLORADO 303-333-7409

File Name : AIRPHWY7 Site Code : 00000011 Start Date : 11/2/2023 Page No : 3

			PORT			E. B			D (HV	/Y 7)			IVATE			E.E	ASEL		`	/Y 7)	
		Sc	outhbo	und			VV	estbou	ind			N	orthbo	und			E	astbou	ind		
Start	Left	Thr	Rig	Ped	App.	Left	Thr		Ped	App.	Left	Thr	Rig	Ped	App.	Left	Thr	Rig	Ped	App.	Int.
Time		u	ht	S	Total		u	ht	S	Total		u	ht	S	Total		u	ht	S	Total	Total
Peak Hour I	From C	04:00 F	PM to (05:45 I	PM - Pe	eak 1 c	of 1														
Intersecti on	04:00) PM																			
Volume	35	1	22	0	58	0	682	18	0	700	0	0	0	0	0	17	104 0	0	0	1057	1815
Percent	60. 3	1.7	37. 9	0.0		0.0	97. 4	2.6	0.0		0.0	0.0	0.0	0.0		1.6	98. 4	0.0	0.0		
04:15 Volume Peak	2	1	7	0	10	0	200	8	0	208	0	0	0	0	0	6	236	0	0	242	460 0.986
Factor High Int. Volume Peak Factor	04:30 14) PM 0	6	0	20 0.72 5	04:15 0	PM 200	8	0	208 0.84 1	0	0	0	0	0	04:00 4) PM 280	0	0	284 0.93 0	



Page 1

CITY: ERIE

COUNTY: BOULDER

DIRECTION: NORTH/SOUTH

LOCATION: AIRPORT DR. N-O E. BASELINE RD (HWY 7)

COUNTER MEASURES INC. 1889 YORK STREET DENVER,COLORADO 80206 303-333-7409

Site Code: 230714 Station ID: 230714

Start	07-Nov-23							
Time	Tue	NORTH	SOUTH			-		 Total
12:00 AM		*	*					*
01:00		*	*					*
02:00		*	*					*
03:00		*	*					*
04:00		*	*					*
05:00		*	*					*
06:00		*	*					*
07:00		*	*					*
08:00		*	*					*
09:00		*	*					*
10:00		28	25					53
11:00		23	27					50
12:00 PM		33	33					66
01:00		32	28					60
02:00		27	24					51
03:00		26	37					63
04:00		22	34					56
05:00		15	42					57
06:00		16	16					32
07:00		12	26					38
08:00		4	11					15
09:00		1	4					5
10:00		2	3					5
11:00		1	2					15 5 5 3
Total		242	312					554
Percent		43.7%	56.3%					
AM Peak	-	10:00	11:00	-	-	-	-	 10:00
Vol.	-	28	27	-	-	-	-	 53
PM Peak	-	12:00	17:00	-	-	-	-	 12:00
Vol.	-	33	42	-	-	-	-	 66

Page 2

CITY: ERIE

COUNTY: BOULDER

DIRECTION: NORTH/SOUTH

LOCATION: AIRPORT DR. N-O E. BASELINE RD (HWY 7)

COUNTER MEASURES INC. 1889 YORK STREET DENVER,COLORADO 80206 303-333-7409

Site Code: 230714 Station ID: 230714

Start Time	08-Nov-23 Wed									Total
12:00 AM	vved	NORTH 0	SOUTH							
01:00		0	1							1
01:00		1	0							1
02:00		1	2							1
03.00		1	2							3 3 16
04:00		13	3							16
06:00		34	7							41
07:00		42	28							70
08:00		42	20							70
			33							68
09:00 10:00		35	33							80
11:00		*	*							*
12:00 PM		*	*							*
01:00		*	*							*
01:00		*	*							*
02:00		*	*							*
03:00		*	*							*
04.00		*	*							*
06:00		*	*							*
07:00		*	*							*
07:00		*	*							*
09:00		*	*							*
10:00		*	*							*
11:00		*	*							*
Total		171	104							275
Percent		62.2%	37.8%							275
AM Peak		02.2%	09:00							08:00
Vol.	-	44	33	-	-	-	-	-	-	08.00 71
PM Peak	-	44		-	-	-	-	-	-	71
Vol.	-	-	-	-	-	-	-	-	-	-
Grand Total	-	413	416	-	-	-	-	-	-	829
Percent		413	50.2%							029
reident		49.0%	J0.∠%							
ADT		ADT 788		AADT 788						

LEVEL OF SERVICE DEFINITIONS From *Highway Capacity Manual*, Transportation Research Board

SIGNALIZED INTERSECTION LEVEL OF SERVICE (LOS)

LOS	<u>Average</u> <u>Vehicle Delay</u> sec/vehicle	Operational Characteristics
A	<10 seconds	Describes operations with low control delay, up to 10 sec/veh. This LOS occurs when progression is extremely favorable and most vehicles arrive during the green phase. Many vehicles do not stop at all. Short cycle lengths may tend to contribute to low delay values.
В	10 to 20 seconds	Describes operations with control delay greater than 10 seconds and up to 20 sec/veh. This level generally occurs with good progression, short cycle lengths, or both. More vehicles stop than with LOS A, causing higher levels of delay.
С	20 to 35 seconds	Describes operations with control delay greater than 20 and up to 35 sec/veh. These higher delays may result from only fair progression, longer cycle length, or both. Individual cycle failures may begin to appear at this level. Cycle failure occurs when a given green phase does not serve queued vehicles, and overflows occur. The number of vehicles stopping is significant at this level, though many still pass through the intersection without stopping.
D	35 to 55 seconds	Describes operations with control delay greater than 35 and up to 55 sec/veh. At LOS D, the influence of congestion becomes more noticeable. Longer delays may result from some combination of unfavorable progression, long cycle lengths, and high v/c ratios. Many vehicles stop, and the proportion of vehicles not stopping declines. Individual cycle failures are noticeable.
E	55 to 80 seconds	Describes operations with control delay greater than 55 and up to 80 sec/veh. These high delay values generally indicate poor progression, long cycle lengths, and high v/c ratios. Individual cycle failures are frequent.
F	>80 seconds	Describes operations with control delay in excess of 80 sec/veh. This level, considered unacceptable to most drivers, often occurs with over-saturation, that is, when arrival flow rates exceed the capacity of lane groups. It may also occur at high v/c ratios with many individual cycle failures. Poor progression and long cycle lengths may also contribute significantly to high delay levels.

LEVEL OF SERVICE DEFINITIONS From *Highway Capacity Manual*, Transportation Research Board

UNSIGNALIZED INTERSECTION LEVEL OF SERVICE (LOS) Applicable to Two-Way Stop Control, All-Way Stop Control, and Roundabouts

LOS	Average Vehicle Control Delay	Operational Characteristics
A	<10 seconds	Normally, vehicles on the stop-controlled approach only have to wait up to 10 seconds before being able to clear the intersection. Left-turning vehicles on the uncontrolled street do not have to wait to make their turn.
В	10 to 15 seconds	Vehicles on the stop-controlled approach will experience delays before being able to clear the intersection. <u>The delay could be up to 15 seconds.</u> Left-turning vehicles on the uncontrolled street may have to wait to make their turn.
С	15 to 25 seconds	Vehicles on the stop-controlled approach can expect delays in the range of 15 to 25 seconds before clearing the intersection. Motorists may begin to take chances due to the long delays, thereby posing a safety risk to through traffic. Left-turning vehicles on the uncontrolled street will now be required to wait to make their turn causing a queue to be created in the turn lane.
D	25 to 35 seconds	This is the point at which a traffic signal may be warranted for this intersection. The delays for the stop-controlled intersection are not considered to be excessive. The length of the queue may begin to block other public and private access points.
E	35 to 50 seconds	The delays for all critical traffic movements are considered to be unacceptable. The length of the queues for the stop-controlled approaches as well as the left-turn movements are extremely long. <u>There is a high probability that this intersection will meet traffic</u> <u>signal warrants.</u> The ability to install a traffic signal is affected by the location of other existing traffic signals. Consideration may be given to restricting the accesses by eliminating the left-turn move- ments from and to the stop-controlled approach.
F	>50 seconds	The delay for the critical traffic movements are probably in excess of 100 seconds. The length of the queues are extremely long. Motorists are selecting alternative routes due to the long delays. <u>The only remedy for these long delays is installing a traffic signal</u> <u>or restricting the accesses.</u> The potential for accidents at this inter- section are extremely high due to motorist taking more risky chances. If the median permits, motorists begin making two-stage left-turns.

Int Delay, s/veh	0.5					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	٦	1	1	1	۰¥	
Traffic Vol, veh/h	16	517	928	28	9	9
Future Vol, veh/h	16	517	928	28	9	9
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	0	0	-
Veh in Median Storage,	# -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	17	562	1009	30	10	10

Major/Minor	Major1	Ν	1ajor2	[Vinor2	
Conflicting Flow All	1039	0	-		1605	1009
Stage 1	-	-	-	-	1009	-
Stage 2	-	-	-	-	596	-
Critical Hdwy	4.12	-	-	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	-	-	-	-	5.42	-
Follow-up Hdwy	2.218	-	-	-	3.518	3.318
Pot Cap-1 Maneuver	669	-	-	-	116	292
Stage 1	-	-	-	-	352	-
Stage 2	-	-	-	-	550	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver		-	-	-	113	292
Mov Cap-2 Maneuver	r -	-	-	-	113	-
Stage 1	-	-	-	-	343	-
Stage 2	-	-	-	-	550	-
Approach	EB		WB		SB	
HCM Control Delay, s	s 0.3		0		30.1	
HCM LOS					D	
Minor Lane/Major Mvi	mt	EBL	EBT	WBT	WBR S	SBLn1
Capacity (veh/h)		669	-	-	-	163
HCM Lane V/C Ratio		0.026	-	-	-	0.12
HCM Control Delay (s	5)	10.5	-	-	-	30.1
HCM Lane LOS		В	-	-	-	D
HCM 95th %tile Q(vel	h)	0.1	-	-	-	0.4

Int Delay, s/veh	2.5					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	٦	1	1	1	Y	
Traffic Vol, veh/h	17	1040	682	18	35	22
Future Vol, veh/h	17	1040	682	18	35	22
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	0	0	-
Veh in Median Storage	,# -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	18	1130	741	20	38	24

Major/Minor	Major1	Ν	/lajor2	1	Vinor2	
Conflicting Flow All	761	0	-	0	1907	741
Stage 1	-	-	-	-	741	-
Stage 2	-	-	-	-	1166	-
Critical Hdwy	4.12	-	-	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	-	-	-	-	5.42	-
Follow-up Hdwy	2.218	-	-	-	3.518	
Pot Cap-1 Maneuver	851	-	-	-	75	416
Stage 1	-	-	-	-	471	-
Stage 2	-	-	-	-	296	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver		-	-	-	73	416
Mov Cap-2 Maneuver	-	-	-	-	73	-
Stage 1	-	-	-	-	461	-
Stage 2	-	-	-	-	296	-
Approach	EB		WB		SB	
HCM Control Delay, s	0.1		0		77.1	
HCM LOS					F	
Minor Lane/Major Mvr	nt	EBL	EBT	WBT	WBR :	SRI n1
Capacity (veh/h)	m	851	LDI	1001		107
HCM Lane V/C Ratio		0.022	-	-	-	0.579
HCM Control Delay (s	•)	9.3	-	-	-	77.1
HCM Lane LOS	·)	7.5 A	_	-		F
HCM 95th %tile Q(vel	1)	0.1	-	-		2.8
	7	0.1				2.0

Int Delay, s/veh	0.6					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	٦	1	1	1	Y	
Traffic Vol, veh/h	17	585	1015	30	10	10
Future Vol, veh/h	17	585	1015	30	10	10
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	0	0	-
Veh in Median Storage,	# -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	18	636	1103	33	11	11

Major/Minor	Major1	Ν	/lajor2]	Vinor2	
Conflicting Flow All	1136	0	-		1775	1103
Stage 1	-	-	-	-	1103	-
Stage 2	-	-	-	-	672	-
Critical Hdwy	4.12	-	-	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	-	-	-	-	5.42	-
Follow-up Hdwy	2.218	-	-	-	3.518	
Pot Cap-1 Maneuver	615	-	-	-	91	257
Stage 1	-	-	-	-	318	-
Stage 2	-	-	-	-	508	-
Platoon blocked, %	. /15	-	-	-	00	257
Mov Cap-1 Maneuver		-	-	-	88	257
Mov Cap-2 Maneuver	· -	-	-	-	88	-
Stage 1	-	-	-	-	309	-
Stage 2	-	-	-	-	508	-
Approach	EB		WB		SB	
HCM Control Delay, s	s 0.3		0		37.9	
HCM LOS					E	
Minor Lane/Major Mv	mt	EBL	EBT	WBT	WBR S	SBLn1
Capacity (veh/h)		615	-	-	-	131
HCM Lane V/C Ratio		0.03	-	-	-	0.166
HCM Control Delay (s	5)	11	-	-	-	37.9
HCM Lane LOS		В	-	-	-	E
HCM 95th %tile Q(vel	h)	0.1	-	-	-	0.6

Int Delay, s/veh	5					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	٦	1	1	1	Y	
Traffic Vol, veh/h	18	1150	820	19	37	23
Future Vol, veh/h	18	1150	820	19	37	23
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	0	0	-
Veh in Median Storage,	# -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	20	1250	891	21	40	25

Major/Minor	Major1	Ν	/lajor2	1	Vinor2	
Conflicting Flow All	912	0	- 10/2		2181	891
Stage 1	712	-	-	-	891	- 071
Stage 2	-	-		-	1290	
Critical Hdwy	4.12	-	-	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	-	-	-	-	5.42	-
Follow-up Hdwy	2.218	-	-	-	3.518	3.318
Pot Cap-1 Maneuver	747	-	-	-	51	341
Stage 1	-	-	-	-	401	-
Stage 2	-	-	-	-	258	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver		-	-	-	50	341
Mov Cap-2 Maneuver	-	-	-	-	50	-
Stage 1	-	-	-	-	390	-
Stage 2	-	-	-	-	258	-
Approach	EB		WB		SB	
HCM Control Delay, s	0.2		0		168.4	
HCM LOS					F	
Minor Lane/Major Mvr	nt	EBL	EBT	WBT	WBR 3	SBLn1
Capacity (veh/h)		747	-	-	-	74
HCM Lane V/C Ratio		0.026	-	-	-	0.881
HCM Control Delay (s)	9.9	-	-	-	168.4
HCM Lane LOS		А	-	-	-	F
HCM 95th %tile Q(veh	1)	0.1	-	-	-	4.4

Int Delay, s/veh	1.8					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	٦	1	1	1	٦	1
Traffic Vol, veh/h	99	585	1015	84	17	21
Future Vol, veh/h	99	585	1015	84	17	21
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	0	0	0
Veh in Median Storage	,# -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	108	636	1103	91	18	23

Major/Minor	Major1	Ма	ajor2	ľ	Minor2	
Conflicting Flow All	1194	0	-	0	1955	1103
Stage 1	-	-	-	-	1103	-
Stage 2	-	-	-	-	852	-
Critical Hdwy	4.12	-	-	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	-	-	-	-	5.42	-
Follow-up Hdwy	2.218	-	-	-	3.518	3.318
Pot Cap-1 Maneuver	585	-	-	-	70	257
Stage 1	-	-	-	-	318	-
Stage 2	-	-	-	-	418	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver		-	-	-	57	257
Mov Cap-2 Maneuver	-	-	-	-	57	-
Stage 1	-	-	-	-	259	-
Stage 2	-	-	-	-	418	-
Approach	EB		WB		SB	
HCM Control Delay, s			0		54.2	
HCM LOS					F	

Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR SBLn1	SBLn2
Capacity (veh/h)	585	-	-	- 57	257
HCM Lane V/C Ratio	0.184	-	-	- 0.324	0.089
HCM Control Delay (s)	12.5	-	-	- 95.9	20.4
HCM Lane LOS	В	-	-	- F	С
HCM 95th %tile Q(veh)	0.7	-	-	- 1.2	0.3

Int Delay, s/veh	24.9					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	٦	1	1	1	٦	1
Traffic Vol, veh/h	31	1150	820	27	84	94
Future Vol, veh/h	31	1150	820	27	84	94
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	0	0	0
Veh in Median Storage	,# -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	34	1250	891	29	91	102

Major/Minor	Major1	Ν	lajor2	N	linor2					
Conflicting Flow All	920	0	-	0	2209	891				
Stage 1	-	-	-	-	891	-				
Stage 2	-	-	-	-	1318	-				
Critical Hdwy	4.12	-	-	-	6.42	6.22				
Critical Hdwy Stg 1	-	-	-	-	5.42	-				
Critical Hdwy Stg 2	-	-	-	-	5.42	-				
Follow-up Hdwy	2.218	-	-	- 3	3.518	3.318				
Pot Cap-1 Maneuver	742	-	-	-	~ 49	341				
Stage 1	-	-	-	-	401	-				
Stage 2	-	-	-	-	250	-				
Platoon blocked, %		-	-	-						
Mov Cap-1 Maneuver	742	-	-	-	~ 47	341				
Mov Cap-2 Maneuver	-	-	-	-	~ 47	-				
Stage 1	-	-	-	-	383	-				
Stage 2	-	-	-	-	250	-				
Approach	EB		WB		SB					
HCM Control Delay, s	0.3		0	\$	307.1					
HCM LOS					F					
Minor Lane/Major Mvr	nt	EBL	EBT	WBT	WBR S	SBLn1 S	BLn2			
Capacity (veh/h)		742	-	-	-	47	341			
HCM Lane V/C Ratio		0.045	-	-	-	1.943	0.3			
HCM Control Delay (s)	10.1	-	-		628.3	20			
HCM Lane LOS	,	В	-	-	-	F	C			
HCM 95th %tile Q(veh	ı)	0.1	-	-	-	9.2	1.2			
Notes										
~: Volume exceeds ca	nacity	\$. Do	lav evo	eeds 30	0s	+· Comr	outation Not De	fined	*: All major volume in platoon	
	pacity	ψ. DC		.ccu3 30	03	Comp		milliou	. All major volume in platoon	

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Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	ሻ	†	†	1	ሻ	1
Traffic Volume (vph)	99	585	1015	84	17	21
Future Volume (vph)	99	585	1015	84	17	21
Turn Type	pm+pt	NA	NA	Perm	Prot	Perm
Protected Phases	5	2	6		4	
Permitted Phases	2			6		4
Detector Phase	5	2	6	6	4	4
Switch Phase						
Minimum Initial (s)	5.0	5.0	5.0	5.0	5.0	5.0
Minimum Split (s)	10.0	20.0	20.0	20.0	20.0	20.0
Total Split (s)	15.0	95.0	80.0	80.0	25.0	25.0
Total Split (%)	12.5%	79.2%	66.7%	66.7%	20.8%	20.8%
Yellow Time (s)	3.0	3.0	3.0	3.0	3.0	3.0
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	-1.0	-1.0
Total Lost Time (s)	5.0	5.0	5.0	5.0	4.0	4.0
Lead/Lag	Lead		Lag	Lag		
Lead-Lag Optimize?	Yes		Yes	Yes		
Recall Mode	None	C-Max	C-Max	C-Max	None	None
Act Effct Green (s)	107.5	109.5	94.4	94.4	7.8	7.8
Actuated g/C Ratio	0.90	0.91	0.79	0.79	0.06	0.06
v/c Ratio	0.31	0.37	0.75	0.07	0.16	0.19
Control Delay	4.4	2.1	14.3	1.4	55.5	23.1
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	4.4	2.1	14.3	1.4	55.5	23.1
LOS	А	А	В	А	E	С
Approach Delay		2.5	13.3		37.3	
Approach LOS		А	В		D	
Intersection Summary						
Cycle Length: 120						
Actuated Cycle Length: 12	0					
Offset: 0 (0%), Referenced	I to phase 2	:EBTL an	d 6:WBT	, Start of (Green	
Natural Cycle: 90						
Control Type: Actuated-Co	ordinated					
Maximum v/c Ratio: 0.75						
Intersection Signal Delay:	9.7			Ir	ntersectio	n LOS: A
Intersection Capacity Utiliz	ation 74.7%)		[(CU Level	of Service
Analysis Period (min) 15						

Splits and Phases: 2: SH 7 (Baseline Rd) & Airport Road

4 _{Ø2 (R)}		Ø4	
95 s		25 s	
	 Ø6 (R)		
15 s	80 s		

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Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	٦	†	↑	1	٦	1
Traffic Volume (veh/h)	99	585	1015	84	17	21
Future Volume (veh/h)	99	585	1015	84	17	21
Initial Q (Qb), veh	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00			1.00	1.00	1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No	No		No	
Adj Sat Flow, veh/h/ln	1870	1870	1870	1870	1870	1870
Adj Flow Rate, veh/h	108	636	1103	91	18	23
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Percent Heavy Veh, %	2	2	2	2	2	2
Cap, veh/h	376	1656	1503	1273	70	62
Arrive On Green	0.04	0.89	0.80	0.80	0.04	0.04
Sat Flow, veh/h	1781	1870	1870	1585	1781	1585
Grp Volume(v), veh/h	108	636	1103	91	18	23
Grp Sat Flow(s), veh/h/ln	1781	1870	1870	1585	1781	1585
Q Serve(g_s), s	1.1	7.1	33.9	1.4	1.2	1.7
Cycle Q Clear(g_c), s	1.1	7.1	33.9	1.4	1.2	1.7
Prop In Lane	1.00	7.1	00.7	1.00	1.00	1.00
Lane Grp Cap(c), veh/h	376	1656	1503	1273	70	62
V/C Ratio(X)	0.29	0.38	0.73	0.07	0.26	0.37
Avail Cap(c_a), veh/h	453	1656	1503	1273	312	277
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	1.00	1.00	1.00	1.00
Uniform Delay (d), s/veh	8.2	1.00	5.7	2.5	55.9	56.2
Incr Delay (d2), s/veh	0.2	0.7	3.2	0.1	1.9	3.6
	0.4		3.Z 0.0		0.0	5.0 0.0
Initial Q Delay(d3),s/veh		0.0		0.0		
%ile BackOfQ(50%),veh/In	0.9	0.3	8.2	0.3	0.6	1.6
Unsig. Movement Delay, s/veh		1.0	0.0	27	57.0	F0 0
LnGrp Delay(d),s/veh	8.6	1.9	8.9	2.6	57.8	59.8
LnGrp LOS	A	Α	Α	A	E	E
Approach Vol, veh/h		744	1194		41	
Approach Delay, s/veh		2.8	8.4		58.9	
Approach LOS		А	А		E	
Timer - Assigned Phs		2		4	5	6
Phs Duration (G+Y+Rc), s		111.3		8.7	9.9	101.4
Change Period (Y+Rc), s		5.0		5.0	5.0	5.0
Max Green Setting (Gmax), s		90.0		20.0	10.0	75.0
Max Q Clear Time (g_c+I1), s		9.1		3.7	3.1	35.9
Green Ext Time (p_c), s		4.0		0.1	0.1	10.8
Intersection Summary						
HCM 6th Ctrl Delay			7.4			
HCM 6th LOS			A			
			A			

	٦	→	+	×	1	1
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	ሻ	†	†	1	ሻ	1
Traffic Volume (vph)	31	1150	820	27	84	94
Future Volume (vph)	31	1150	820	27	84	94
Turn Type	pm+pt	NA	NA	Perm	Prot	Perm
Protected Phases	5	2	6		4	
Permitted Phases	2			6		4
Detector Phase	5	2	6	6	4	4
Switch Phase						
Minimum Initial (s)	5.0	5.0	5.0	5.0	5.0	5.0
Minimum Split (s)	10.0	20.0	20.0	20.0	20.0	20.0
Total Split (s)	15.0	95.0	80.0	80.0	25.0	25.0
Total Split (%)	12.5%	79.2%	66.7%	66.7%	20.8%	20.8%
Yellow Time (s)	3.0	3.0	3.0	3.0	3.0	3.0
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	-1.0	-1.0
Total Lost Time (s)	5.0	5.0	5.0	5.0	4.0	4.0
Lead/Lag	Lead		Lag	Lag		
Lead-Lag Optimize?	Yes		Yes	Yes		
Recall Mode	None	C-Max	C-Max	C-Max	None	None
Act Effct Green (s)	98.5	98.5	91.8	91.8	12.5	12.5
Actuated g/C Ratio	0.82	0.82	0.76	0.76	0.10	0.10
v/c Ratio	0.08	0.82	0.63	0.02	0.49	0.40
Control Delay	3.2	12.0	10.4	1.6	59.3	13.8
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	3.2	12.0	10.4	1.6	59.3	13.8
LOS	А	В	В	А	E	В
Approach Delay		11.7	10.1		35.2	
Approach LOS		В	В		D	
Intersection Summary						
Cycle Length: 120						
Actuated Cycle Length: 120)					
Offset: 0 (0%), Referenced	to phase 2	:EBTL an	d 6:WBT	Start of	Green	
Natural Cycle: 90						
Control Type: Actuated-Coo	ordinated					
Maximum v/c Ratio: 0.82						
Intersection Signal Delay: 1				Ir	ntersectio	n LOS: B
Intersection Capacity Utiliza	ation 72.7%)		[(CU Level	of Service
Analysis Period (min) 15						

Splits and Phases: 2: SH 7 (Baseline Rd) & Airport Road



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Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	۲	<u> </u>	1	1	5	1
Traffic Volume (veh/h)	31	1150	820	27	84	94
Future Volume (veh/h)	31	1150	820	27	84	94
Initial Q (Qb), veh	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00			1.00	1.00	1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No	No		No	
Adj Sat Flow, veh/h/ln	1870	1870	1870	1870	1870	1870
Adj Flow Rate, veh/h	34	1250	891	29	91	102
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Percent Heavy Veh, %	2	2	2	2	2	2
Cap, veh/h	444	1560	1430	1212	162	144
Arrive On Green	0.03	0.83	0.76	0.76	0.09	0.09
Sat Flow, veh/h	1781	1870	1870	1585	1781	1585
Grp Volume(v), veh/h	34	1250	891	29	91	102
Grp Sat Flow(s), veh/h/ln	1781	1870	1870	1585	1781	1585
Q Serve(g_s), s	0.4	40.1	25.7	0.5	5.9	7.5
Cycle Q Clear(g_c), s	0.4	40.1	25.7	0.5	5.9	7.5
Prop In Lane	1.00			1.00	1.00	1.00
Lane Grp Cap(c), veh/h	444	1560	1430	1212	162	144
V/C Ratio(X)	0.08	0.80	0.62	0.02	0.56	0.71
Avail Cap(c_a), veh/h	542	1560	1430	1212	312	277
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	1.00	1.00	1.00	1.00
Uniform Delay (d), s/veh	5.6	5.0	6.4	3.4	52.3	53.0
Incr Delay (d2), s/veh	0.1	4.4	2.1	0.0	3.1	6.3
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	0.1	7.6	7.4	0.1	2.8	6.7
Unsig. Movement Delay, s/veh						
LnGrp Delay(d),s/veh	5.7	9.4	8.4	3.4	55.3	59.3
LnGrp LOS	А	А	А	А	E	E
Approach Vol, veh/h		1284	920		193	
Approach Delay, s/veh		9.3	8.3		57.4	
Approach LOS		A	A		E	
						,
Timer - Assigned Phs		2		4	5	6
Phs Duration (G+Y+Rc), s		105.1		14.9	8.4	96.7
Change Period (Y+Rc), s		5.0		5.0	5.0	5.0
Max Green Setting (Gmax), s		90.0		20.0	10.0	75.0
Max Q Clear Time (g_c+I1), s		42.1		9.5	2.4	27.7
Green Ext Time (p_c), s		14.9		0.4	0.0	7.0
Intersection Summary						
HCM 6th Ctrl Delay			12.8			
HCM 6th LOS			12.0 B			
			U			

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Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	ሻ	††	† †	1	5	1
Traffic Volume (vph)	100	1055	1675	85	30	40
Future Volume (vph)	100	1055	1675	85	30	40
Turn Type	pm+pt	NA	NA	Perm	Prot	Perm
Protected Phases	5	2	6		4	
Permitted Phases	2			6		4
Detector Phase	5	2	6	6	4	4
Switch Phase						
Minimum Initial (s)	5.0	5.0	5.0	5.0	5.0	5.0
Minimum Split (s)	10.0	20.0	20.0	20.0	20.0	20.0
Total Split (s)	20.0	95.0	75.0	75.0	25.0	25.0
Total Split (%)	16.7%	79.2%	62.5%	62.5%	20.8%	20.8%
Yellow Time (s)	3.0	3.0	3.0	3.0	3.0	3.0
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	5.0	5.0	5.0	5.0	5.0	5.0
Lead/Lag	Lead		Lag	Lag		
Lead-Lag Optimize?	Yes		Yes	Yes		
Recall Mode	None	C-Max	C-Max	C-Max	None	None
Act Effct Green (s)	104.4	105.4	91.2	91.2	7.7	7.7
Actuated g/C Ratio	0.87	0.88	0.76	0.76	0.06	0.06
v/c Ratio	0.46	0.37	0.68	0.08	0.29	0.30
Control Delay	21.9	1.2	2.8	0.1	59.3	20.9
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	21.9	1.2	2.8	0.1	59.3	20.9
LOS	С	А	А	А	E	С
Approach Delay		3.0	2.7		37.6	
Approach LOS		А	А		D	
Intersection Summary						
Cycle Length: 120						
Actuated Cycle Length: 12	0					
Offset: 42 (35%), Reference	ced to phase	2:EBTL	and 6:WE	3T, Start o	of Green	
Natural Cycle: 75						
Control Type: Actuated-Co	ordinated					
Maximum v/c Ratio: 0.68						
Intersection Signal Delay:				Ir	ntersectio	n LOS: A
Intersection Capacity Utiliz	ation 68.5%)		[(CU Level	of Service
Analysis Period (min) 15						

Splits and Phases: 2: SH 7 (Baseline Rd) & Airport Road

		≪ ↓ Ø4
95 s		25 s
▶ _{Ø5}	 Ø6 (R)	
20 s	75 s	

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Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	1	† †	† †	1	<u> </u>	1
Traffic Volume (veh/h)	100	1055	1675	85	30	40
Future Volume (veh/h)	100	1055	1675	85	30	40
Initial Q (Qb), veh	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00			1.00	1.00	1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No	No		No	
Adj Sat Flow, veh/h/ln	1870	1870	1870	1870	1870	1870
Adj Flow Rate, veh/h	109	1147	1821	92	33	43
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Percent Heavy Veh, %	2	2	2	2	2	2
Cap, veh/h	267	3112	2820	1258	73	65
Arrive On Green	0.04	0.88	0.79	0.79	0.04	0.04
Sat Flow, veh/h	1781	3647	3647	1585	1781	1585
Grp Volume(v), veh/h	109	1147	1821	92	33	43
Grp Sat Flow(s), veh/h/ln	1781	1777	1777	1585	1781	1585
Q Serve(\underline{g}), s	1.2	7.1	26.1	1.5	2.2	3.2
Cycle Q Clear(g_c), s	1.2	7.1	26.1	1.5	2.2	3.2
Prop In Lane	1.00	/.1	20.1	1.00	1.00	1.00
Lane Grp Cap(c), veh/h	267	3112	2820	1258	73	65
V/C Ratio(X)	0.41	0.37	0.65	0.07	0.45	0.66
Avail Cap(c_a), veh/h	418	3112	2820	1258	297	264
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	1.00	1.00	1.00	1.00
Uniform Delay (d), s/veh	7.6	1.00	5.3	2.7	56.2	56.7
Incr Delay (d2), s/veh	1.0	0.3	1.2	0.1	4.3	10.9
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.1	4.3 0.0	0.0
%ile BackOfQ(50%),veh/ln	0.0	0.0	5.8	0.0	1.1	3.0
· · · ·		0.5	0.C	0.5	1.1	5.0
Unsig. Movement Delay, s/veh		1.7	6 1	2.0	40 E	676
LnGrp Delay(d),s/veh	8.6		6.4	2.8	60.5	67.6
LnGrp LOS	A	A	A	А	E	E
Approach Vol, veh/h		1256	1913		76	
Approach Delay, s/veh		2.3	6.2		64.5	
Approach LOS		A	A		E	
Timer - Assigned Phs		2		4	5	6
Phs Duration (G+Y+Rc), s		110.1		9.9	9.9	100.2
Change Period (Y+Rc), s		5.0		5.0	5.0	5.0
Max Green Setting (Gmax), s		90.0		20.0	15.0	70.0
Max Q Clear Time (g_c+I1), s		9.1		5.2	3.2	28.1
Green Ext Time (p_c), s		9.3		0.1	0.2	19.7
Intersection Summary						
HCM 6th Ctrl Delay			6.1			
HCM 6th LOS			A			
			А			

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Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	ሻ	† †	† †	1	5	1
Traffic Volume (vph)	100	2000	2235	50	90	100
Future Volume (vph)	100	2000	2235	50	90	100
Turn Type	pm+pt	NA	NA	Perm	Prot	Perm
Protected Phases	5	2	6		4	
Permitted Phases	2			6		4
Detector Phase	5	2	6	6	4	4
Switch Phase						
Minimum Initial (s)	5.0	5.0	5.0	5.0	5.0	5.0
Minimum Split (s)	10.0	20.0	20.0	20.0	20.0	20.0
Total Split (s)	12.0	90.0	78.0	78.0	30.0	30.0
Total Split (%)	10.0%	75.0%	65.0%	65.0%	25.0%	25.0%
Yellow Time (s)	3.0	3.0	3.0	3.0	3.0	3.0
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	-1.0	-2.0
Total Lost Time (s)	5.0	5.0	5.0	5.0	4.0	3.0
Lead/Lag	Lead		Lag	Lag		
Lead-Lag Optimize?	Yes		Yes	Yes		
Recall Mode	None	C-Max	C-Max	C-Max	None	None
Act Effct Green (s)	98.0	98.0	84.2	84.2	13.0	14.0
Actuated g/C Ratio	0.82	0.82	0.70	0.70	0.11	0.12
v/c Ratio	0.57	0.75	0.98	0.05	0.51	0.40
Control Delay	24.5	9.0	21.6	4.7	59.2	15.5
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	24.5	9.0	21.6	4.7	59.2	15.5
LOS	С	А	С	А	E	В
Approach Delay		9.8	21.2		36.2	
Approach LOS		А	С		D	
Intersection Summary						
Cycle Length: 120						
Actuated Cycle Length: 12	0					
Offset: 0 (0%), Referenced	I to phase 2	:EBTL an	d 6:WBT,	, Start of (Green	
Natural Cycle: 100						
Control Type: Actuated-Co	ordinated					
Maximum v/c Ratio: 0.98						
Intersection Signal Delay:	16.6			Ir	ntersectio	n LOS: B
Intersection Capacity Utiliz)		(CU Level	of Service
Analysis Period (min) 15						
J						

Splits and Phases: 2: SH 7 (Baseline Rd) & Airport Road

Ø2 (R) ♥	≪ ™ Ø4
90 s	30 s
Ø5 Ø6 (R)	
12 s 78 s	

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Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	<u> </u>	<u></u>	1	1	<u> </u>	1
Traffic Volume (veh/h)	100	TT 2000	TT 2235	50	90	100
Future Volume (veh/h)	100	2000	2235	50	90	100
Initial Q (Qb), veh	0	2000	2235	0	⁹⁰	0
Ped-Bike Adj(A_pbT)	1.00	0	U	1.00	1.00	1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00
	1.00	No	No	1.00	No	1.00
Work Zone On Approach	1070	1870	1870	1870		1870
Adj Sat Flow, veh/h/ln	1870				1870	
Adj Flow Rate, veh/h	109	2174	2429	54	98	109
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Percent Heavy Veh, %	2	2	2	2	2	2
Cap, veh/h	159	2948	2656	1185	170	165
Arrive On Green	0.04	0.83	0.75	0.75	0.10	0.10
Sat Flow, veh/h	1781	3647	3647	1585	1781	1585
Grp Volume(v), veh/h	109	2174	2429	54	98	109
Grp Sat Flow(s), veh/h/ln	1781	1777	1777	1585	1781	1585
Q Serve(g_s), s	1.5	32.2	65.5	1.1	6.3	7.9
Cycle Q Clear(g_c), s	1.5	32.2	65.5	1.1	6.3	7.9
Prop In Lane	1.00	02.2	00.0	1.00	1.00	1.00
Lane Grp Cap(c), veh/h	159	2948	2656	1185	170	165
V/C Ratio(X)	0.68	0.74	0.91	0.05	0.58	0.66
. ,	191	2948	2656	1185	386	357
Avail Cap(c_a), veh/h						
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	1.00	1.00	1.00	1.00
Uniform Delay (d), s/veh	34.5	4.5	12.1	4.0	51.9	51.7
Incr Delay (d2), s/veh	7.6	1.7	6.2	0.1	3.1	4.5
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	2.7	5.4	19.3	0.3	3.0	7.1
Unsig. Movement Delay, s/veh	l .					
LnGrp Delay(d),s/veh	42.1	6.2	18.4	4.0	55.0	56.3
LnGrp LOS	D	А	В	А	E	E
Approach Vol, veh/h		2283	2483		207	
Approach Delay, s/veh		7.9	18.0		55.7	
Approach LOS		A	B		E	
••						
Timer - Assigned Phs		2		4	5	6
Phs Duration (G+Y+Rc), s		104.5		15.5	9.9	94.7
Change Period (Y+Rc), s		5.0		5.0	5.0	5.0
Max Green Setting (Gmax), s		85.0		25.0	7.0	73.0
Max Q Clear Time (g_c+I1), s		34.2		9.9	3.5	67.5
Green Ext Time (p_c), s		28.4		0.5	0.1	5.1
Intersection Summary						
			15.0			
HCM 6th Ctrl Delay			15.0			
HCM 6th LOS			В			

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Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	ሻ	††	† †	1	ሻ	1
Traffic Volume (vph)	182	1055	1675	139	37	51
Future Volume (vph)	182	1055	1675	139	37	51
Turn Type	pm+pt	NA	NA	Perm	Prot	Perm
Protected Phases	5	2	6		4	
Permitted Phases	2			6		4
Detector Phase	5	2	6	6	4	4
Switch Phase						
Minimum Initial (s)	5.0	5.0	5.0	5.0	5.0	5.0
Minimum Split (s)	10.0	20.0	20.0	20.0	20.0	20.0
Total Split (s)	20.0	95.0	75.0	75.0	25.0	25.0
Total Split (%)	16.7%	79.2%	62.5%	62.5%	20.8%	20.8%
Yellow Time (s)	3.0	3.0	3.0	3.0	3.0	3.0
All-Red Time (s)	2.0	2.0	2.0	2.0	2.0	2.0
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	5.0	5.0	5.0	5.0	5.0	5.0
Lead/Lag	Lead		Lag	Lag		
Lead-Lag Optimize?	Yes		Yes	Yes		
Recall Mode	None	C-Max	C-Max	C-Max	None	None
Act Effct Green (s)	103.9	104.9	85.5	85.5	8.2	8.2
Actuated g/C Ratio	0.87	0.87	0.71	0.71	0.07	0.07
v/c Ratio	0.67	0.37	0.72	0.13	0.33	0.35
Control Delay	44.4	1.3	6.9	0.5	60.0	19.5
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	44.4	1.3	6.9	0.5	60.0	19.5
LOS	D	А	А	А	E	В
Approach Delay		7.6	6.4		36.6	
Approach LOS		А	А		D	
Intersection Summary						
Cycle Length: 120						
Actuated Cycle Length: 12						
Offset: 42 (35%), Reference	ced to phase	2:EBTL	and 6:WE	3T, Start o	of Green	
Natural Cycle: 80						
Control Type: Actuated-Co	ordinated					
Maximum v/c Ratio: 0.72						
Intersection Signal Delay:				Ir	ntersectio	n LOS: A
Intersection Capacity Utiliz	ation 73.1%)		[(CU Level	of Service
Analysis Period (min) 15						

Splits and Phases: 2: SH 7 (Baseline Rd) & Airport Road

		≪ ₩ Ø4	
95 s		25 s	
▶ _{Ø5}	 Ø6 (R)		
20 s	75 s		

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Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	۲	††	††	1	۲	1
Traffic Volume (veh/h)	182	1055	1675	139	37	51
Future Volume (veh/h)	182	1055	1675	139	37	51
Initial Q (Qb), veh	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00			1.00	1.00	1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No	No		No	
Adj Sat Flow, veh/h/ln	1870	1870	1870	1870	1870	1870
Adj Flow Rate, veh/h	198	1147	1821	151	40	55
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Percent Heavy Veh, %	2	2	2	2	2	2
Cap, veh/h	257	3079	2783	1242	89	79
Arrive On Green	0.04	0.87	0.78	0.78	0.05	0.05
Sat Flow, veh/h	1781	3647	3647	1585	1781	1585
						55
Grp Volume(v), veh/h	198	1147	1821	151	40	
Grp Sat Flow(s),veh/h/ln	1781	1777	1777	1585	1781	1585
Q Serve(g_s), s	2.4	7.6	27.3	2.7	2.6	4.1
Cycle Q Clear(g_c), s	2.4	7.6	27.3	2.7	2.6	4.1
Prop In Lane	1.00			1.00	1.00	1.00
Lane Grp Cap(c), veh/h	257	3079	2783	1242	89	79
V/C Ratio(X)	0.77	0.37	0.65	0.12	0.45	0.69
Avail Cap(c_a), veh/h	406	3079	2783	1242	297	264
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	1.00	1.00	1.00	1.00
Uniform Delay (d), s/veh	19.4	1.6	5.8	3.1	55.4	56.1
Incr Delay (d2), s/veh	4.8	0.3	1.2	0.2	3.5	10.2
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/In	4.8	0.5	6.5	0.6	1.3	3.8
Unsig. Movement Delay, s/veh						
LnGrp Delay(d),s/veh	24.2	1.9	7.0	3.3	58.9	66.3
LnGrp LOS	С.	A	7.0 A	A	E	E
Approach Vol, veh/h		1345	1972		95	<u>L</u>
••		5.2	6.7		63.2	
Approach Delay, s/veh						
Approach LOS		А	А		E	
Timer - Assigned Phs		2		4	5	6
Phs Duration (G+Y+Rc), s		109.0		11.0	10.0	99.0
Change Period (Y+Rc), s		5.0		5.0	5.0	5.0
Max Green Setting (Gmax), s		90.0		20.0	15.0	70.0
Max Q Clear Time (q_c+11) , s		9.6		6.1	4.4	29.3
Green Ext Time (p_c), s		9.3		0.2	0.4	19.8
		7.0		0.2	0.1	17.0
Intersection Summary						
HCM 6th Ctrl Delay			7.7			
HCM 6th LOS			А			

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EBL	EBT	WBT	WBR	SBL	SBR
ሻ			1	ሻ	1
78	2000	2235	58	137	171
78	2000	2235	58	137	171
pm+pt	NA	NA	Perm	Prot	Perm
5	2	6		4	
2			6		4
5	2	6	6	4	4
5.0	5.0	5.0	5.0	5.0	5.0
10.0	20.0	20.0	20.0	20.0	20.0
12.0	90.0	78.0	78.0	30.0	30.0
10.0%	75.0%	65.0%	65.0%	25.0%	25.0%
3.0	3.0	3.0	3.0	3.0	3.0
2.0	2.0	2.0	2.0	2.0	2.0
0.0	0.0	0.0	0.0	-1.0	-2.0
5.0	5.0	5.0	5.0	4.0	3.0
Lead		Lag	Lag		
Yes		Yes	Yes		
None	C-Max	C-Max	C-Max	None	None
94.6	94.6		84.2	16.4	17.4
0.79	0.79	0.70	0.70	0.14	0.14
0.49	0.78	0.98	0.06	0.62	0.59
20.7	11.1	21.7	4.8	59.5	29.8
0.0	0.0	0.0	0.0	0.0	0.0
20.7	11.1	21.7	4.8	59.5	29.8
С	В	С	А	E	С
	11.5	21.3		43.0	
	В	С		D	
o phase 2	:EBTL an	d 6:WBT,	Start of (Green	
o phase 2	:EBTL an	d 6:WBT,	Start of (Green	
o phase 2 dinated	:EBTL an	d 6:WBT,	Start of (Green	
	:EBTL an	d 6:WBT,	Start of (Green	
	:EBTL an	d 6:WBT,		Green ntersectio	n LOS: B
dinated		d 6:WBT,	Ir	ntersectio	n LOS: B of Service
	 78 70 <	↑↑ 78 2000 78 2000 78 2000 78 2000 pm+pt NA 5 2 2 2 5 2 5 2 5 2 5 2 5 2 5 2 0 20 10.0 20.0 10.0% 75.0% 3.0 3.0 2.0 2.0 0.0 0.0 10.0% 75.0% 3.0 3.0 2.0 0.0 0.0 0.0 5.0 5.0 Lead - Yes - None C-Max 94.6 94.6 0.79 0.79 0.49 0.78 20.7 11.1 0.0 0.0 20.7 11.1 C B 11.5	↑↑ ↑↑ 78 2000 2235 78 2000 2235 78 2000 2235 pm+pt NA NA 5 2 6 2 2 6 2 2 6 2 2 6 2 2 6 2 2 6 2 2 6 2 2 6 2 2 6 2 2 6 2 2 6 10.0 20.0 20.0 10.0 90.0 78.0 10.0 90.0 78.0 10.0 0.0 0.0 2.0 2.0 2.0 0.0 0.0 0.0 2.0 2.0 2.0 0.0 0.0 0.0 2.0 2.0 2.0 0.0 0.0 0.0 <td>↑ ↑↑ ↑↑ 78 2000 2235 58 78 2000 2235 58 78 2000 2235 58 pm+pt NA NA Perm 5 2 6 6 2 - 6 6 5 2 6 6 0 - - 6 5 2 6 6 0 - - 6 5 2 6 6 0 - - 6 5 2 0 6 0 - 20.0 20.0 10.0 20.0 20.0 20.0 12.0 90.0 78.0 78.0 10.0% 75.0% 65.0% 65.0% 3.0 3.0 3.0 2.0 0.0 0.0 0.0 2.0 0.0 5.0 5.0</td> <td>M M M M M 78 2000 2235 58 137 78 2000 2235 58 137 pm+pt NA NA Perm Prot 5 2 6 4 2 - 6 4 2 2 6 4 2 - 6 4 2 - 6 4 2 - 6 4 2 - 6 4 2 - 6 4 2 - 6 4 2 2 6 6 50 5.0 5.0 5.0 10.0 20.0 20.0 20.0 11.0 20.0 20.0 20.0 10.0% 75.0% 65.0% 65.0% 3.0 3.0 3.0 3.0 3.0 3.0 2.0</td>	↑ ↑↑ ↑↑ 78 2000 2235 58 78 2000 2235 58 78 2000 2235 58 pm+pt NA NA Perm 5 2 6 6 2 - 6 6 5 2 6 6 0 - - 6 5 2 6 6 0 - - 6 5 2 6 6 0 - - 6 5 2 0 6 0 - 20.0 20.0 10.0 20.0 20.0 20.0 12.0 90.0 78.0 78.0 10.0% 75.0% 65.0% 65.0% 3.0 3.0 3.0 2.0 0.0 0.0 0.0 2.0 0.0 5.0 5.0	M M M M M 78 2000 2235 58 137 78 2000 2235 58 137 pm+pt NA NA Perm Prot 5 2 6 4 2 - 6 4 2 2 6 4 2 - 6 4 2 - 6 4 2 - 6 4 2 - 6 4 2 - 6 4 2 - 6 4 2 2 6 6 50 5.0 5.0 5.0 10.0 20.0 20.0 20.0 11.0 20.0 20.0 20.0 10.0% 75.0% 65.0% 65.0% 3.0 3.0 3.0 3.0 3.0 3.0 2.0

Splits and Phases: 2: SH 7 (Baseline Rd) & Airport Road

ø₂ (R) ♥	▲ Ø4	
90 s	30 s	
▶ Ø5 ♥ ∞6 (R)		
12 s 78 s		

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Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	٦	††	††	1	ሻ	1
Traffic Volume (veh/h)	78	2000	2235	58	137	171
Future Volume (veh/h)	78	2000	2235	58	137	171
Initial Q (Qb), veh	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00	-	-	1.00	1.00	1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No	No		No	
Adj Sat Flow, veh/h/ln	1870	1870	1870	1870	1870	1870
Adj Flow Rate, veh/h	85	2174	2429	63	149	186
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Percent Heavy Veh, %	2	2	2	2	2	2
Cap, veh/h	137	2775	2488	1110	257	242
Arrive On Green	0.04	0.78	0.70	0.70	0.14	0.15
Sat Flow, veh/h	1781	3647	3647	1585	1781	1585
Grp Volume(v), veh/h	85	2174	2429	63	149	186
Grp Sat Flow(s), veh/h/ln	1781	1777	1777	1585	1781	1585
Q Serve(\underline{g}), s	1.5	41.4	77.7	1.5	9.4	13.5
			77.7	1.5 1.5		13.5
Cycle Q Clear(g_c), s	1.5	41.4	11.1		9.4	
Prop In Lane	1.00	0775	2400	1.00	1.00	1.00
Lane Grp Cap(c), veh/h	137	2775	2488	1110	257	242
V/C Ratio(X)	0.62	0.78	0.98	0.06	0.58	0.77
Avail Cap(c_a), veh/h	171	2775	2488	1110	386	357
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	1.00	1.00	1.00	1.00
Uniform Delay (d), s/veh	34.3	7.4	17.1	5.6	48.0	48.8
Incr Delay (d2), s/veh	4.5	2.3	13.3	0.1	2.1	5.9
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	1.9	10.1	27.6	0.4	4.4	11.8
Unsig. Movement Delay, s/veh	1					
LnGrp Delay(d),s/veh	38.9	9.7	30.3	5.7	50.0	54.7
LnGrp LOS	D	А	С	А	D	D
Approach Vol, veh/h		2259	2492		335	
Approach Delay, s/veh		10.8	29.7		52.6	
Approach LOS		B	C		D	
			Ŭ			
Timer - Assigned Phs		2		4	5	6
Phs Duration (G+Y+Rc), s		98.7		21.3	9.7	89.0
Change Period (Y+Rc), s		5.0		5.0	5.0	5.0
Max Green Setting (Gmax), s		85.0		25.0	7.0	73.0
Max Q Clear Time (g_c+I1), s		43.4		15.5	3.5	79.7
Green Ext Time (p_c), s		25.4		0.8	0.0	0.0
Intersection Summary						
			22.8			
HCM 6th Ctrl Delay						
HCM 6th LOS			С			

PROJECT SHEET BASE DESIGN STANDARDS

Complete one Project Sheet for each project that includes Stormwater Quality Control Measures. Please email <u>stormwater@erieco.gov</u> with any questions. This document acceptance shall not be construed to relieve any requirement to conform to the Standards and Specifications not specifically addressed in this form. The engineering design and concept remains the responsibility of the professional engineer.

SITE INFORMATION

Erie Village Fifth Filing Replat B		
on: C.W. Bixler Boulevard and E. County Line Road	1	
itted Date: 10/08/2021 Submitted By:		
t Email: mcoonce@porchfronthomes.com Applicant Phone: 303.442.8453		
anization: Porchfront Homes at Erie Village, LLC		
rbed: 19.79		
xisting Impervious: 2.0% New Net Impervious: 75%		
	Reviewed By:	
Requirements		
Design Details are included for all Control Measures (CM)		
List or include a description of any Source CMs (i.e. preventing pollutants from contacting		
stormwater) or other non-structural CMs:		
S-1 Covering Outdoor Storage and Handling Areas		
S-2 Spill Prevention, Containment and Control		
S-5 Good Housekeeping		
S-6 Preventative Maintenance		
S-7 Vehicle Maintenance, Fueling and Storage		
S-11 Street Sweeping and Cleaning		
S-12 Storm Sewer System Cleaning		
Does project overlap multiple MS4 Jurisdictions	Yes No	
If project overlaps jurisdictions, provide written agreement designating responsibility for CM		
requirements, review, inspections		
	on: C.W. Bixler Boulevard and E. County Line Road te: 10/08/2021 ill: mcoonce@porchfronthomes.com anization: Porchfront Homes at Erie Village, LLC rbed: 19.79 vious: 2.0% Requirements Design Details are included for all Control Measu List or include a description of any Source CMs (i stormwater) or other non-structural CMs: • S-1 Covering Outdoor Storage and Hand • S-2 Spill Prevention, Containment and C • S-5 Good Housekeeping • S-6 Preventative Maintenance • S-7 Vehicle Maintenance, Fueling and S • S-11 Street Sweeping and Cleaning • S-12 Storm Sewer System Cleaning • Does project overlap multiple MS4 Jurisdictions If project overlaps jurisdictions, provide written	

DESIGN STANDARDS

Design Standards may be used in combination, as necessary, to meet the requirements. Additional design methods may be considered if they comply with the MS4 Permit. Evaluation of suitability of Stormwater Quality Control Measures (CMs) is based on pollutant removal, flood attenuation and long-term maintenance. CMs must be designed in accordance with the most current version of <u>USDCM vol. 3</u>, <u>Chapter 4 "Treatment BMPs"</u> and the Town of Erie's Standards and Specifications. CMs must also meet the specific requirements for each Design Standard used. Design Standard requirements can be found on the MS4 general permit here: <u>COR90000</u>

- 1. Indicate below, which Design Standards will be used for the project, and
- 2. Complete a separate, corresponding Design Standards checklist for each CM (e.g., WQCV, etc.)

Design Standard	# CMs	Location/Identifying information
WQCV	1	Pond A – North of C. W. Bixler Boulevard
Pollutant Removal		
Runoff Reduction		
Regional WQCV Control Measure		
Regional WQCV Facility		

CHECKLIST WQCV Standard

WQCV STANDARD Criteria

Control measure(s) must be designed to provide treatment and/or infiltration of the Water Quality Capture Volume (WQCV) for 100% of the site.

Complete checklist if using the WQCV Standard to meet Design Standard requirements.

Project Name: Erie Village Fifth Filing Replat B		
Preparer	Requirements	
Х	Control measure(s) provide treatment and/or infiltration of the WQCV for 100% of the site	
Х	% of site treated: 100%	
Х	CM type: Extended Detention Basin	CM ID/location: Pond A – North of C. W.
		Bixler Boulevard
Х	See Drainage Report section: See Section IV.B.2	

If less than 100% of the site is treated, complete the following:

Preparer	Requirements	
N/A	% of site not treated by control measures (not to exceed 20% or 1 acre):	
	%	size (acres)
N/A	Provide explanation that the excluded area is	impractical to treat:
N/A	Provide explanation that another CM is not p	racticable for the untreated area:

Endorsement Attached to Policy No. OX25152287.1185881 Our Order No. 25152287

Issued By Old Republic National Title Insurance Company

The Company herey insures the insured against loss or damage arising from the effect of any instrument recorded in the public records affecting the title to the land or the lien of the insured mortgage subsequent to the effective date of the policy or of the date of the last previous search of said records, and prior to date of this endorsement, except:

QUIT CLAIM DEED RECORDED APRIL 2, 2019 AT RECEPTION NO. <u>4477982</u>. EASEMENT DEED AND AGREEMENT RECORDED APRIL 24, 2019 AT RECEPTION NO. <u>4483705</u>. STATEMENT OF AUTHORITY FOR REAL INVESTMENTS LLC RECORDED JUNE 14, 2019 AT RECEPTION NO. <u>4497571</u>.

NOTICE FOR REQUEST OF SURFACE DEVELOPMENT RECORDED JUNE 19, 2019 AT RECEPTION NO. <u>4498658</u> AND <u>4498659</u>, AMENDMENTS THERETO RECORDED JULY 17, 2019 AT RECEPTION NO. <u>4506261</u> AND <u>4506262</u>.

This endorsement does no afford coverage as to taxes, bonds or assessments, if any, except to the extent expressly stated.

Dated: NOVEMBER 07, 2019

This endorsement is issued as part of the Policy. Except as it expressly states, it does not (i) modify any of the terms and provisions of the Policy, (ii) modify any prior endorsements, (iii) extend the Date of Policy, or (iv) increase the Amount of Insurance. To the extent a provision of the Policy or a previous endorsement is inconsistent with an express provision of this endorsement, this endorsement controls. Otherwise, this endorsement is subject to all of the terms and provisions of the Policy and of any prior endorsements.

Old Republic National Title Insurance Company

By: LAND TITLE GUARANTEE COMPANY

By: CBRants



State Documentary Fee Date: March 27, 2019 \$45.00

Warranty Deed

(Pursuant to 38-30-113 C.R.S.)

THIS DEED, made on March 27th, 2019 by SHERIDAN SCHOFIELD AND PEGGY J. SCHOFIELD Grantor(s), of the County of Douglas and State of Colorado for the consideration of (\$450,000.00) ***Four Hundred Fifty Thousand and 00/100*** dollars in hand paid, hereby sells and conveys to DAVID S. NASSAR Grantee(s), whose street address is 395 AIRPORT DRIVE, ERIE, CO 80516, County of Weld, and State of Colorado, the following real property in the County of Weld, and State of Colorado, to wit:

TRACT E-2, ERIE AIR PARK TRACT E MINOR SUBDIVISION, COUNTY OF WELD, STATE OF COLORADO

also known by street and number as: VACANT, ERIE, CO 80516

with all its appurtenances and warrants the title to the same, subject to general taxes for the year 2019 and those specific Exceptions described by reference to recorded documents as reflected in the Title Documents accepted by Grantee(s) in accordance with Record Title Matters (Section 8.2) of the Contract to Buy and Sell Real Estate relating to the above described real property; distribution utility easements, (including cable TV); those specifically described rights of third parties not shown by the public records of which Grantee(s) has actual knowledge and which were accepted by Grantee(s) in accordance with Off-Record Title Matters (Section 8.3) and Current Survey Review (Section 9) of the Contract to Buy and Sell Real Estate relating to the above described real property; inclusions of the Property within any special tax district; Any special assessment if the improvements were not installed as of the date of Buyer's signature on the Contract to Buy and Sell Real Estate Closing; and other **NONE**

SHERIDAN SCHOFIEL J. SCHOEIELD PEGGY State of Colorado))ss County of BOULDER)

NOTARY ID 19914007156 My Commission Expires May 24, 2019

The foregoing instrument was acknowledged before me on this day of March 27th, 2019 by SHERIDAN SCHOFIELD AND PEGGY J. SCHOFIELD

111 Kork Witness my hand and official seal My Commission expires: Notary Public JACQUELINE BECK NOTARY PUBLIC **FATE OF COLORADO**

4477980 04/02/2019 08:10 AM Total Pages: 1 Rec Fee: \$13.00 Doc Fee: \$45.00 Carly Koppes - Clerk and Recorder, Weld County, CO

When recorded return to: DAVIE

DAVID S. NASSAR 395 AIRPORT DRIVE, ERIE, CO 80516



4477982 04/02/2019 08:10 AM Total Pages: 1 Rec Fee: \$13.00 Carly Koppes - Clerk and Recorder, Weld County, CO

State Documentary Fee Date: 03/27/2019 \$0.00 No Doc Fee Required

Quit Claim Deed

(Pursuant to 38-30-116 C.R.S.)

THIS DEED, made on March 27, 2019 by DAVID S. NASSAR Grantor(s) of the County of BOULDER and State of COLORADO for the consideration of *** Ten Dollars and Other Good and Valuable Consideration *** dollars in hand paid, hereby sells and quitclaims to REAL INVESTMENTS LLC, A COLORADO LIMITED LIABILITY COMPANY Grantee(s), as Entity whose street address is 395 AIRPORT DRIVE, ERIE, CO 80516 County of Weld, State of Colorado, the following real property in the County of Weld and State of Colorado, to wit:

TRACT E-2, ERIE AIR PARK TRACT E MINOR SUBDIVISION, COUNTY OF WELD, STATE OF COLORADO

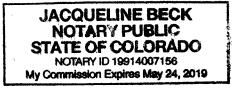
also known by street and number as VACANT, ERIE, CO 80516 with all its appurtenances.

DAVID S. NASSAT DAVID S. MASSAR State of)ss

County of

The foregoing instrument was acknowledged before me on this day of March 27, 2019 by DAVID S. NASSAR

Notary Public My Commission xńire



When recorded return to:

VACANT, ERIE, CO 80516







Land Title Guarantee Company Customer Distribution

PREVENT FRAUD - Please remember to call a member of our closing team when *initiating a wire transfer or providing wiring instructions.*

Order Number: **FCC25152287-10**

Property Address: VACANT, ERIE, CO 80516

PLEASE CONTACT YOUR CLOSER OR CLOSER'S ASSISTANT FOR WIRE TRANSFER INSTRUCTIONS

For Closing Assistance Jackie Beck 2595 CANYON BLVD #340 BOULDER, CO 80302 (720) 406-2087 (Work) (303) 393-4851 (Work Fax) jbeck@ltgc.com Company License: CO44565

Buyer/Borrower

DAVID NASSAR 395 AIRPORT DRIVE ERIE, CO 80516 david@marketwise.com Delivered via: Electronic Mail

Closer's Assistant

Alaina Greenhouse 2595 CANYON BLVD #340 BOULDER, CO 80302 (720) 406-2097 (Work) (303) 393-3976 (Work Fax) agreenhouse@ltgc.com Contact License: CO545891 Company License: CO44565

For Title Assistance

Ft. Collins Customer Care 772 WHALERS WAY #100 FORT COLLINS, CO 80525 (970) 282-3649 (Work) (970) 282-3652 (Work Fax) customercare@ltgc.com

Date: 03/29/2019

Seller/Owner

SHERIDAN SCHOFIELD AND PEGGY SCHOFIELD 44 BANTALA PLACE CASTLE ROCK, CO 80108 (303) 663-3963 (Work) jschofld@aol.com Delivered via: Electronic Mail



Land Title Guarantee Company Estimate of Title Fees

Order Number:	FCC25152287-10	Date: 03/29/2019
Property Address:	VACANT, ERIE, CO 80516	
Parties:	DAVID S. NASSAR	
	SHERIDAN SCHOFIELD AND PEGGY J. SCHOFIELD <u>AND ERIE ST</u> COLORADO LIMITED LIABILITY COMPANY AS THEIR INTEREST I	· · · ·

Visit Land Title's Website at <u>www.ltgc.com</u> for directions to any of our offices.

Estimate of Title insurance Fees	
"ALTA" Owner's Policy 06-17-06 Builder/Developer Rate	<u>\$706.00</u>
Deletion of Standard Exception(s)	\$100.00
Tax Certificate	\$26.00
	Total <u>\$832.00</u>
If Land Title Guarantee Company will be closing this transaction, the fees listed above will be collected at closing.	
Thank you for your order!	

Chain of Title Documents:

Weld county recorded 11/02/2001 under reception no. 2897454 Weld county recorded 01/27/1993 under reception no. 2319662

Plat Map(s):

Weld county recorded 03/22/2019 under reception no. 4475348 Weld county recorded 05/03/1978 under reception no. 1752380

Old Republic National Title Insurance Company

Schedule A

Order Number: FCC25152287-10

Property Address:

VACANT, ERIE, CO 80516

1. Effective Date:

03/21/2019 at 5:00 P.M.

2. Policy to be Issued and Proposed Insured:

"ALTA" Owner's Policy 06-17-06 Builder/Developer Rate Proposed Insured: DAVID S. NASSAR \$450,000.00

3. The estate or interest in the land described or referred to in this Commitment and covered herein is:

A Fee Simple

4. Title to the estate or interest covered herein is at the effective date hereof vested in:

SHERIDAN SCHOFIELD AND PEGGY J. SCHOFIELD <u>AND ERIE STORAGE, LLC, A COLORADO LIMITED</u> <u>LIABILITY COMPANY AS THEIR INTEREST MAY APPEAR</u>

5. The Land referred to in this Commitment is described as follows:

TRACT E-2, ERIE AIR PARK TRACT E MINOR SUBDIVISION, COUNTY OF WELD, STATE OF COLORADO

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Old Republic National Title Insurance Company

Schedule B-1

(Requirements)

Order Number: FCC25152287-10

The following are the requirements to be complied with:

Payment to or for the account of the grantors or mortgagors of the full consideration for the estate or interest to be insured.

Proper instrument(s) creating the estate or interest to be insured must be executed and duly filed for record, to-wit:

- 1. (THIS ITEM WAS INTENTIONALLY DELETED)
- 2. WARRANTY DEED FROM SHERIDAN SCHOFIELD AND PEGGY J. SCHOFIELD TO DAVID S. NASSAR CONVEYING SUBJECT PROPERTY.
- 3. PROVIDE LAND TITLE GUARANTEE COMPANY WITH A CURRENT IMPROVEMENT SURVEY PLAT OR AN ALTA SURVEY OF SUBJECT PROPERTY. UPON REVIEW, ADDITIONAL REQUIREMENTS AND/OR EXCEPTIONS MAY BE NECESSARY.

LAND TITLE IS NOT RESPONSIBLE FOR ORDERING SAID IMPROVEMENT SURVEY PLAT OR AN ALTA SURVEY.

SAID SURVEY MUST BE CERTIFIED TO LAND TITLE GUARANTEE COMPANY AND OLD REPUBLIC NATIONAL TITLE INSURANCE COMPANY.

- 4. (THIS ITEM WAS INTENTIONALLY DELETED)
- 5. <u>GOOD AND SUFFICIENT DEED FROM ERIE STORAGE, LLC, TO DAVID S. NASSAR CONVEYING SUBJECT</u> <u>PROPERTY.</u>
- 6. WRITTEN CONFIRMATION THAT THE INFORMATION CONTAINED IN STATEMENT OF AUTHORITY FOR ERIE STORAGE, LLC, A COLORADO LIMITED LIABILITY COMPANY RECORDED MARCH 30, 2006 AT RECEPTION NO. 3374676 IS CURRENT.

NOTE: SAID INSTRUMENT DISCLOSES SAUNDERS BUCKSTEIN AS THE MEMBER AUTHORIZED TO EXECUTE INSTRUMENTS CONVEYING, ENCUMBERING OR OTHERWISE AFFECTING TITLE TO REAL PROPERTY ON BEHALF OF SAID ENTITY. IF THIS INFORMATION IS NOT ACCURATE, A CURRENT STATEMENT OF AUTHORITY MUST BE RECORDED.

Old Republic National Title Insurance Company

Schedule B-1

(Requirements)

Order Number: FCC25152287-10

The following are the requirements to be complied with:

NOTE: ITEMS 1-3 OF THE STANDARD EXCEPTIONS WILL BE DELETED UPON RECEIPT OF AN APPROVED SURVEY. MATTERS DISCLOSED BY SAID SURVEY MAY BE ADDED TO SCHEDULE B-2 HEREOF.

UPON THE APPROVAL OF THE COMPANY AND THE RECEIPT OF A NOTARIZED FINAL LIEN AFFIDAVIT, ITEM NO. 4 OF THE STANDARD EXCEPTIONS ON THE OWNER'S POLICY, WILL BE AMENDED AS FOLLOWS:

ITEM NO. 4 OF THE STANDARD EXCEPTIONS IS DELETED AS TO ANY LIENS OR FUTURE LIENS RESULTING FROM WORK OR MATERIAL FURNISHED AT THE SPECIFIC, DIRECT REQUEST, AND WITH THE ACTUAL KNOWLEDGE OF SHERIDAN SCHOFIELD AND <u>PEGGY J. SCHOFIELD AND ERIE STORAGE,</u> <u>LLC, A COLORADO LIMITED LIABILITY COMPANY AS THEIR INTEREST MAY APPEAR.</u> <u>OLD</u> REPUBLIC NATIONAL TITLE INSURANCE COMPANY SHALL HAVE NO LIABILITY FOR ANY LIENS ARISING FROM WORK OR MATERIAL FURNISHED AT THE SPECIFIC, DIRECT REQUEST, AND WITH THE ACTUAL KNOWLEDGE OF DAVID S. NASSAR.

NOTE: ITEM 5 OF THE STANDARD EXCEPTIONS WILL BE DELETED IF LAND TITLE GUARANTEE COMPANY CONDUCTS THE CLOSING OF THE CONTEMPLATED TRANSACTION(S) AND RECORDS THE DOCUMENTS IN CONNECTION THEREWITH.

NOTE: UPON PROOF OF PAYMENT OF 2016 TAXES, ITEM 6 WILL BE AMENDED TO READ:

TAXES AND ASSESSMENTS FOR THE YEAR 2017 AND SUBSEQUENT YEARS.

Old Republic National Title Insurance Company

Schedule B-2

(Exceptions)

Order Number: FCC25152287-10

The policy or policies to be issued will contain exceptions to the following unless the same are disposed of to the satisfaction of the Company:

- 1. Any facts, rights, interests, or claims thereof, not shown by the Public Records but that could be ascertained by an inspection of the Land or that may be asserted by persons in possession of the Land.
- 2. Easements, liens or encumbrances, or claims thereof, not shown by the Public Records.
- 3. Any encroachment, encumbrance, violation, variation, or adverse circumstance affecting the Title that would be disclosed by an accurate and complete land survey of the Land and not shown by the Public Records.
- 4. Any lien, or right to a lien, for services, labor or material heretofore or hereafter furnished, imposed by law and not shown by the Public Records.
- 5. Defects, liens, encumbrances, adverse claims or other matters, if any, created, first appearing in the public records or attaching subsequent to the effective date hereof but prior to the date of the proposed insured acquires of record for value the estate or interest or mortgage thereon covered by this Commitment.
- 6. (a) Taxes or assessments that are not shown as existing liens by the records of any taxing authority that levies taxes or assessments on real property or by the Public Records; (b) proceedings by a public agency that may result in taxes or assessments, or notices of such proceedings, whether or not shown by the records of such agency or by the Public Records.
- 7. (a) Unpatented mining claims; (b) reservations or exceptions in patents or in Acts authorizing the issuance thereof; (c) water rights, claims or title to water.
- 8. ALL MINERALS ON AND UNDER THE SUBJECT PROPERTY, INCLUDING BUT NOT LIMITED TO COAL, OIL AND GAS AS WELL AS THE RIGHT OF INGRESS AND EGRESS UPON AND ACROSS SAID LANDS FOR THE PURPOSE OF PROSPECTING FOR, MINING, TREATING, PROCESSING, TAKING AND TRANSPORTING ANY AND ALL MINERALS AND FOR THE CONSTRUCTION OF PLANTS, HOUSES, BUILDINGS, OFFICES, DUMPS, ROADS, POWER LINES, PIPE LINES AND OTHER STRUCTURES INCIDENTAL TO SUCH OPERATIONS, AS RESERVED BY THE ROCKY MOUNTAIN FUEL COMPANY IN WARRANTY DEED RECORDED AUGUST 27, 1946 IN BOOK 1186 AT PAGE <u>313</u>, AND ANY INTEREST THEREIN OR RIGHTS THEREUNDER.
- 9. CONDITION THAT THE OWNER OF THE SUBJECT PROPERTY, HIS SUCCESSORS AND ASSIGNS, FOREVER WAIVES AND RELEASES ANY AND ALL CLAIM OR CLAIMS HE MIGHT HAVE OR ACQUIRE IN THE FUTURE ARISING OUT OF ANY INJURY FOR DAMAGES, AS WELL AS ANY RIGHT TO ENJOIN THE ROCKY MOUNTAIN FUEL COMPANY, ITS SUCCESSORS IN INTEREST AND ASSIGNS, BECAUSE OF ANY INJURY OR THREATENED INJURY CAUSED OR OCCASIONED AT ANY TIME BY SUBSIDENCE OR OTHER DISTURBANCES OF THE SURFACE OF THE SUBJECT PROPERTY OCCASIONED BY ANY MINING OPERATIONS OR ACTIVITIES INCIDENT THERETO INVOLVING THE MINERALS THEREON OR THEREUNDER, AS IMPOSED IN WARRANTY DEED FROM THE ROCKY MOUNTAIN FUEL COMPANY RECORDED AUGUST 27, 1946, IN BOOK 1186 AT PAGE <u>313</u>.
- 10. RIGHT OF WAY FOR ELECTRIC TRANSMISSION LINE PURPOSES AS CONTAINED IN INSTRUMENT RECORDED JULY 21, 1954 IN BOOK 1395 AT PAGE <u>571</u>.
- 11. RIGHT OF WAY EASEMENT AS GRANTED TO PUBLIC SERVICE COMPANY OF COLORADO IN INSTRUMENT RECORDED JULY 21, 1954, IN BOOK 1395 AT PAGE <u>573</u>.

ALTA COMMITMENT

Old Republic National Title Insurance Company

Schedule B-2

(Exceptions)

Order Number: FCC25152287-10

The policy or policies to be issued will contain exceptions to the following unless the same are disposed of to the satisfaction of the Company:

- 12. RIGHT OF WAY EASEMENT AS GRANTED TO THE MOUNTAIN STATES TELEPHONE AND TELEGRAPH COMPANY IN INSTRUMENT RECORDED APRIL 20, 1957, IN BOOK 1475 AT PAGE <u>553</u>.
- 13. TERMS, CONDITIONS AND PROVISIONS OF EASEMENT RECORDED OCTOBER 31, 1961 IN BOOK 1598 AT PAGE <u>165</u>.
- 14. TERMS, CONDITIONS AND PROVISIONS OF ANNEXATION AGREEMENT RECORDED DECEMBER 28, 1977 UNDER RECEPTION NO. <u>1739852</u>.
- 15. TERMS, CONDITIONS AND PROVISIONS OF ERIE AIR PARK SUBDIVISION AGREEMENT RECORDED MAY 03, 1978 UNDER RECEPTION NO. <u>1752378</u>.
- 16. TERMS, CONDITIONS AND PROVISIONS OF AVIATION EASEMENT AND AGREEMENT RECORDED MAY 11, 1978 UNDER RECEPTION NO. <u>1753139</u>.
- 17. TERMS, CONDITIONS AND PROVISIONS OF EASEMENT FOR RUNWAY LIGHT INSTALLATION AND MAINTENANCE, DRAINAGE AND SNOW REMOVAL AGREEMENT RECORDED MAY 11, 1978 UNDER RECEPTION NO. <u>1753142</u>.
- 18. TERMS, CONDITIONS AND PROVISIONS OF SOLAR EASEMENT AND AGREEMENT RECORDED MAY 11, 1978 UNDER RECEPTION NO. <u>1753143</u>.
- 19. EASEMENTS, CONDITIONS, COVENANTS, RESTRICTIONS, RESERVATIONS AND NOTES ON THE PLAT OF ERIE AIR PARK SUBDIVISION RECORDED MAY 03, 1978 UNDER RECEPTION NO. <u>1752380</u>.
- 20. THE EFFECT, IF ANY, OF LETTER RECORDED AUGUST 12, 1982 UNDER RECEPTION NO. 1900277.
- 21. TERMS, CONDITIONS AND PROVISIONS OF LEASE RECORDED SEPTEMBER 29, 1982 AT RECEPTION NO. <u>1905076</u>.

NOTE: EXTENSION OF THE ABOVE LEASE AS CLAIMED BY AFFIDAVIT OF PRODUCTION WAS RECORDED OCTOBER 12, 1984 UNDER RECEPTION NO. <u>1984915</u>.

- 22. RESTRICTIVE COVENANTS, WHICH DO NOT CONTAIN A FORFEITURE OR REVERTER CLAUSE, AS CONTAINED IN INSTRUMENT RECORDED MAY 11, 1978, UNDER RECEPTION NO. <u>1753140</u> AND AS AMENDED IN INSTRUMENT RECORDED SEPTEMBER 30, 1993, UNDER RECEPTION NO. <u>2352630</u> IN BOOK 1404 AND AS AMENDED DECEMBER 27, 1993 AT RECEPTION NO. <u>2365912</u> AND AS AMENDED IN INSTRUMENT RECORDED DECEMBER 21, 1995, UNDER RECEPTION NO. <u>2468577</u> IN BOOK 1524 AND AMENDED OCTOBER 22, 2002 AT RECEPTION NO. <u>2998230</u>
- 23. TERMS, CONDITIONS AND PROVISIONS OF AGREEMENT RECORDED APRIL 28, 1986 AT RECEPTION NO. 2051362.
- 24. TERMS, CONDITIONS AND PROVISIONS OF ASSESSMENT RECORDED NOVEMBER 21, 1990 AT RECEPTION NO. 2233799.
- 25. THE TERMS AND PROVISIONS OF ORDINANCE NOS. 409 AND 411, RECORDED FEBRUARY 4, 1991 UNDER RECEPTION NO. <u>2240420</u> AND FEBRUARY 25, 1991 UNDER RECEPTION NO. <u>2242128</u>
- 26. TERMS, CONDITIONS AND PROVISIONS OF AGREEMENT RECORDED MARCH 05, 1991 AT RECEPTION NO. 2243072.

ALTA COMMITMENT

Old Republic National Title Insurance Company

Schedule B-2

(Exceptions)

Order Number: FCC25152287-10

The policy or policies to be issued will contain exceptions to the following unless the same are disposed of to the satisfaction of the Company:

- 27. ORDER OF INCLUSION FOR WELD COUNTY PORTION OF THE TOWN OF ERIE INTO THE NORTHERN COLORADO WATER CONSERVANCY DISTRICT RECORDED FEBRUARY 6, 1992 UNDER RECEPTION NO. 2277399.
- 28. TERMS, AGREEMENTS, PROVISIONS, CONDITIONS AND OBLIGATIONS, AS CONTAINED IN AGREEMENT REGARDING INSTALLATION OF SANITARY SEWER LINES BY AND BETWEEN ERIE WATER AND SANITATION DISTRICT AND ROBERT LEE ROCK RECORDED AUGUST 13, 1992 UNDER RECEPTION NO. 2299958 IN BOOK 1347
- 29. RESTRICTIVE COVENANTS, WHICH DO NOT CONTAIN A FORFEITURE OR REVERTER CLAUSE, AS CONTAINED IN INSTRUMENT RECORDED DECEMBER 27, 1993, UNDER RECEPTION NO. <u>2365912</u>.
- 30. TERMS, CONDITIONS AND PROVISIONS OF ORDER RECORDED APRIL 18, 1995 AT RECEPTION NO. 2434694.
- 31. TERMS, CONDITIONS AND PROVISIONS OF ORDER RECORDED APRIL 27, 1995 AT RECEPTION NO. 2435904.
- 32. MATTERS AS SET FORTH ON SURVEY RECORDED JUNE 28, 2002 AT RECEPTION NO. 2969635
- 33. TERMS, CONDITIONS AND PROVISIONS OF OPTION RECORDED MARCH 20, 2006 AT RECEPTION NO. 3371704.
- 34. TERMS, CONDITIONS AND PROVISIONS OF TAXIWAY EASEMENT DEED AND AGREEMENT RECORDED DECEMBER 15, 2006 AT RECEPTION NO. <u>3442230</u>.
- 35. EXISTING LEASES OR TENANCIES, IF ANY
- 36. ANY LOSS OR DAMAGE WHICH THE PROPOSED INSUREDS MAY INCUR BY REASON OF THE FAILURE TO COMPLY WITH THE LAWS AND REGULATIONS OF ANY STATE, COUNTY OR OTHER AUTHORITY RELATING TO THE SUBDIVISION OF THE LAND TO BE INSURED.
- 37. ANY FACTS, RIGHTS, INTERESTS OR CLAIMS WHICH MAY EXIST OR ARISE BY REASON OF THE FOLLOWING FACTS SHOWN ON ALTA/NSPS LAND TITLE SURVEY CERTIFIED _____ PREPARED BY SCOTT, COX & ASSOCIATES, INC., JOB #17150A:
 A. STORM DRAINAGE LINES AND MANHOLES
 B. WATER LINE SAID DOCUMENT STORED AS OUR ESI
- 38. EASEMENTS, CONDITIONS, COVENANTS, RESTRICTIONS, RESERVATIONS AND NOTES ON THE PLAT OF ERIE AIR PARK TRACT E MINOR SUBDIVISION RECORDED <u>MARCH 22, 2019 UNDER</u> RECEPTION NO. <u>4475348.</u>



LAND TITLE GUARANTEE COMPANY DISCLOSURE STATEMENTS

Note: Pursuant to CRS 10-11-122, notice is hereby given that:

- (A) The Subject real property may be located in a special taxing district.
- (B) A certificate of taxes due listing each taxing jurisdiction will be obtained from the county treasurer of the county in which the real property is located or that county treasurer's authorized agent unless the proposed insured provides written instructions to the contrary. (for an Owner's Policy of Title Insurance pertaining to a sale of residential real property).
- (C) The information regarding special districts and the boundaries of such districts may be obtained from the Board of County Commissioners, the County Clerk and Recorder, or the County Assessor.

Note: Effective September 1, 1997, CRS 30-10-406 requires that all documents received for recording or filing in the clerk and recorder's office shall contain a top margin of at least one inch and a left, right and bottom margin of at least one half of an inch. The clerk and recorder may refuse to record or file any document that does not conform, except that, the requirement for the top margin shall not apply to documents using forms on which space is provided for recording or filing information at the top margin of the document.

Note: Colorado Division of Insurance Regulations 8-1-2 requires that "Every title entity shall be responsible for all matters which appear of record prior to the time of recording whenever the title entity conducts the closing and is responsible for recording or filing of legal documents resulting from the transaction which was closed". Provided that Land Title Guarantee Company conducts the closing of the insured transaction and is responsible for recording the legal documents from the transaction, exception number 5 will not appear on the Owner's Title Policy and the Lenders Policy when issued.

Note: Affirmative mechanic's lien protection for the Owner may be available (typically by deletion of Exception no. 4 of Schedule B, Section 2 of the Commitment from the Owner's Policy to be issued) upon compliance with the following conditions:

- (A) The land described in Schedule A of this commitment must be a single family residence which includes a condominium or townhouse unit.
- (B) No labor or materials have been furnished by mechanics or material-men for purposes of construction on the land described in Schedule A of this Commitment within the past 6 months.
- (C) The Company must receive an appropriate affidavit indemnifying the Company against un-filed mechanic's and material-men's liens.
- (D) The Company must receive payment of the appropriate premium.
- (E) If there has been construction, improvements or major repairs undertaken on the property to be purchased within six months prior to the Date of Commitment, the requirements to obtain coverage for unrecorded liens will include: disclosure of certain construction information; financial information as to the seller, the builder and or the contractor; payment of the appropriate premium fully executed Indemnity Agreements satisfactory to the company, and, any additional requirements as may be necessary after an examination of the aforesaid information by the Company.

No coverage will be given under any circumstances for labor or material for which the insured has contracted for or agreed to pay.

Note: Pursuant to CRS 10-11-123, notice is hereby given:

This notice applies to owner's policy commitments disclosing that a mineral estate has been severed from the surface estate, in Schedule B-2.

- (A) That there is recorded evidence that a mineral estate has been severed, leased, or otherwise conveyed from the surface estate and that there is substantial likelihood that a third party holds some or all interest in oil, gas, other minerals, or geothermal energy in the property; and
- (B) That such mineral estate may include the right to enter and use the property without the surface owner's permission.

Note: Pursuant to CRS 10-1-128(6)(a), It is unlawful to knowingly provide false, incomplete, or misleading facts or information to an insurance company for the purpose of defrauding or attempting to defraud the company. Penalties may include imprisonment, fines, denial of insurance, and civil damages. Any insurance company or agent of an insurance company who knowingly provides false, incomplete, or misleading facts or information to a policyholder or claimant for the purpose of defrauding or attempting to defraud the policyholder or claimant with regard to a settlement or award payable from insurance proceeds shall be reported to the Colorado Division of Insurance within the Department of Regulatory Agencies.

Note: Pursuant to Colorado Division of Insurance Regulations 8-1-3, notice is hereby given of the availability of a closing protection letter for the lender, purchaser, lessee or seller in connection with this transaction.

JOINT NOTICE OF PRIVACY POLICY OF LAND TITLE GUARANTEE COMPANY, LAND TITLE GUARANTEE COMPANY OF SUMMIT COUNTY LAND TITLE INSURANCE CORPORATION AND OLD REPUBLIC NATIONAL TITLE INSURANCE COMPANY

This Statement is provided to you as a customer of Land Title Guarantee Company as agent for Land Title Insurance Corporation and Old Republic National Title Insurance Company.

We want you to know that we recognize and respect your privacy expectations and the requirements of federal and state privacy laws. Information security is one of our highest priorities. We recognize that maintaining your trust and confidence is the bedrock of our business. We maintain and regularly review internal and external safeguards against unauthorized access to non-public personal information ("Personal Information").

In the course of our business, we may collect Personal Information about you from:

- applications or other forms we receive from you, including communications sent through TMX, our web-based transaction management system;
- your transactions with, or from the services being performed by us, our affiliates, or others;
- a consumer reporting agency, if such information is provided to us in connection with your transaction;

and

and Title

Since 1967

• The public records maintained by governmental entities that we either obtain directly from those entities, or from our affiliates and non-affiliates.

Our policies regarding the protection of the confidentiality and security of your Personal Information are as follows:

- We restrict access to all Personal Information about you to those employees who need to know that information in order to provide products and services to you.
- We maintain physical, electronic and procedural safeguards that comply with federal standards to protect your Personal Information from unauthorized access or intrusion.
- Employees who violate our strict policies and procedures regarding privacy are subject to disciplinary action.
- We regularly assess security standards and procedures to protect against unauthorized access to Personal Information.

WE DO NOT DISCLOSE ANY PERSONAL INFORMATION ABOUT YOU WITH ANYONE FOR ANY PURPOSE THAT IS NOT PERMITTED BY LAW.

Consistent with applicable privacy laws, there are some situations in which Personal Information may be disclosed. We may disclose your Personal Information when you direct or give us permission; when we are required by law to do so, for example, if we are served a subpoena; or when we suspect fraudulent or criminal activities. We also may disclose your Personal Information when otherwise permitted by applicable privacy laws such as, for example, when disclosure is needed to enforce our rights arising out of any agreement, transaction or relationship with you.

Our policy regarding dispute resolution is as follows: Any controversy or claim arising out of or relating to our privacy policy, or the breach thereof, shall be settled by arbitration in accordance with the rules of the American Arbitration Association, and judgment upon the award rendered by the arbitrator(s) may be entered in any court having jurisdiction thereof.



Commitment to Insure ALTA Commitment - 2006 Rev.

OLD REPUBLIC NATIONAL TITLE INSURANCE COMPANY, a Minnesota corporation, (Company), for a valuable consideration, commits to issue its policy or policies of title insurance, as identified in Schedule A, in favor of the Proposed Insured named in Schedule A, as owner or mortgagee of the estate or interest in the land described or referred to in Schedule A, upon payment of the premiums and charges and compliance with the requirements; all subject to the provisions of Schedule A and B and to the Conditions of this Commitment.

This Commitment shall be effective only when the identity of the Proposed Insured and the amount of the policy or policies committed for have been inserted in Schedule A by the Company. All liability and obligation under this commitment shall cease and terminate six months after the Effective Date or when the policy or policies committed for shall issue, whichever first occurs, provided that the failure to issue such policy or policies is not the fault of the Company.

Conditions and Stipulations

- 1. The term "mortgage", when used herein, shall include deed of trust, trust deed, or other security instrument.
- 2. If the proposed Insured has or acquires actual knowledge of any defect, lien, encumbrance, adverse claim or other matter affecting the estate or interest or mortgage thereon covered by this Commitment other than those shown in Schedule B hereof, and shall fail to disclose such knowledge to Company in writing, the Company shall be relieved from liability for any loss or damage resulting from any act of reliance hereon to the extent the Company is prejudiced by failure to so disclose such knowledge. If the proposed Insured shall disclose such knowledge to the Company, or if the Company otherwise acquires actual knowledge of any such defect, lien, encumbrance, adverse claim or other matter, the Company at its option may amend Schedule B of this Commitment accordingly, but such amendment shall not relieve the Company from liability previously incurred pursuant to paragraph 3 of these Conditions and Stipulations.
- 3. Liability of the Company under this Commitment shall be only to the named proposed Insured and such parties included under the definition of Insured in the form of policy or policies committed for and only for actual loss incurred in reliance hereon in undertaking in good faith (a) to comply with the requirements hereof or (b) to eliminate exceptions shown in Schedule B, or (c) to acquire or create the estate or interest or mortgage thereon covered by this Commitment. In no event shall such liability exceed the amount stated in Schedule A for the policy or policies committed for and such liability is subject to the insuring provisions and the Conditions and Stipulations and the Exclusions from Coverage of the form of policy or policies committed for in favor of the proposed Insured which are hereby incorporated by reference and are made a part of this Commitment except as expressly modified herein.
- 4. This commitment is a contract to issue one or more title insurance policies and is not an abstract of title or a report of the condition of title. Any action or actions or rights of action that the proposed Insured may have or may bring against the Company arising out of the status of the title to the estate or interest or the status of the mortgage thereon covered by this Commitment must be based on and are subject to the provisions of this Commitment.
- 5. The policy to be issued contains an arbitration clause. All arbitrable matters when the Amount of Insurance is \$2,000,000 or less shall be arbitrated at the option of either the Company or the Insured as the exclusive remedy of the parties. You may review a copy of the arbitration rules at www.alta.org.

Standard Exceptions

In addition to the matters contained in the Conditions and Stipulations and Exclusions from Coverage above referred to, this Commitment is also subject to the following:

- 1. Rights or claims of parties in possession not shown by the Public records.
- 2. Easements, or claims of easements, not shown by the Public Records.
- 3. Discrepancies, conflicts in boundary lines, shortage in area, encroachments, and any facts which a correct survey or inspection of the Land would disclose and which are not shown by the Public Records.
- 4. Any lien, or right to a lien, for services, labor or material theretofore or hereafter furnished, imposed by law and not shown by the Public Records.
- 5. Defects, liens, encumbrances, adverse claims or other matters, if any, created, first appearing in the Public Records or attaching subsequent to the effective date hereof but prior to the date the proposed insured acquires of record for value the estate or interest or mortgage thereon covered by this Commitment.

IN WITNESS WHEREOF, Old Republic National Title Insurance Company has caused its corporate name and seal to be affixed by its duly authorized officers on the date shown in Schedule A to be valid when countersigned by a validating officer or other authorized signatory.

Issued by: Land Title Guarantee Company 3033 East First Avenue Suite 600 Denver, Colorado 80206 303-321-1880

President



Old Republic National Title Insurance Company, a Stock Company 400 Second Avenue South Minneapolis, Minnesota 55401 (612)371-1111

/ho.VALSUbery

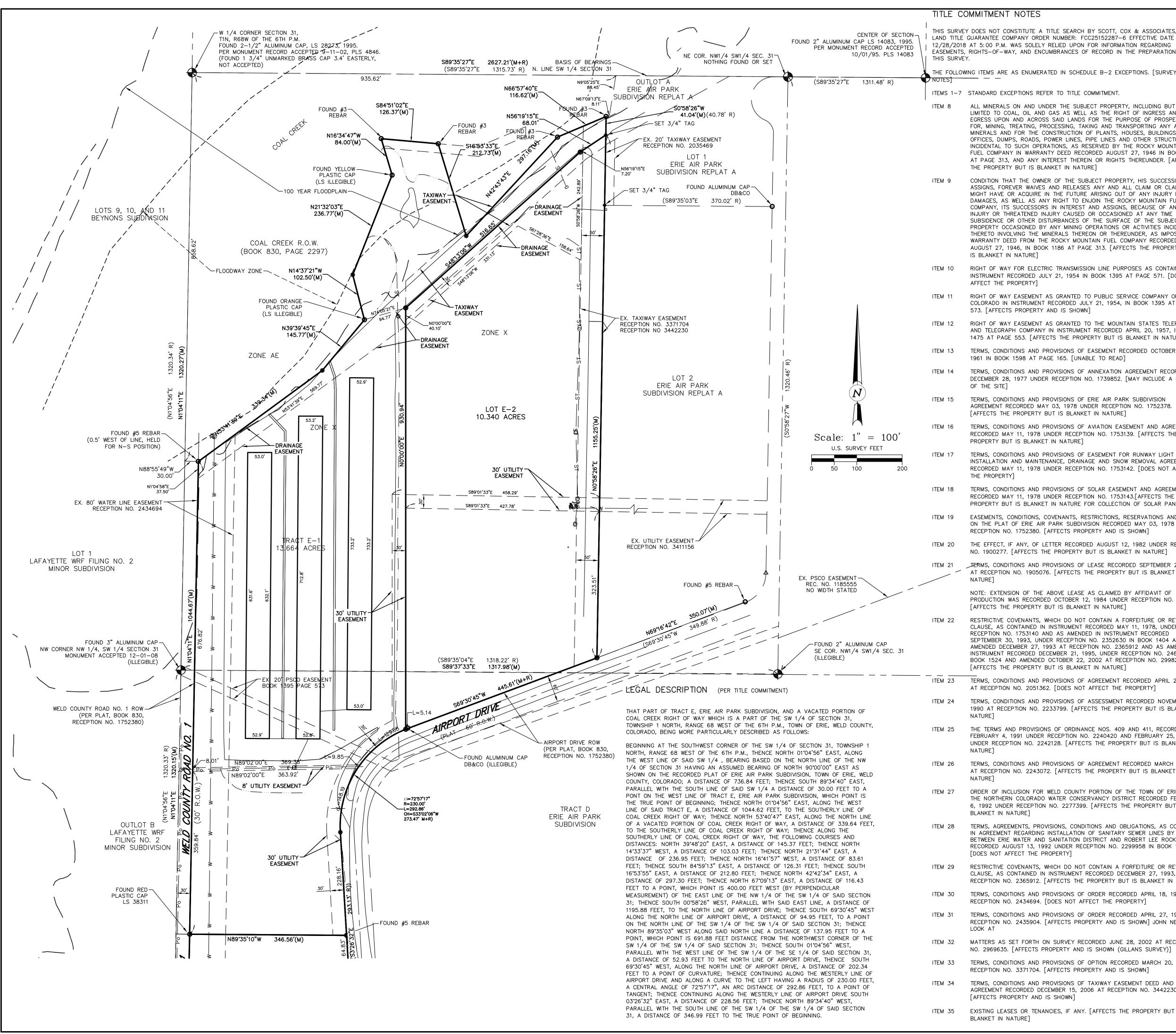
Mark Bilbrey, President

Rande Yeager, Secretary

AMERICAN LAND TITLE ASSOCIATION ALTA COMMITMENT FORM Adopted Copyright 2006-2019 American Land Title Association. All rights reserved.







THIS SURVEY DOES NOT CONSTITUTE A TITLE SEARCH BY SCOTT, COX & ASSOCIATES, INC. EASEMENTS, RIGHTS-OF-WAY, AND ENCUMBRANCES OF RECORD IN THE PREPARATION OF

THE FOLLOWING ITEMS ARE AS ENUMERATED IN SCHEDULE B-2 EXCEPTIONS. [SURVEYOR'S

ALL MINERALS ON AND UNDER THE SUBJECT PROPERTY, INCLUDING BUT NOT LIMITED TO COAL, OIL AND GAS AS WELL AS THE RIGHT OF INGRESS AND EGRESS UPON AND ACROSS SAID LANDS FOR THE PURPOSE OF PROSPECTING FOR, MINING, TREATING, PROCESSING, TAKING AND TRANSPORTING ANY AND ALL MINERALS AND FOR THE CONSTRUCTION OF PLANTS, HOUSES, BUILDINGS, OFFICES, DUMPS, ROADS, POWER LINES, PIPE LINES AND OTHER STRUCTURES INCIDENTAL TO SUCH OPERATIONS, AS RESERVED BY THE ROCKY MOUNTAIN FUEL COMPANY IN WARRANTY DEED RECORDED AUGUST 27, 1946 IN BOOK 1186 AT PAGE 313, AND ANY INTEREST THEREIN OR RIGHTS THEREUNDER. [AFFECTS

CONDITION THAT THE OWNER OF THE SUBJECT PROPERTY, HIS SUCCESSORS AND ASSIGNS, FOREVER WAIVES AND RELEASES ANY AND ALL CLAIM OR CLAIMS HE MIGHT HAVE OR ACQUIRE IN THE FUTURE ARISING OUT OF ANY INJURY FOR DAMAGES, AS WELL AS ANY RIGHT TO ENJOIN THE ROCKY MOUNTAIN FUEL COMPANY, ITS SUCCESSORS IN INTEREST AND ASSIGNS, BECAUSE OF ANY INJURY OR THREATENED INJURY CAUSED OR OCCASIONED AT ANY TIME BY SUBSIDENCE OR OTHER DISTURBANCES OF THE SURFACE OF THE SUBJECT PROPERTY OCCASIONED BY ANY MINING OPERATIONS OR ACTIVITIES INCIDENT THERETO INVOLVING THE MINERALS THEREON OR THEREUNDER, AS IMPOSED IN WARRANTY DEED FROM THE ROCKY MOUNTAIN FUEL COMPANY RECORDED AUGUST 27, 1946, IN BOOK 1186 AT PAGE 313. [AFFECTS THE PROPERTY BUT

ITEM 10 RIGHT OF WAY FOR ELECTRIC TRANSMISSION LINE PURPOSES AS CONTAINED IN INSTRUMENT RECORDED JULY 21, 1954 IN BOOK 1395 AT PAGE 571. [DOES NOT

ITEM 11 RIGHT OF WAY EASEMENT AS GRANTED TO PUBLIC SERVICE COMPANY OF COLORADO IN INSTRUMENT RECORDED JULY 21, 1954, IN BOOK 1395 AT PAGE

ITEM 12 RIGHT OF WAY EASEMENT AS GRANTED TO THE MOUNTAIN STATES TELEPHONE AND TELEGRAPH COMPANY IN INSTRUMENT RECORDED APRIL 20, 1957, IN BOOK 1475 AT PAGE 553. [AFFECTS THE PROPERTY BUT IS BLANKET IN NATURE]

ITEM 13 TERMS, CONDITIONS AND PROVISIONS OF EASEMENT RECORDED OCTOBER 31,

TERMS, CONDITIONS AND PROVISIONS OF ANNEXATION AGREEMENT RECORDED DECEMBER 28, 1977 UNDER RECEPTION NO. 1739852. [MAY INCLUDE A PORTION

TERMS, CONDITIONS AND PROVISIONS OF ERIE AIR PARK SUBDIVISION AGREEMENT RECORDED MAY 03, 1978 UNDER RECEPTION NO. 1752378.

ITEM 16 TERMS, CONDITIONS AND PROVISIONS OF AVIATION EASEMENT AND AGREEMENT RECORDED MAY 11, 1978 UNDER RECEPTION NO. 1753139. [AFFECTS THE

> TERMS, CONDITIONS AND PROVISIONS OF EASEMENT FOR RUNWAY LIGHT INSTALLATION AND MAINTENANCE, DRAINAGE AND SNOW REMOVAL AGREEMENT RECORDED MAY 11, 1978 UNDER RECEPTION NO. 1753142. [DOES NOT AFFECT

> TERMS, CONDITIONS AND PROVISIONS OF SOLAR EASEMENT AND AGREEMENT RECORDED MAY 11, 1978 UNDER RECEPTION NO. 1753143. [AFFECTS THE PROPERTY BUT IS BLANKET IN NATURE FOR COLLECTION OF SOLAR PANELS]

ITEM 19 EASEMENTS, CONDITIONS, COVENANTS, RESTRICTIONS, RESERVATIONS AND NOTES ON THE PLAT OF ERIE AIR PARK SUBDIVISION RECORDED MAY 03, 1978 UNDER

ITEM 20 THE EFFECT, IF ANY, OF LETTER RECORDED AUGUST 12, 1982 UNDER RECEPTION NO. 1900277. [AFFECTS THE PROPERTY BUT IS BLANKET IN NATURE]

> JERMS, CONDITIONS AND PROVISIONS OF LEASE RECORDED SEPTEMBER 29, 1982 AT RECEPTION NO. 1905076. [AFFECTS THE PROPERTY BUT IS BLANKET IN

NOTE: EXTENSION OF THE ABOVE LEASE AS CLAIMED BY AFFIDAVIT OF PRODUCTION WAS RECORDED OCTOBER 12, 1984 UNDER RECEPTION NO. 1984915.

RESTRICTIVE COVENANTS, WHICH DO NOT CONTAIN A FORFEITURE OR REVERTER CLAUSE, AS CONTAINED IN INSTRUMENT RECORDED MAY 11, 1978, UNDER RECEPTION NO. 1753140 AND AS AMENDED IN INSTRUMENT RECORDED SEPTEMBER 30, 1993, UNDER RECEPTION NO. 2352630 IN BOOK 1404 AND AS AMENDED DECEMBER 27, 1993 AT RECEPTION NO. 2365912 AND AS AMENDED IN INSTRUMENT RECORDED DECEMBER 21, 1995, UNDER RECEPTION NO. 2468577 IN BOOK 1524 AND AMENDED OCTOBER 22, 2002 AT RECEPTION NO. 2998230.

TERMS, CONDITIONS AND PROVISIONS OF AGREEMENT RECORDED APRIL 28, 1986 AT RECEPTION NO. 2051362. [DOES NOT AFFECT THE PROPERTY]

TERMS, CONDITIONS AND PROVISIONS OF ASSESSMENT RECORDED NOVEMBER 21, 1990 AT RECEPTION NO. 2233799. [AFFECTS THE PROPERTY BUT IS BLANKET IN

ITEM 25 THE TERMS AND PROVISIONS OF ORDINANCE NOS. 409 AND 411, RECORDED FEBRUARY 4, 1991 UNDER RECEPTION NO. 2240420 AND FEBRUARY 25, 1991 UNDER RECEPTION NO. 2242128. [AFFECTS THE PROPERTY BUT IS BLANKET IN

ITEM 26 TERMS, CONDITIONS AND PROVISIONS OF AGREEMENT RECORDED MARCH 05, 1991 AT RECEPTION NO. 2243072. [AFFECTS THE PROPERTY BUT IS BLANKET IN

ITEM 27 ORDER OF INCLUSION FOR WELD COUNTY PORTION OF THE TOWN OF ERIE INTO THE NORTHERN COLORADO WATER CONSERVANCY DISTRICT RECORDED FEBRUARY 6, 1992 UNDER RECEPTION NO. 2277399. [AFFECTS THE PROPERTY BUT IS

ITEM 28 TERMS, AGREEMENTS, PROVISIONS, CONDITIONS AND OBLIGATIONS, AS CONTAINED IN AGREEMENT REGARDING INSTALLATION OF SANITARY SEWER LINES BY AND BETWEEN ERIE WATER AND SANITATION DISTRICT AND ROBERT LEE ROCK RECORDED AUGUST 13, 1992 UNDER RECEPTION NO. 2299958 IN BOOK 1347.

ITEM 29 RESTRICTIVE COVENANTS, WHICH DO NOT CONTAIN A FORFEITURE OR REVERTER CLAUSE, AS CONTAINED IN INSTRUMENT RECORDED DECEMBER 27, 1993, UNDER RECEPTION NO. 2365912. [AFFECTS THE PROPERTY BUT IS BLANKET IN NATURE]

ITEM 30 TERMS, CONDITIONS AND PROVISIONS OF ORDER RECORDED APRIL 18, 1995 AT RECEPTION NO. 2434694. [DOES NOT AFFECT THE PROPERTY]

> TERMS, CONDITIONS AND PROVISIONS OF ORDER RECORDED APRIL 27, 1995 AT RECEPTION NO. 2435904. [AFFECTS PROPERTY AND IS SHOWN] JOHN NEEDS TO

ITEM 32 MATTERS AS SET FORTH ON SURVEY RECORDED JUNE 28, 2002 AT RECEPTION NO. 2969635. [AFFECTS PROPERTY AND IS SHOWN (GILLANS SURVEY)] ITEM 33 TERMS, CONDITIONS AND PROVISIONS OF OPTION RECORDED MARCH 20, 2006 AT RECEPTION NO. 3371704. [AFFECTS PROPERTY AND IS SHOWN]

> TERMS, CONDITIONS AND PROVISIONS OF TAXIWAY EASEMENT DEED AND AGREEMENT RECORDED DECEMBER 15, 2006 AT RECEPTION NO. 3442230.

EXISTING LEASES OR TENANCIES, IF ANY. [AFFECTS THE PROPERTY BUT IS

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LEGEND

EXISTING CONTOUR EXISTING SWALE

PUBLIC LAND CORNER FOUND

SET #5 REBAR WITH 1" RED PLASTIC CAP STAMPED SCOTT COX ASC PLS 24302 (P&C) (UNLESS NOTED) SET NAIL AND 3/4" BRASS TAG STAMPED PLS 24302 (NAIL&TAG) AS NOTED FOUND MONUMENT AS NOTED

EXISTING ELECTRIC METER

EXISTING WATER VALVE

EXISTING GAS METER EXISTING WATER METER

CONTROL POINT EXISTING FIRE HYDRANT EXISTING FENCE

EXISTING WATER W/FIRE HYDRANT EXISTING STORM SEWER W/MANHOLE

RECORD COURSE

MEASURED COURSE PER THIS SURVEY RECORD OR CALCULATED POSITION

TO FOUND MONUMENT

- THE BASIS OF BEARINGS IS THE WEST LINE OF THE SW 1/4 OF SECTION 31, T1N, R68W OF THE 6TH P.M. BETWEEN THE FOUND MONUMENTS SHOWN HEREON AND BEARS NO1°04'56"E, PER THE PLAT.
- 2. BENCH MARK: NGS POINT AI5917 (LOCSUR), AN ALUMINUM DISK SET IN TOP OF CONCRETE MONUMENT LOCATED 122.4 FEET WEST-SOUTHWEST FROM THE CENTER OF RUNWAY 15-33 AT ERIE AIR PARK. ELEVATION =5117.77' NAVD88.
- 3. THE SIZE AND TYPE OF MONUMENTS FOUND ARE SHOWN HEREON.
- 4. NOTICE: ACCORDING TO COLORADO LAW, YOU MUST COMMENCE ANY LEGAL ACTION BASED ON ANY DEFECT IN THIS SURVEY WITHIN THREE YEARS AFTER YOU FIRST DISCOVERED SUCH DEFECT. IN NO EVENT, MAY ANY ACTION BASED UPON ANY DEFECT IN THIS SURVEY BE COMMENCED MORE THAN TEN YEARS FROM THE DATE OF THE CERTIFICATION SHOWN HEREON. CRS-13-80-105 (3)(a)
- FLOOD PLAIN DESIGNATION OF THE SURVEYED PROPERTY PER LETTER OF MAP REVISION CASE NO.: 13-08-0247 EFFECTIVE DATE DECEMBER 28, 2012 IS ZONE X, BEING AREAS DETERMINED TO BE OUTSIDE THE 0.2% ANNUAL CHANCE FLOODPLAIN.
- THE LOCATION OF THE ABOVE GROUND UTILITIES SHOWN HEREON ARE BASED ON THE FIELD SURVEY BY SCOTT, COX & ASSOCIATES, INC. THE LOCATIONS OF THE UNDERGROUND UTILITIES SHOWN HEREON ARE BASED ON SAID SURVEY AND INFORMATION PROVIDED BY UNCC, CITY OF BOULDER, XCEL AND QWEST MAPPING SCOTT, COX & ASSOCIATES, INC. IS NOT RESPONSIBLE FOR UTILITY INFORMATION PROVIDED BY OTHERS. SCOTT, COX & ASSOCIATES, INC. RECOMMENDS THAT THE LOCATION OF THE UTILITIES BE FIELD VERIFIED PRIOR TO ANY DIGGING ON, OR ADJACENT TO THE SUBJECT PROPERTY.
- PLATS AND LAND SURVEY PLATS DEPOSITED AT BOULDER LAND USE DEPARTMENT, REFERENCED OR USED FOR THIS SURVEY: ERIE AIR PARK SUBDIVISION REPLAT A, RECEPTION NO. 02302520; ERIE AIR PARK SUBDIVISION, RECEPTION NO. 1752380.
- 8. ALL ADJOINING STREETS ARE PUBLIC.
- THERE IS OBSERVED EVIDENCE OF CURRENT EARTH MOVING WORK. THERE IS NO 9. OBSERVED EVIDENCE OF BUILDING CONSTRUCTION OR BUILDING ADDITIONS. NO OBSERVED EVIDENCE OF RECENT STREET OR SIDEWALK CONSTRUCTION OR REPAIRS. NO OBSERVED EVIDENCE OF WETLAND AREAS AS DELINEATED BY APPROPRIATE AUTHORITIES. NO RECORD OF OFFSITE EASEMENTS OR SERVITUDES BENEFITING THE SURVEYED PROPERTY.

CERTIFICATION

SURVEY NOTES

TO: LAND TITLE GUARANTEE COMPANY; OLD REPUBLIC NATIONAL TITLE INSURANCE COMPANY: DAVID S. NASSAR: SHERIDAN SCHOFIELD AND PEGGY J. SCHOFIELD

THIS IS TO CERTIFY THAT THIS MAP OR PLAT AND THE SURVEY ON WHICH IT IS BASED WERE MADE IN ACCORDANCE WITH THE 2016 MINIMUM STANDARD DETAIL REQUIREMENTS FOR ALTA/NSPS LAND TITLE SURVEYS, JOINTLY ESTABLISHED AND ADOPTED BY ALTA AND NSPS, AND INCLUDES ITEMS 1-5, 6a, 8, 11, AND 13 OF TABLE A THEREOF. THE FIELDWORK WAS COMPLETED ON JANUARY 25, 2018.

24302 A. JOHN BURI, PLS 24302 FOR AND ON BEHALF OF SCOTT, COX & ASSOCIATES

ALTA/NSPS LAND TITLE SURVEY TRACT E-2 ERIE AIR PARK TRACT E MINOR SUBDIVISION LOCATED IN THE SW 1/4 SEC. 31 T1N, R68W OF THE 6TH P.M. TOWN OF ERIE COUNTY OF BOULDER STATE OF COLORADO

AIRPORT ROAD

SCOTT, COX & ASSOCIATES, INC. consulting engineers • surveyors 1530 55th Street • Boulder, Colorado 80303 (303) 444 - 3051						
Designed by _	AJB	Date	Scale	Drawing no.		Sheet
	JAS	10/11/19	1"=100'	175	IOC-1	1
Drawn by _		Revision	Description		Date	Project no.
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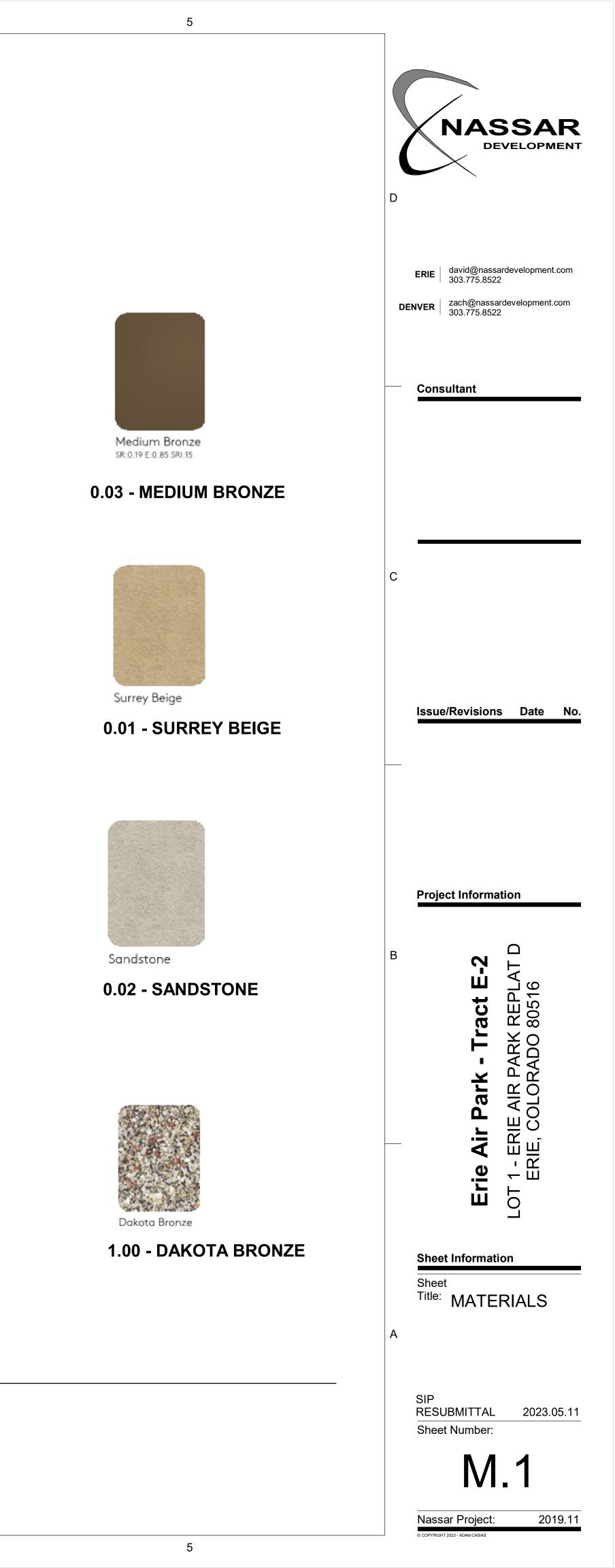


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Prepared For: Real Investments, LLC c/o Nassar Development 3000 Airport Drive, Unit 203 Erie, CO 80516

Attention: Mr. David Nassar

Job Number: 19-0040

November 29, 2018

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TABLE OF CONTENTS

	Page
Purpose and Scope of Study	1
Planned Development	2
Site Conditions	2
Geologic Setting and Hazards	3
Initial Subsurface Exploration	9
Laboratory Testing	10
Subsurface Conditions	10
Preliminary Geotechnical Considerations on Development	12
Anticipated Foundation and Floor System Options	12
Water-Soluble Sulfates	13
Soil Corrosivity	14
Project Earthwork	16
Excavation Considerations	19
Utility Pipe Installation	21
Surface Drainage	23
Preliminary Pavement Sections	26
Additional Exploration Requirements	27
Closure	
Locations of Test Holes	Figure 1
Logs of Test Holes	Figure 2
Legend and Notes	Figure 3
Summary of Laboratory Test Results	Table 1
Summary of Soil Corrosion Test Results	Table 2
Detailed Drill Logs	Appendix A

PURPOSE AND SCOPE OF STUDY

This report presents the results of a preliminary geotechnical evaluation performed by GROUND Engineering Consultants, Inc. (GROUND) for the Real Investments, LLC in support of design of the proposed development of Erie Air Park Lot E-2 in Erie, Colorado. Our study was conducted in general accordance with GROUND's Proposal No. 1908-1591, dated August 27th, 2019

A field exploration program was conducted to obtain information on the subsurface conditions. Material samples obtained during the subsurface exploration were tested in the laboratory to provide data on the engineering characteristics of the on-site soils. The results of the field exploration and laboratory testing are presented herein.

This preliminary report has been prepared to summarize the data obtained and to present our findings and conclusions based on the proposed development/improvements and the subsurface conditions encountered. Preliminarv design parameters and a discussion of engineering considerations related to the proposed improvements are included herein. This report should be understood and utilized in its entirety; specific sections of the text, drawings, graphs, tables, and other information contained within this report are intended to be understood in the context of the entire report. This includes the *Closure* section of the report which outlines important limitations on the information contained herein.

This report was prepared for design purposes of Real Investments, LLC based on our understanding of the proposed project at the time of preparation of this report. The data, conclusions, opinions, and preliminary geotechnical parameters provided herein should not be construed to be sufficient for other purposes, including the use by contractors, or any other parties for any reason not specifically related to the design of the project. Furthermore, the information provided in this report was based on the exploration and testing methods described below. Deviations between what was reported herein and the actual surface and/or subsurface conditions may exist, and in some cases those deviations may be significant. The preliminary / initial information presented in this report is not sufficient for design. Additional, structure-specific subsurface exploration and site evaluation MUST be performed prior to final design and construction.

PLANNED DEVELOPMENT

We understand that the subject development is currently in preliminary or feasibility stage of development. Provided information indicates that proposed construction may ultimately consist of five hangar structures with concrete pavement. Grading information was unavailable at the time of this report preparation. Based on the existing site topography, material cuts and fills up to approximately 3 feet may be necessary to facilitate construction. We assume structural loads likely will be light to moderate, typical of this type of construction. We assume no below grade levels are planned for construction. Additionally, we understand paved parking areas and drive lanes are also anticipated.

If the proposed development differs significantly from that described above, GROUND should be notified to re-evaluate the conclusions and parameters contained herein.

SITE CONDITIONS

At the time of our subsurface exploration program, the site generally existed as an undeveloped lot. Construction debris and stockpiles of fill materials were observed at the time of drilling. No samples of these materials were sampled or tested as a part of this study. The



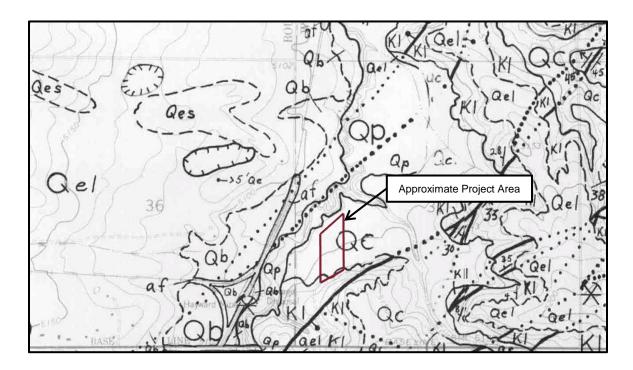
site is bordered by a natural drainage to the north, commercial buildings to the east and west and Airport Drive to the south. The ground surface is generally flat with an overall slope down to the north at a slope of approximately 1 percent.

Man-made fill was observed to varying depths in most of test holes during the subsurface exploration program. The exact extents, limits, and composition of any man-made fill were not determined as part of the scope of work addressed by this study and should be expected to potentially exist at varying depths and locations across the site.

GEOLOGIC SETTING AND HAZARDS

Site Geology

Published geologic maps, e.g., Colton and Anderson (1977),¹ depict the project area as underlain by Upper Holocene and Upper Pleistocene Colluvium (**Qc**) and by the Upper Cretaceous Laramie Formation (**KI**). Alluvial deposits are also mapped in the project area as well. A portion of the geologic map is reproduced below.



Colluvium, in the project area, generally consists of fine to coarse grained sands, clays, and silts similar to the bedrock materials from which they are derived. Cobble and boulder sized clasts of bedrock can be present as well.

Alluvium generally consist of fine to coarse sands and gravels with cobbles and boulders. Clay and silt lenses are present locally. The large cobbles and boulders present locally can be difficult to handle or process.

¹ Colton, R.B., and Anderson, L.W., 1977, Preliminary geologic map of the Erie quadrangle, Boulder, Weld, and Adams Counties, Colorado: U.S. Geological Survey, Miscellaneous Field Studies Map MF-882, scale 1:24,000

The Laramie Formation generally consists of interbedded sandstone, claystone, siltstone, shale, and coal. The claystones and shales are typically moderately to highly expansive and some sandstones, along with other well-cemented beds, of Denver Formation can be very hard and difficult to excavate. Additionally, the coal beds present in the Laramie Formation have been mined locally.

Geologic Hazards

<u>Expansive Soils</u> Swelling clayey soils and bedrock change volume in response to changes in moisture content that can occur seasonally, or in response to changes in land use, including development. Expansion potentials vary with moisture contents, density, and details of the clay chemistry and mineralogy. The swell potential in any particular area can vary markedly both laterally and vertically due to the complex interbedding of the site soil and bedrock materials. Moisture changes also occur erratically, resulting in conditions that cannot always be predicted.

The shallow earth materials underlying the site included silts and clays and the underlying bedrock includes claystones. The plasticity of the site soils ranged from moderately to highly plastic. Swell-consolidation testing indicated a very significant potential for heave at the site with swells up to 8.1 percent measured against surcharge pressures approximating overburden loads (see Table 1). Design-level geotechnical evaluations of individual building sites, roadways, and other movement sensitive structures should include an assessment of the presence of swelling materials in the foundation soils, so that appropriate, remedial design and construction can be implemented, as necessary.

<u>Collapsible Soils</u> Certain surficial deposits in the Denver metropolitan area, typically eolian (wind-blown), materials are known to be susceptible to local hydro-consolidation or "collapse." Hydro-consolidation consists of a significant volume loss due to restructuring of the constituent grains of the soil to a more compact arrangement upon wetting. Undocumented fills soils, like those present on site, also can be susceptible to "collapse."

Significant consolidations were not measured in the swell-consolidation testing performed on site materials. However, given the presence of undocumented fill soils at the site, consolidations may be possible in site soils. Again, design-level geotechnical

evaluations for building design, roadway alignment, etc. should include an assessment of the possible presence of collapsible materials in the foundation soils, so that appropriate, remedial design and construction can be implemented, if necessary.

<u>Radon</u> Testing for the possible presence of radon gas prior to project development does not yield useful results regarding the potential accumulation of radon in completed structures. Radon accumulations typically are found in basements or other enclosed portions of buildings built in areas underlain at relatively shallow depths by granitic crystalline rock. The likelihood of encountering radon in concentrations exceeding applicable health standards on the subject site, underlain by relatively deep soils and sedimentary bedrock, is significantly lower.

Radon testing should be performed in each building on-site, after construction is completed. Proper ventilation usually is sufficient to mitigate potential radon accumulations. Building designs should accommodate such ventilation for all building areas.

<u>Seismic Activity / Faulting</u> Neither site reconnaissance nor review of available geologic maps indicated the trace of an active or potentially active fault traversing or immediately adjacent to the site. Therefore, the likelihood of surface fault rupture at the site is considered to be relatively low.

The closest extent of a documented active or potentially active fault to the site is the Rock Creek Fault, which is located approximately 8.2 miles to the southwest (Kirkham and Rogers, 1981²; Colorado Geological Survey, 2008³). This suspect fault has a cumulative length of approximately 2.5 miles, trends generally northeast, and is generally considered to be a high angle, listric, northwest dipping, reverse fault with late Cenozoic displacement. The risk of this fault giving rise to damaging, earthquake-induced ground motions at the site is considered to be relatively low give the magnitudes of previously recorded events in the project area and last known movements of the fault.

² Kirkham, R.M., and W. P. Rogers, 1981, *Earthquake Potential in Colorado, A Preliminary Evaluation*, Colorado Geological Survey, Bulletin 43.

³ Colorado Geological Survey, 2008, *Preliminary Quaternary Fault and Fold Database, and Map Server*, <u>http://geosurvey.state.co.us/Default.aspx?tabid=453</u>.

Additionally, published geologic maps, such as Colton and Anderson (1977),⁴ depict older faults within about 500 feet of the project site. These faults are only mapped as displacing older deposits and are not show as displacing younger, Quaternary deposits. Therefore, we consider the likelihood of surface fault rupture related to these faults to be low.

We consider the site to be likely to fall within the parameters of a Seismic Site Class D site, in accordance with 2015 IBC based on extrapolation of available data to depth. However, in the due to the relatively shallow nature of the bedrock, portions of the site may classify as Site Class C, but additionally information will be necessary. If a quantitative assessment of the classification is needed, shear wave velocity testing to 100+ feet or other surface testing methods will be required. A proposal for this work can be provided upon request. Compared with other regions of Colorado, recorded earthquake frequency in the project area is moderate.

<u>Slope Stability and Erosion</u> Colton and others (1975),⁵ as well as larger scale geologic maps providing coverage of the site that were reviewed for this study, did not depict landslide deposits on or adjacent to the subject site.

The site is gently sloping, but nearly flat lying in terms of slope stability. During our preliminary reconnaissance of site area, no evidence was obviously noted of mass-wasting processes associated with steep slopes, such as landslides, slumps, or unusual soil creep. Therefore, the likelihood of project developments being affected by existing large scale, unanticipated slope instabilities is considered low.

Preliminarily, it is our opinion that un-retained, permanent slope cuts be less than 10 feet in height and maintain a maximum 3 : 1 (horizontal : vertical) slope angle or less with proper erosion control measures implemented. Steeper and/or taller slopes may be possible, but must be evaluated on a case-by-case basis. Proper surface drainage controls to reduce the potential for erosional slope damage need to be implemented in the grading design to control runoff, which may be increased due to proposed pavement

⁴ Colton, R.B., and Anderson, L.W., 1977, Preliminary geologic map of the Erie quadrangle, Boulder, Weld, and Adams Counties, Colorado: U.S. Geological Survey, Miscellaneous Field Studies Map MF-882, scale 1:24,000

⁵ Colton, R.B., J.A. Holligan, and L.W. Anderson, 1975, *Preliminary Map of Landslide Deposits, Denver 1° x 2° Quadrangle, Colorado*, U.S. Geological Survey, Miscellaneous Field Studies Map MF-705.

surfaces, structures, and landscape irrigation. Re-vegetation or other means of protection should be used on graded slopes.

<u>Flooding</u> The subject property abuts a reach of Coal Creek. The Flood Insurance Rate Map (FIRM) produced by for the area FEMA (2019),⁶ depicts the northern portion of the project site as being within Zone AE, which indicates a special flood hazard area and significant risk of flooding. The southern portion of the site, however, is mapped as being within Zone X indicating a minimal risk of flooding. Therefore, portions of site do appear to be vulnerable to flooding. <u>Therefore, the site and any planned grade changes should be evaluated by a civil engineer with regard to flood risk.</u>

<u>Wetland Potential</u> No obvious indications of conditions similar to jurisdictional wetlands were apparent during GROUND's site reconnaissance. Additionally, according to the U.S. Fish and Wildlife Service,⁷ the project site is not designated as a wetland area. However, areas associated with the Coal Creek to north of the site, are mapped as jurisdictional wetlands. Site development should adhere to all regulations concerning wetland protection. Explicit designation of wetlands was not included as part of the scope of this study.

<u>Mining Activity and Mining Related Subsidence</u> Review of U.S. Geological Survey geologic maps covering the site Roberts, Hynes, and Woodward (2001)⁸ and Turney and Murray-Williams (1983)⁹ and other available, published maps depicting areas of coal extraction, indicate past mining activities within greater project that are mapped as extending beneath the project site. However, no mineshafts, adits, or other structures are depicted as being on the subject parcel, but many such structures are shown within the greater project area.

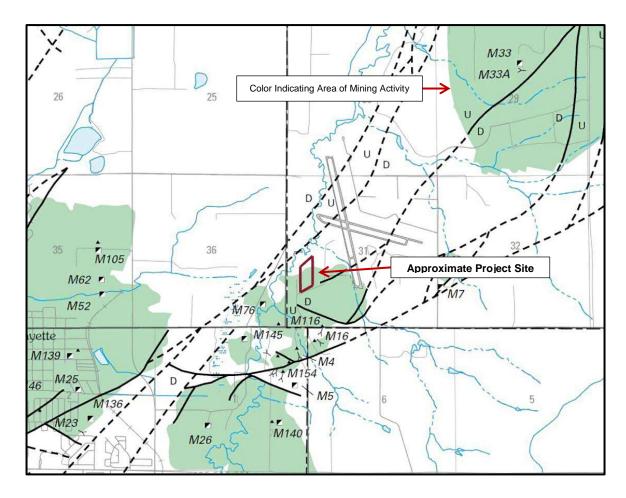
 ⁶ Federal Emergency Management Administration, 2013, <u>https://hazards-</u> <u>fema.maps.arcgis.com/apps/webappviewer/index.html?id=8b0adb51996444d4879338b5529aa9cd</u> accessed on 11/26/2019

⁷ U.S. Fish and Wildlife Service, National Wetlands Inventory, , <u>www.fws.gov/wetlands</u> accessed on 11/26/2019

⁸ Roberts, S.B., Hynes, J.L., and Woodward, C.L., 2001, Maps Showing the Extent of Mining, Locations of Mine Shafts, Adits, Air Shafts, Bedrock Faults, and Thickness of Overburden Above Abandoned Coal Mines in the Boulder-Weld Coal Field, Boulder, Weld, and Adams Counties, Colorado. U.S. Geological Survey, Geological Investigations Series Map I-2735.

 ⁹ Turney, J.E., Murray-Williams L., 1983, Colorado Front Range Inactive Coal Mine Data and Subsidence, Boulder County, Colorado Geological Survey, Plate 3 of 12.

Nearby mines with workings are presented below in a summary table and are shown on a portion of the Robert, Hynes, and Woodward (2001) map reproduced below.



Map ID	Name of Mine Working	Alternate / Previous Name	Years Active
M16	Blue Ribbon	-	1933
M76	Irvington	Haywood	1907-1908 1899-1906
M116	Parkdale	-	1907-1916
M154	Vaughn		1897-1906

Mines and Mine Workings Near the Project Site³

Mine workings that are mapped within the project area are depicted as being 150 to 250 feet below existing grades. Coal and lignite were not observed in the fill however, based on our experience in the Erie area coal and/or lignite may be encountered during construction. No indications of mining structures (i.e., shafts, adits, etc.) were apparent on the site during the site reconnaissance, however.

Published geologic maps do not indicate formations underlying the site at shallow depths that include evaporite (salt, gypsum, etc.) deposits, limestones or other materials vulnerable to subsurface dissolution. Therefore, the likelihood of subsidence associated with such rock types or other hazards related to subsurface dissolution appears to be low.

INITIAL SUBSURFACE EXPLORATION

Subsurface exploration for the project was conducted on November 5th, 2019. A total of five (5) test holes were drilled using a truck-mounted drill rig advancing continuous flight auger. The test holes were advanced to depths of about 28 to 37 feet below existing grade within approximate areas planned for development. Test holes were advanced to their planned termination depths to evaluate the subsurface conditions as well as to retrieve samples for laboratory testing and analysis. A representative of GROUND directed the subsurface exploration, logged the test holes in the field, and prepared the samples for transport to our laboratory. The test holes were backfilled following data collection operations.

Samples of the subsurface materials were retrieved with a 2-inch I.D. 'California' liner sampler or a 1.375-inch I.D. standard split spoon sampler. The sampler was driven into the substrata with blows from a 140-pound hammer falling 30 inches, a procedure similar to the Standard Penetration Test described by ASTM Method D1586. Penetration resistance values, when properly evaluated, indicate the relative density or consistency of soils. Depth and elevations at which the samples were obtained and associated penetration resistance values are shown on the test hole logs.

The approximate locations of the test holes are shown on Figure 1. Logs of the test holes are presented on Figure 2 and Appendix A. Explanatory notes and a legend are provided on Figure 3.

LABORATORY TESTING

Samples retrieved from our test holes were examined and visually classified in the laboratory by the project engineer. Laboratory testing of soil and bedrock samples included standard property tests, such as natural moisture contents, dry unit weights, grain size analyses, and Atterberg limits. Swell-consolidation testing, water soluble sulfates, and corrosivity testing were performed on select samples as well. Laboratory tests were performed in general accordance with applicable ASTM protocols. Results of the laboratory testing program are summarized in Tables 1 and 2.

SUBSURFACE CONDITIONS

In general, the test holes penetrated a thin layer of topsoil¹⁰, approximately 6 inches thick (greater or lesser thicknesses likely exist locally), underlain fill materials consisting of sandy clay with local gravel and claystone materials that extended to approximately up to approximately 11 feet below existing grades. These materials were underlain by sandy clay at depths ranging from approximately 1 to 11 feet below existing grades. Fat clay materials were encountered below the sandy clay or fill materials in test hole 1 to 3 and continued to depths of approximately 35 to 36 feet below existing grade. Siltstone/Claystone bedrock materials were encountered below the sandy clay at depths and 5 at depths of 5 and 14 feet below existing grades. These materials clay materials continued to the test hole termination depths of approximately 28 to 34 feet below

¹⁰ 'Topsoil' as used herein is defined geotechnically. The materials so described may or may not be suitable for landscaping or as a growth medium for such plantings as may be proposed for the project.

existing grades. A layer of sand and gravel, approximately 1.5 feet in thickness, was observed locally in test hole 2 at a depth of approximately 35 feet below existing grades. The test holes extended to depths between 28 and 37 feet below existing grades.

It also should be noted that coarse gravel, cobbles and boulders are not well represented in samples obtained from small diameter test holes. At this site, therefore, it should be anticipated that gravel and cobbles, and possibly boulders, may be present in the fill and native soils, as well as comparably sized fragments of construction debris, even where not included in the general descriptions of the site soil types below.

Fill materials were predominantly sandy clay with some local gravel and claystone materials, were medium to highly plastic, fine grained with trace gravel, dry to moist, and red-brown to gray-brown to brown in color with iron staining.

Clay materials were sandy, medium plastic, fine grained, dry to slightly moist, hard, and gray-brown in color with iron staining and local caliche staining.

Fat Clay materials were, highly plastic, fine grained, slightly moist to wet, medium stiff to hard, and gray-brown in color with iron staining and local caliche staining.

Sand and Gravel materials were clayey and fine to coarse grained with gravel, medium plastic, wet, medium dense to dense, and gray brown in color.

Claystone Bedrock was slightly sandy, fine grained, dry to moist, moderately to highly plastic, medium hard to very hard and resistant, and gray-brown in color with iron staining.

Groundwater was encountered at depths ranging from approximately 27 to 33 feet below existing grade at the time of drilling. Groundwater was re-checked in test hole 2 approximately 1 hour after drilling operations and was measured at approximately 23 feet below existing grades. Other test holes were backfilled due to safety. Groundwater levels can be expected to fluctuate, however, in response to annual and longer-term cycles of precipitation, irrigation, surface drainage, land use, and the development of transient, perched water conditions.

Swell-Consolidation Testing suggested a potential for swell in the tested on-site materials. Swells ranging from approximately 1.5 up to 8.1 percent were measured upon wetting under various surcharge pressures (see Table 1).

PRELIMINARY GEOTECHNICAL CONSIDERATIONS ON DEVELOPMENT

As stated, specific grading information was unavailable at the time of this report preparation. Based on the existing topography of the site, material cuts and fills up to approximately 3 feet may be necessary to facilitate construction. We assume that the building will be lightly to moderately loaded.

Primary geotechnical considerations at the project site consist of variable depths of existing fill materials, a large potential for heave within existing site materials and variable depth to bedrock materials at the project site.

Groundwater was encountered at depths ranging from approximately 23 to 33 feet below existing grade at the time of drilling. Therefore, groundwater will likely not be a factor for shallow excavations, but may be a factor in for deep foundation elements

Presented below are preliminary considerations and parameters regarding geotechnical aspects of the proposed development. These considerations and parameters are provided to assist with preliminary project planning. <u>Additional, structure-specific</u> <u>studies must be performed prior to final design.</u>

ANTICIPATED FOUNDATION AND FLOOR SYSTEM OPTIONS

Deep Foundation/Structural Floor Systems For the least potential for movement (approximately ½ inch), it is GROUND's opinion that a deep foundation system consisting of straight-shaft drilled piers advanced into the underlying bedrock with a structural floor system be utilized. Additionally, building entryways and other attached building appurtenances should ideally be founded on piers the same as the main building structure, to reduce the potential of differential movement. It is anticipated that bedrock penetrations of approximately 20 to 25 feet and pier lengths ranging from approximately 45 feet to greater than 60 feet would satisfy geotechnical conditions for the proposed structure. The actual pier lengths, however, should be based on the design loads, etc., as determined by the structural engineer following site-specific geotechnical explorations.

Anticipated piers may be designed for allowable end bearing pressures of 25,000 to 30,000 psf and a skin friction of 1,875 to 2,250 psf for the portion of the pier penetrating competent bedrock.

Shallow Foundation/Slab-on-grade Floor Systems Alternatively, but not equal in performance, a shallow foundation and slab-on-grade floor system could be constructed on a fill prism of imported granular fill materials. Based on our exploration and limited analysis program, an over-excavation and re-placement of the existing site materials with non-expansive import materials to a depth of at least 15 feet below the existing grade may be necessary to support a shallow foundation and slab-on-grade floor system for the proposed construction. Please note that greater thicknesses of remedial earthwork may be required beneath footings/slabs following final geotechnical exploration and laboratory testing programs.

We anticipate that allowable bearing pressures where footings bear on imported nonexpansive granular fill materials will range from 2,000 to 3,000 psf for associated settlements of about 1 inch. Similarly, slabs-on-grade bearing on 15 feet or more of imported non-expansive granular fill material could be designed based on an allowable subgrade vertical modulus (K) ranging from 100 to 200 pci.

Note that a combination of deep foundations with a reinforced slab on grade may be desirable from a cost standpoint assuming that the owner can accept the increased potential for slab movements. A risk assessment can be determined after final structure locations are identified and further subsurface exploration is completed

WATER-SOLUBLE SULFATES

The concentrations of water-soluble sulfates measured in a selected sample retrieved from the test holes was approximately 0.05 percent by weight (See Table 2). Such concentrations of soluble sulfates represent a negligible environment for sulfate attack on concrete exposed to these materials. Degrees of attack are based on the scale of 'negligible,' 'moderate,' 'severe' and 'very severe' as described in the "Design and Control of Concrete Mixtures," published by the Portland Cement Association (PCA). The Colorado Department of Transportation (CDOT) utilizes a corresponding scale with 4 classes of severity of sulfate exposure (Class 0 to Class 3) as described in the published table below.

REQUIREMENTS TO PROTECT AGAINST DAMAGE TO CONCRETE BY SULFATE

Severity of Sulfate Exposure	Water-Soluble Sulfate (SO₄) In Dry Soil (%)	Sulfate (SO₄) In Water (ppm)	Water Cementitious Ratio (maximum)	Cementitious Material Requirements
Class 0	0.00 to 0.10	0 to 150	0.45	Class 0
Class 1	0.11 to 0.20	151 to 1500	0.45	Class 1
Class 2	0.21 to 2.00	1501 to 10,000	0.45	Class 2
Class 3	2.01 or greater	10,001 or greater	0.40	Class 3

ATTACK FROM EXTERNAL SOURCES OF SULFATE

Based on this datum no use of a special, sulfate-resistant cement in project concrete appears necessary.

SOIL CORROSIVITY

Data were obtained to support an initial assessment of the potential for corrosion of ferrous metals in contact with earth materials at the site, based on the conditions at the time of GROUND's evaluation. The test results are summarized in Table 2.

Reduction-Oxidation testing in a selected sample indicated a negative potential: approximately -97 millivolts. Such low potentials typically create a more corrosive environment.

Sulfide Reactivity testing indicated a 'positive' result in the local soils. The presence of sulfides in the soils suggests a more corrosive environment.

Soil Resistivity In order to assess the "worst case" for mitigation planning, a sample of material retrieved from the test holes was tested for resistivity in the laboratory, after being saturated with water, rather than in the field. Resistivity also varies inversely with temperature. Therefore, the laboratory measurements were made at a controlled temperature. Measurement of electrical resistivity indicated a value of approximately 1,950 ohm-centimeters in the selected sample of site soils.

pH Where pH is less than 4.0, soil serves as an electrolyte; the pH range of about 6.5 to 7.5 indicates soil conditions that are optimum for sulfate reduction. In the pH range

above 8.5, soils are generally high in dissolved salts, yielding a low soil resistivity.¹¹ Testing of a selected sample of site soils indicated a pH value of about 8.8.

Corrosivity Assessment The American Water Works Association (AWWA) has developed a point system scale used to predict corrosivity. The scale is intended for protection of ductile iron pipe but is valuable for project steel selection. When the scale equals 10 points or higher, protective measures for ductile iron pipe are indicated. The AWWA scale is presented below. The soil characteristics refer to the conditions at and above pipe installation depth.

Table A.1 Soil-Test Evaluation

Soil Characteristic / Value Points **Redox Potential** < 0 (negative values) 5 0 to +50 mV 4 +50 to +100 mV 31/2 > +100 mV 0 Sulfide Reactivity Positive 31/2 Trace 2 Negative 0 Soil Resistivity 10 <1,500 ohm-cm 1,500 to 1,800 ohm-cm 8 1,800 to 2,100 ohm-cm 5 2 2,100 to 2,500 ohm-cm 2,500 to 3,000 ohm-cm 1 >3,000 ohm-cm 0 pН 0 to 2.0 5 2.0 to 4.0 3 4.0 to 6.5 0 6.5 to 7.5 0 * 7.5 to 8.5 0 >8.5 3 Moisture Poor drainage, continuously wet 2 Fair drainage, generally moist 1 Good drainage, generally dry 0 * If sulfides are present and low or negative redox-potential results (< 50 mV) are obtained, add three (3) points for this range.

¹¹ American Water Works Association ANSI/AWWA C105/A21.5-05 Standard.

We anticipate that drainage at the site after construction will be effective. Nevertheless, based on the preliminary values obtained for this study, the overburden soils and bedrock appear to comprise a corrosive environment for ferrous metals (16½).

If additional information is needed regarding soil corrosivity, then the American Water Works Association or a corrosion engineer should be contacted. It should be noted, however, that changes to the site conditions during construction, such as the import of other soils, or the intended or unintended introduction of off-site water, might alter corrosion potentials significantly.

PROJECT EARTHWORK

The following information is for private improvements; public roadways or utilities should be constructed in accordance with applicable municipal / agency standards.

General Considerations Site grading should be performed as early as possible in the construction sequence to allow settlement of fills and surcharged ground to be realized to the greatest extent prior to subsequent construction.

Prior to earthwork construction, concrete/asphalt, vegetation and other deleterious materials should be removed and disposed of off-site or stockpiled for reuse evaluation. Relic underground utilities should be abandoned in accordance with applicable regulations, removed as necessary, and properly capped.

Topsoil present on-site should not be incorporated into ordinary fills. Instead, topsoil should be stockpiled during initial grading operations for placement in areas to be landscaped or for other approved uses. As mentioned, the topsoil encountered was not tested for quality and may not be suitable for all landscaping purposes.

Existing Fill Soils Man-made fill was encountered during the exploration. Actual contents and composition of any man-made fill materials are not known; therefore, some of the excavated man-made fill materials (if encountered) may not be suitable for replacement as backfill. The geotechnical engineer should be retained during site excavations to observe the excavated fill materials and provide guidance for its suitability for reuse.

Use of Existing Native Soils Overburden soils that are free of trash, organic material, construction debris, and other deleterious materials are suitable, in general, for placement as compacted fill. Organic materials should not be incorporated into project fills.

Fragments of rock, cobbles, and inert construction debris (e.g., concrete or asphalt) larger than 3 inches in maximum dimension will require special handling and/or placement to be incorporated into project fills. In general, such materials should be placed as deeply as possible in the project fills. Existing asphalt or road base materials, if processed sufficiently, could potentially be used as grading materials. A geotechnical engineer should be consulted regarding appropriate parameters for usage of such materials on a case-by-case basis when such materials have been identified during earthwork. Standard parameters that likely will be generally applicable can be found in Section 203 of the current CDOT Standard Specifications for Road and Bridge Construction.

Imported Fill Materials If it is necessary to import material to the site, the imported soils should be free of organic material, and other deleterious materials. **Imported material should consist of soils that have less than 50 percent passing the No. 200** Sieve and should have a plasticity index of less than 15. Representative samples of the materials proposed for import should be tested and approved by the geotechnical engineer prior to transport to the site.

Fill Platform Preparation Prior to filling, the top 8 to 12 inches of in-place materials on which fill soils will be placed should be scarified, moisture conditioned and properly compacted in accordance with the parameters below to provide a uniform base for fill placement. If over-excavation is to be performed, then these parameters for subgrade preparation are for the subgrade **below the bottom** of the specified over-excavation depth.

If surfaces to receive fill expose loose, wet, soft, or otherwise deleterious material, additional material should be excavated, or other measures taken to establish a firm platform for filling. The surfaces to receive fill must be effectively stable prior to placement of fill.

Fill Placement Fill materials should be thoroughly mixed to achieve a uniform moisture content, placed in uniform lifts not exceeding 8 inches in loose thickness, and properly compacted.

Soils that classify as GP, GW, GM, GC, SP, SW, SM, or SC in accordance with the USCS classification system (granular materials) should be compacted to 95 or more percent of the maximum modified Proctor dry density at moisture contents within 2 percent of optimum moisture content as determined by ASTM D1557.

Site Soils that classify as ML and CL, should be compacted to 95 percent of the maximum standard Proctor density at moisture contents from 1 percent below to 3 percent above the optimum moisture content as determined by ASTM D698. No fill materials should be placed, worked, rolled while they are frozen, thawing, or during poor/inclement weather conditions.

Site soils that classify as CH should be compacted to 95 percent of the maximum standard Proctor density at moisture contents from 1 percent above to 3 percent above the optimum moisture content as determined by ASTM D698 and should not be used as structural fill.

Care should be taken with regard to achieving and maintaining proper moisture contents during placement and compaction. Materials that are not properly moisture conditioned may exhibit significant pumping, rutting, and deflection at moisture contents near optimum and above. The contractor should be prepared to handle soils of this type, including the use of chemical stabilization, if necessary.

Compaction areas should be kept separate, and no lift should be covered by another until relative compaction and moisture content within the ranges are obtained.

Settlements Settlements will occur in filled ground, typically on the order of 1 to 2 percent of the fill depth. If fill placement is performed properly and is tightly controlled, in GROUND's experience the majority (on the order of 60 to 80 percent) of that settlement will typically take place during earthwork construction, provided the contractor achieves the compaction levels provided herein. The remaining potential settlements likely will take several months or longer to be realized, and may be exacerbated if these fills are subjected to changes in moisture content.

Cut and Filled Slopes Permanent site slopes supported by on-site soils up to 10 feet in height may be constructed no steeper than 3 (H) to 1 (V). In the event slopes greater than 10 feet in height are planned, a slope stability analysis should be performed. Minor raveling or surficial sloughing should be anticipated on slopes cut at this angle until vegetation is well re-established. Surface drainage should be designed to direct water away from slope faces.

Use of Squeegee Relatively uniformly graded fine gravel or coarse sand, i.e., "squeegee," or similar materials commonly are proposed for backfilling foundation excavations, utility trenches (excluding approved pipe bedding), and other areas where employing compaction equipment is difficult. In general, GROUND does not suggest this procedure for the following reasons:

Although commonly considered "self-compacting," uniformly graded granular materials require densification after placement, typically by vibration. The equipment to densify these materials is not available on many job-sites.

Even when properly densified, uniformly graded granular materials are permeable and allow water to reach and collect in the lower portions of the excavations backfilled with those materials. This leads to wetting of the underlying soils and resultant potential loss of bearing support as well as increased local heave or settlement.

Wherever possible, excavations should be backfilled with approved, on-site soils placed as properly compacted fill. Where this is not feasible, use of "Controlled Low Strength Material" (CLSM), i.e., a lean, sand-cement slurry ("flowable fill") or a similar material for backfilling should be considered.

Where "squeegee" or similar materials are proposed for use by the contractor, the design team should be notified by means of a Request for Information (RFI), so that the proposed use can be considered on a case-by-case basis. Where "squeegee" meets the project requirements for pipe bedding material, however, it is acceptable for that use.

EXCAVATION CONSIDERATIONS

Excavation Difficulty Test holes for the subsurface exploration were advanced to the depths indicated on the test hole logs by means of conventional, truck-mounted,

geotechnical drill equipment. We anticipate no significant excavation difficulties with heavy duty excavation equipment in good working condition.

Temporary un-shored excavation slopes for other areas up to 10 feet in height should be cut no steeper than 1.5 (H) to 1 (V) in the site soils in the absence of seepage. Some surficial sloughing may occur on slope faces cut at this angle. As stated, local conditions encountered during construction, such as loose, dry sand, or soft or wet materials, or seepage will require flatter slopes. Stockpiling of materials should not be permitted closer to the tops of temporary slopes than 5 feet or a distance equal to the depth of the excavation, whichever is greater.

Should site constraints prohibit the use of the provided slope angles, temporary shoring should be used. The shoring should be designed to resist the lateral earth pressure exerted by structure, traffic, equipment, and stockpiles. GROUND can provide shoring design upon request.

Groundwater was encountered at depths ranging from approximately 23 to 33 feet below existing grade at the time of drilling. Therefore, groundwater may be a significant factor in deep excavations and deep trench excavations. The contractor should be prepared to dewater excavations. If seepage or groundwater is encountered in project excavations, the geotechnical engineer should evaluate the conditions and provide additional parameters and considerations, as appropriate. Drilled pier excavations will encounter groundwater and very hard, resistant bedrock. The Contractor should be prepared to penetrate resistant bedrock and to install piers in the presence of groundwater.

Good surface drainage should be provided around temporary excavation slopes to direct surface runoff away from the slope faces. A properly designed swale should be provided at the top of the excavations. In no case should water be allowed to pond at the site. Slopes should be protected against erosion. Erosion along the slopes will result in sloughing and could lead to a slope failure. Any excavations in which personnel will be working must comply with all OSHA Standards and Regulations (CFR 29 Part 1926). The contractor's "responsible person" should evaluate the soil exposed in the excavations as part of the contractor's safety procedures. GROUND has provided the information above solely as a service to the client, and is not assuming responsibility for construction site safety or the contractor's activities.

UTILITY PIPE INSTALLATION

Pipe Support The bearing capacity of the site soils appeared adequate, in general, for support of the proposed utility lines. The pipe + contents are less dense than the soils which will be displaced for installation. Therefore, GROUND anticipates no significant pipe settlements in these materials where properly bedded.

Excavation bottoms may expose soft, loose, or otherwise deleterious materials, including debris. Firm materials may be disturbed by the excavation process. All such unsuitable materials should be excavated and replaced with properly compacted fill. Areas allowed to pond water will require excavation and replacement with properly compacted fill. The contractor should take particular care to ensure adequate support near pipe joints which are less tolerant of extensional strains.

Trench Backfilling Settlement of compacted soil trench backfill materials will occur, even where all the backfill is placed and compacted correctly. Typical settlements are on the order of 1 to 2 percent of fill thickness. However, the need to compact to the lowest portion of the backfill must be balanced against the need to protect the pipe from damage from the compaction process. Some thickness of backfill may need to be placed at compaction levels lower than specified (or smaller compaction equipment used together with thinner lifts) to avoid damaging the pipe. Protecting the pipe in this manner can result in somewhat greater surface settlements. Therefore, although other alternatives may be available, the following options are presented for consideration:

<u>Controlled Low Strength Material</u>: Because of these limitations, the most conservative option consists of backfilling the entire depth of the trench (both bedding and common backfill zones) with "controlled low strength material" (CLSM), i.e., a lean, sand-cement slurry, "flowable fill," or similar material along all trench alignment reaches with low tolerances for surface settlements.

If used, the CLSM used as pipe bedding and trench backfill should exhibit a 28-day unconfined compressive strength between 50 to 200 psi so that re-excavation is not unusually difficult.

Placement of the CLSM in several lifts or other measures likely will be necessary to avoid 'floating' the pipe. Measures also should be taken to maintain pipe alignment during CLSM placement.

<u>Compacted Soil Backfilling</u> For most projects, site-generated materials are utilized for backfilling. Where compacted soil backfilling is employed, using the site soils or similar materials as backfill, the risk of backfill settlements entailed in the selection of this higher risk alternative must be anticipated and accepted by the Client/Owner.

We anticipate that the on-site soils excavated from trenches will be suitable, in general, for use as common trench backfill within the above-described limitations. Backfill soils should be free of vegetation, organic debris and other deleterious materials. Fragments of rock, cobbles, and inert construction debris (e.g., concrete or asphalt) coarser than 3 inches in maximum dimension should not be incorporated into trench backfills.

Soils placed for compaction as trench backfill should be conditioned to a relatively uniform moisture content, placed and compacted in accordance with the *Project Earthwork* section of this report.

Pipe Bedding Pipe bedding materials, placement and compaction should meet the specifications of the pipe manufacturer and applicable municipal standards. Bedding should be brought up uniformly on both sides of the pipe to reduce differential loadings.

As discussed above, the use of CLSM or similar material in lieu of granular bedding and compacted soil backfill should be considered where the tolerance for surface settlement is low. (Placement of CLSM as bedding to at least 12 inches above the pipe can protect the pipe and assist construction of a well-compacted conventional backfill, although possibly at an increased cost relative to the use of conventional bedding.)

If a granular bedding material is specified, with regard to potential migration of fines into the pipe bedding, design and installation follow ASTM D2321. If the granular bedding does not meet filter criteria for the enclosing soils, then non-woven filter fabric (e.g., Mirafi[®] 140N, or the equivalent) should be placed around the bedding to reduce migration of fines into the bedding which can result in severe, local surface settlements. Where this protection is not provided, settlements can develop/continue several months or years after completion of the project. In addition, clay or concrete cut-off walls should be installed to interrupt the granular bedding section to reduce the rates and volumes of water transmitted along the sewer alignment which can contribute to migration of fines.

If granular bedding is specified, the contractor should anticipate that significant volumes of on-site soils may not be suitable for that use. Materials proposed for use as pipe bedding should be tested by a geotechnical engineer for suitability prior to use. Imported materials should be tested and approved by a geotechnical engineer prior to transport to the site.

SURFACE DRAINAGE

The site soils are relatively stable with regard to moisture content – volume relationships at their existing moisture contents. Other than the anticipated, post-placement settlement of fills, post-construction soil movement will result primarily from the introduction of water into the soil underlying the proposed structure, hardscaping, and pavements. Based on the site surface and subsurface conditions encountered in this study, we do not anticipate a rise in the local water table sufficient to approach foundation or floor elevations. Therefore, wetting of the site soils likely will result from infiltrating surface waters (precipitation, irrigation, etc.), and water flowing along constructed pathways such as bedding in utility pipe trenches.

The following drainage measures should be incorporated as part of project design and during construction. The facility should be observed periodically to evaluate the surface drainage and identify areas where drainage is ineffective. Routine maintenance of site drainage should be undertaken throughout the design life of the project. If these measures are not implemented and maintained effectively, the movement estimates provided in this report could be exceeded.

- Wetting or drying of the foundation excavations and underslab areas should be avoided during and after construction as well as throughout the improvements' design life. Permitting increases/variations in moisture to the adjacent or supporting soils may result in a decrease in bearing capacity and an increase in volume change of the underlying soils, and increased total and/or differential movements.
- 2) Positive surface drainage measures should be provided and maintained to reduce water infiltration into foundation soils.

The ground surface surrounding the exterior of each building should be sloped to drain away from the foundation in all directions. A minimum slope of 12 inches in the first 10 feet should be incorporated in the areas not covered with pavement or concrete slabs, or a minimum 3 percent in the first 10 feet in the areas covered

with pavement or concrete slabs. Reducing the slopes to comply with ADA requirements may be necessary by other design professionals but may entail an increased potential for moisture infiltration and subsequent volume change of the underlying soils and resultant distress.

In no case should water be allowed to pond near or adjacent to foundation elements, hardscaping, utility trench alignments, etc.

- 3) Drainage should be established and maintained to direct water away from sidewalks and other hardscaping as well as utility trench alignments. Where the ground surface does not convey water away readily, additional post-construction movements and distress should be anticipated.
- 4) In GROUND's experience, it is common during construction that in areas of partially completed paving or hardscaping, bare soil behind curbs and gutters, and utility trenches, water is allowed to pond after rain or snow-melt events. Wetting of the subgrade can result in loss of subgrade support and increased settlements / increased heave. By the time final grading has been completed, significant volumes of water can already have entered the subgrade, leading to subsequent distress and failures. The contractor should maintain effective site drainage throughout construction so that water is directed into appropriate drainage structures.
- 5) On some sites, slopes may descend toward buildings locally. Such slopes can be created during grading even on comparatively flat sites. In such cases, even where the slopes as described above are implemented effectively, water may flow toward and beneath a structure or other site improvements with resultant additional, post-construction movements. Where the final site configuration includes graded or retained slopes descending toward the improvements, surface drainage swales and/or interceptor drains should be installed between the improvements and the slope.

Where irrigation is applied on or above slopes, drainage structures commonly are needed near the toe-of-slope to prevent on-going or recurrent wet conditions.

- 6) Roof downspouts and drains should discharge well beyond the perimeter of the structure foundations (minimum 10 feet) and backfill zones and be provided with positive conveyance off-site for collected waters.
- 7) Based on our experience with similar facilities, the project may include landscaping/watering near site improvements. Irrigation water – both that applied to landscaped areas and over-spray – is a significant cause of distress to improvements. To reduce the potential for such distress, vegetation requiring watering should be located 10 or more feet from building perimeters, flatwork, or other improvements. Irrigation sprinkler heads should be deployed so that applied water is not introduced near or into foundation/subgrade soils. Landscape irrigation should be limited to the minimum quantities necessary to sustain healthy plant growth.
- 8) Use of drip irrigation systems can be beneficial for reducing over-spray beyond planters. Drip irrigation can also be beneficial for reducing the amounts of water introduced to foundation/subgrade soils, but only if the total volumes of applied water are controlled with regard to limiting that introduction. Controlling rates of moisture increase beneath the foundations, floors, and other improvements should take higher priority than minimizing landscape plant losses.

Where plantings are desired within 10 feet of a building, it is GROUND's opinion that the plants be placed in water-tight planters, constructed either in-ground or above-grade, to reduce moisture infiltration in the surrounding subgrade soils. Planters should be provided with positive drainage and landscape underdrains. As an alternative involving a limited increase in risk, the use of water-tight planters may be replaced by local shallow underdrains beneath the planter beds. Colorado Geological Survey – Special Publication 43 provides additional guidelines for landscaping and reducing the amount of water that infiltrates into the ground.

GROUND understands many municipalities require landscaping within 10 feet of building perimeters. Provided that positive, effective surface drainage is initially implemented and maintained throughout the life of the facility and the Owner understands and accepts the risks associated with this requirement, vegetation that requires little to no watering may be located within 10 feet of the building perimeter.

- 9) Inspections must be made by facility representatives to make sure that the landscape irrigation is functioning properly throughout operation and that excess moisture is not applied.
- 10) Plastic membranes should not be used to cover the ground surface adjacent to the building as soil moisture tends to increase beneath these membranes. Perforated "weed barrier" membranes that allow ready evaporation from the underlying soils may be used.

Cobbles or other materials that tend to act as baffles and restrict surface flow should not be used to cover the ground surface near the foundations.

- 11) Maintenance as described herein may include complete removal and replacement of site improvements in order to maintain effective surface drainage.
- 12) Detention ponds commonly are incorporated into drainage design. When a detention pond fills, the rate of release of the water is controlled and water is retained in the pond for a period of time. Where in-ground storm sewers direct surface water to the pond, the granular pipe bedding also can direct shallow groundwater or infiltrating surface water toward the pond. Thus, detention ponds can become locations of enhanced and concentrated infiltration into the subsurface, leading to wetting of foundation soils in the vicinity with consequent heave or settlement. Therefore, unless the pond is clearly down-gradient from the proposed buildings and other structures that would be adversely affected by wetting of the subgrade soils, including off-site improvements, the detention pond should be provided with an effective, low permeability liner. In addition, cut-off walls and/or drainage provisions should be provided for the bedding materials surrounding storm sewer lines flowing to the pond.

PRELIMINARY PAVEMENT SECTIONS

A pavement section is a layered system designed to distribute concentrated traffic loads to the subgrade. Performance of the pavement structure is directly related to the physical properties of the subgrade soils and traffic loadings. The standard care of

Preliminary Subsurface Exploration Program Erie Air Park Tract E Lot E-2 Erie, Colorado

practice in pavement design describes the flexible pavement section as a "20-year" design pavement: however, most flexible pavements will not remain in satisfactory condition without routine maintenance and rehabilitation procedures performed throughout the life of the pavement.

We anticipate pavement sections for the internal drives and parking areas may consist of a full depth asphalt section ranging from approximately 5 to 7 inches of asphalt. Composite sections with equivalent structural sections can be provided in the final report. A minimum section of 6 inches of Portland cement concrete underlain by at least 6 inches of Class 6 aggregate base course may also be necessary. Heavy truck traffic and loading/unloading areas should ideally be designed as a reinforced slab and consist of at least 6 to 7 inches of concrete underlain by at least 6 inches of Class 6 aggregate base course. Additionally, composite sections consisting of asphalt over aggregate base course may be utilized.

Due to the swell potential observed in the site soils, typical subgrade preparation on the order of 12 inches will likely not be sufficient at the project site. Greater depth of over-excavation should be anticipated depending on the owners tolerances for movement. Greater depths of subgrade processing will further reduce potential pavement movements.

The collection and diversion of surface drainage away from paved areas is extremely important to satisfactory performance of the pavements. The subsurface and surface drainage systems should be carefully designed to ensure removal of the water from paved areas and subgrade soils. Allowing surface waters to pond on pavements will cause premature pavement deterioration. Where topography, site constraints, or other factors limit or preclude adequate surface drainage, pavements should be provided with edge drains to reduce loss of subgrade support. The long-term performance of the pavement also can be improved greatly by proper backfilling and compaction behind curbs, gutters, and sidewalks so that ponding is not permitted and water infiltration is reduced.

ADDITIONAL EXPLORATION REQUIREMENTS

The above data and information are based on a limited preliminary subsurface exploration only. Additional geotechnical studies <u>must</u> be performed to further evaluate

the site for building-specific foundation and floor system, retaining wall parameters, final site grading, and pavement sections.

CLOSURE

Geotechnical Review The author of this report or a GROUND principal should be retained to review project plans and specifications to evaluate whether they comply with the intent of the measures discussed in this report. The review should be requested in writing.

In addition, building-specific geotechnical exploration(s) must be completed for the project prior to final design and construction.

Materials Testing Real Investments, LLC should consider retaining a geotechnical engineer to perform materials testing during construction. The performance of such testing or lack thereof, however, in no way alleviates the burden of the contractor or subcontractor from constructing in a manner that conforms to applicable project documents and industry standards. The contractor or pertinent subcontractor is ultimately responsible for managing the quality of his work; furthermore, testing by the geotechnical engineer does not preclude the contractor from obtaining or providing whatever services that he deems necessary to complete the project in accordance with applicable documents.

Limitations This report has been prepared for Real Investments, LLC as it pertains to design of the proposed Erie Air Park Lot E-2 Development as described herein. It should not be assumed to contain sufficient information for other parties or other purposes. The Client has agreed to the terms, conditions, and liability limitations outlined in our proposal between the Real Investments, LLC and GROUND. Reliance upon our report is not granted to any other potential owner, contractor, or lender. Requests for third-party reliance should be directed to GROUND in writing; granting reliance by GROUND is not guaranteed.

In addition, GROUND has assumed that the final geotechnical subsurface exploration will be performed prior to construction. Changes in project plan development or schedule should be brought to the attention of the Geotechnical Engineer, in order that the preliminary geotechnical information may be re-evaluated and, as necessary, modified.

Preliminary Subsurface Exploration Program Erie Air Park Tract E Lot E-2 Erie, Colorado

The preliminary geotechnical conclusions in this report were based on subsurface information from a limited number of exploration points, as shown in Figure 1, as well as the means and methods described herein. Subsurface conditions were interpolated between and extrapolated beyond these locations. It is not possible to guarantee the subsurface conditions are as indicated in this report. Actual conditions exposed during construction may differ from those encountered during site exploration. In addition, a contractor who obtains information from this report for development of his scope of work or cost estimates does so solely at his own risk and may find the geotechnical information in this report to be inadequate for his purposes or find the geotechnical conditions described herein to be at variance with his experience in the greater project area. The contractor should obtain the additional geotechnical information that is necessary to develop his workscope and cost estimates with sufficient precision. This includes, but is not limited to, information regarding excavation conditions, earth material usage, current depths to groundwater, etc. Because of the necessarily limited nature of the subsurface exploration performed for this study, the contractor should be allowed to evaluate the site using test pits or other means to obtain additional subsurface information to prepare his bid.

If during construction, surface, soil, bedrock, or groundwater conditions appear to be at variance with those described herein, a geotechnical engineer should be retained at once, so that our conclusions for this site may be re-evaluated in a timely manner and dependent aspects of project design can be modified, as necessary.

The materials present on-site are stable at their natural moisture content, but may change volume or lose bearing capacity or stability with changes in moisture content. Performance of the proposed structure and pavement will depend on implementation of the conclusions and information in this report and on proper maintenance after construction is completed. Because water is a significant cause of volume change in soils and rock, allowing moisture infiltration may result in movements, some of which will exceed estimates provided herein and should therefore be expected by the Owner.

ALL DEVELOPMENT CONTAINS INHERENT RISKS. It is important that ALL aspects of this report, as well as the estimated performance (and limitations with any such estimations) of proposed improvements are understood by Real Investments, LLC. Utilizing the geotechnical parameters and measures herein for planning, design, and/or construction constitutes understanding and acceptance of the conclusions with regard to risk and other information provided herein, associated improvement performance, as well as the limitations inherent within such estimates. Ensuring correct interpretation of the contents of this report by others is not the responsibility of GROUND. If any information referred to herein is not well understood, it is imperative that owner contact the author or a GROUND principal immediately. We will be available to meet to discuss the risks and remedial approaches presented in this report, as well as other potential approaches, upon request.

Current applicable codes may contain criteria regarding performance of structures and/or site improvements which may differ from those provided herein. Our office should be contacted regarding any apparent disparity.

GROUND makes no warranties, either expressed or implied, as to the professional data, opinions or conclusions contained herein. Because of numerous considerations that are beyond GROUND's control, the economic or technical performance of the project cannot be guaranteed in any respect.

This document, together with the concepts and conclusions presented herein, as an instrument of service, is intended only for the specific purpose and client for which it was prepared. Re-use of, or improper reliance on this document without written authorization and adaption by GROUND Engineering Consultants, Inc., shall be without liability to GROUND Engineering Consultants, Inc.

GROUND appreciates the opportunity to complete this portion of the project and welcomes the opportunity to provide the Real Investments, LLC or the owner with a proposal for additional geotechnical exploration at the project site.

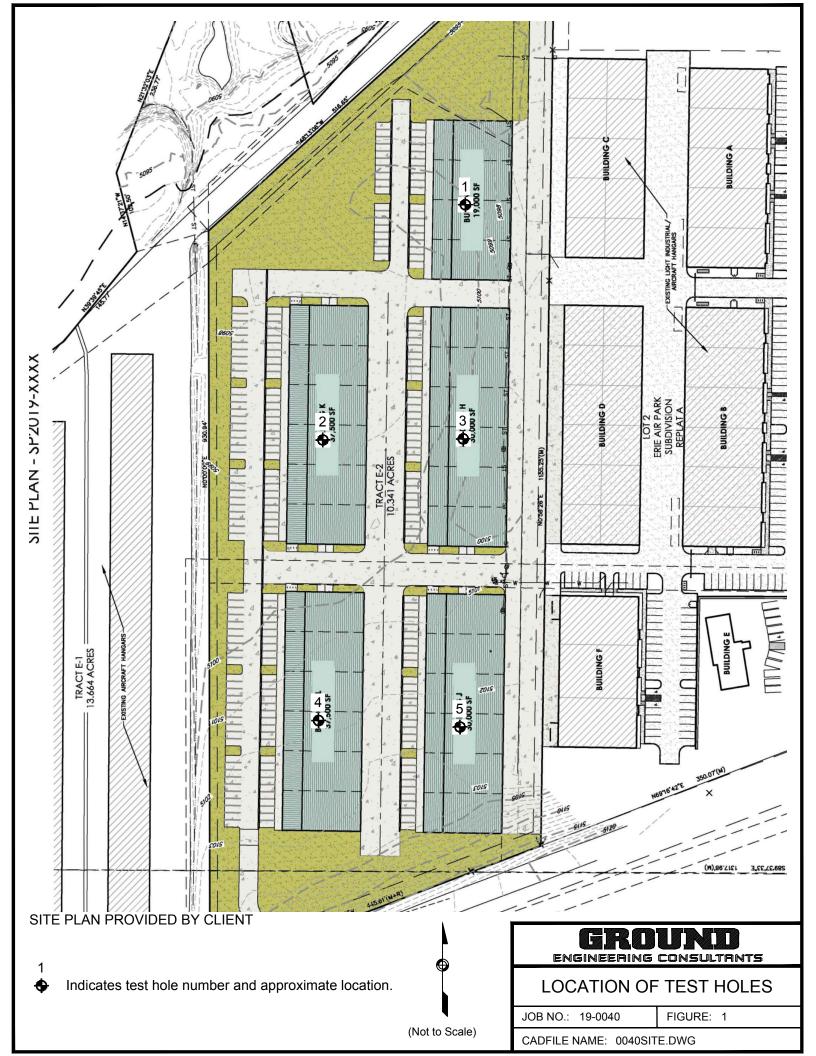
Sincerely,

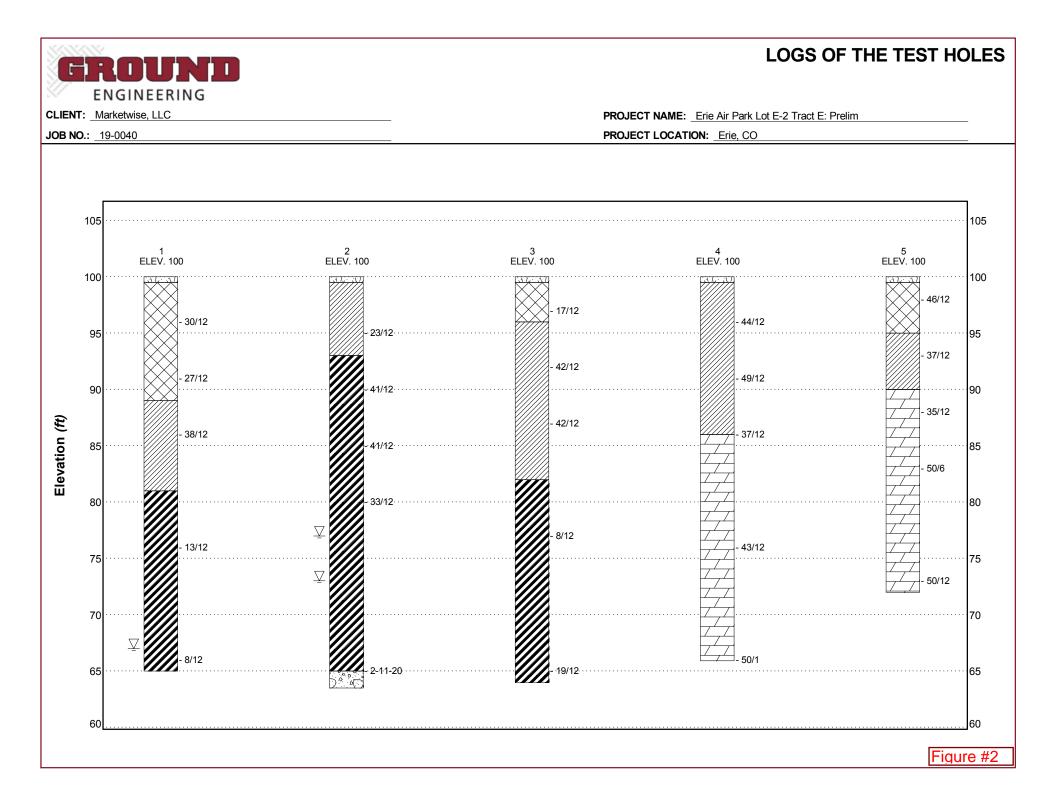
GROUND Engineering Consultants, Inc.



Kelsey Van Bemmel, P.E.

Reviewed by Joseph Zorack, P.E.





LEGEND AND NOTES



CLIENT: Marketwise, LLC

JOB NO.: 19-0040

PROJECT NAME: Erie Air Park Lot E-2 Tract E: Prelim

Modified California Liner Sampler

Standard Penetration Test Sampler

23 / 12 Drive sample blow count indicates 23 blows of a

23 / 12 Drive sample blow count indicates 23 blows of a 140 pound hammer falling 30 inches were required to drive

140 pound hammer falling 30 inches were required to drive

PROJECT LOCATION: _Erie, CO

SAMPLER SYMBOLS

the sampler 12 inches.

the sampler 12 inches.

MATERIAL SYMBOLS



TOPSOIL

FAT CLAY (CH)



LEAN CLAY

FILL

SAND AND GRAVEL

CLAYSTONE BEDROCK

NOTE: See Detailed Logs for Material descriptions.

ABBREVIATIONS

- $\[\ensuremath{\mathbb{Z}}\]$ Water Level at Time of Drilling, or as Shown
- ▼ Water Level at End of Drilling, or as Shown

NV	No Value
NP	Non-Plastic

▼ Water Level After 24 Hours, or as Shown

NOTES

1. Test holes were drilled on 11/5/2019 with 4" solid stem auger.

2. Locations of the test holes were determined approximately by pacing from features shown on the site plan provided.

3. Elevations of the test holes were not measured and the logs of the test holes are drawn to depth. Nominal elevation of "100 feet" indicates existing ground level at the test hole at the time of drilling.

4. The test hole locations and elevations should be considered accurate only to the degree implied by the method used.

5. The lines between materials shown on the test hole logs represent the approximate boundaries between material types and the transitions may be gradual.

6. Groundwater level readings shown on the logs were made at the time and under the conditions indicated. Fluctuations in the water level may occur with time.

7. The material descriptions on these logs are for general classification purposes only. See full text of this report for descriptions of the site materials & related information.

8. All test holes were immediately backfilled upon completion of drilling, unless otherwise specified in this report.

Figure #3



Client: Real Investments, LLC

Project No.: 19-0040

Erie Air Park

Lot E-2

	TABLE 1: SUMMARY OF LABORATORY TEST RESULTS														
Sample	Location			(Gradatio	n	Atterbe	rg Limits	Swell/0	Collapse	Unco	nfined		AASHTO	
Test Hole	Depth	Natural Moisture Content	Natural Dry Density	Gravel	Sand	Fines	Liquid Limit	Plasticity Index	Change	Surcharge	•	ressive ngth	USCS Equivalent Classification	Equivalent Classification (Group Index)	Sample Description
No.	(feet)	(%)	(pcf)	(%)	(%)	(%)			(%)*	(psf)	(psi)	(ksf)		(Group maex)	
TH-1	4	10	118	-	-	64.5	30	21	3.4	500	-	-	s(CL)	A-6 (10)	Fill: sandy CLAY
TH-1	9	9.8	121.8	-	-	67.3	34	15	-	-	-	-	s(CL)	A-6 (8)	Fill: sandy CLAY
TH-2	10	14.3	118.7	-	-	91.9	54	27	7.1	1000	-	-	СН	A-7-6 (28)	FAT CLAY
TH-3	3	7.3	SD	-	-	49.7	NV	NP	-	-	•	-	SM	A-4 (0)	Fill: silty SAND
TH-3	8	10.3	124.2	-	-	82.8	50	28	6.9	1000	-	-	(CL)s	A-7-6 (24)	CLAY with sand
TH-4	4	11.1	120.5	-	-	77.2	47	20	7.2	500	-	-	(CL)s	A-7-6 (16)	CLAY with sand
TH-4	24	18	111.7	-	-	94.7	65	33	-	-	97.6	14.05	СН	A-7-5 (38)	Claystone Bedrock
TH-5	7	11.4	124.1	-	-	87.1	46	26	-	-	273	39.31	CL	A-7-6 (24)	CLAY
TH-5	12	17.8	107.6	-	-	77.6	60	30	8.1	1500	-	-	(CH)s	A-7-5 (25)	Clayestone Bedrock
TH-5	17	10.1	128.5	-	-	86.0	41	21	1.5	2000	-	-	CL	A-7-6 (18)	Claystone Bedrock

*Negative indicates collapse, SD = Sample disturbed, NV = No value, NP = Non-plastic



Client: Real Investments, LLC

Project No.: 19-0040

Erie Air Park

Lot E-2

TABLE 2: SUMMARY OF SOIL CORROSION TEST RESULTS													
Sample	Location	Water		Redox		Resistivity	116.65	AASHTO					
Test Hole No.	Depth (feet)	Soluble Sulfates (%)	рН	Potential (mV)	Sulfide Reactivity*	(ohm-cm)	USCS Equivalent Classification	Equivalent Classification (Group Index)	Sample Description				
TH-3	2	0.05	8.8	-97.0	Positive	1,950	SM	A-4 (0)	Silty SAND				

*Performed by eAnalytics Laboratory.

Appendix A Detailed Drill Logs



PAGE 1 OF 1

CLIENT: Marketwise, LLC

JOB N	IO .: <u>1</u>	9-0040		PRO	JECT L	OCATIO	DN: _Er	ie, CO					
E		Бо		,be	t	sture %)	cf)	ssing eve	Atte Lir	rberg nits	idation large ssf)	ed ive	
Elevation (#)	Depth (ff)	Graphic Log	Material Descriptions and Drilling Notes	Sample Type	Blow Count	Natural Moisture Content (%)	Natural Dry Density <i>(pcf)</i>	Percent Passing No. 200 Sieve	Liquid Limit	Plasticity Index	Swell/Consolidation (%) at Surcharge Pressure (<i>psf</i>)	Unconfined Compressive Strength <i>(kst</i>)	NSCS
100	0	<u>x11x x11x x1</u>	TOPSOIL								ο –		
	 		FILL: Predominantly sandy clay with some local gravel and claystone materials, were medium to highly plastic, fine grained with trace gravel, dry to moist, and red-brown to gray-brown to brown in color with iron staining.										
_ 95	5				30/12	10.0	118.0	65	30	21	3.4 @ 500		CL
_ 90	10				27/12	9.8	121.8	67	34	15			CL
			CLAY: Sandy, medium plastic, fine grained, dry to slightly moist, hard, and gray-brown in color with iron staining and local caliche staining.										
 <u>85</u> 	_ <u>15</u> 				38/12								
 - 80 	 		FAT CLAY : Highly plastic, fine grained, slightly moist to wet, medium stiff to hard, and gray-brown in color with iron staining an local caliche staining.	_									
 					13/12								
	<u>30</u>		Groundwater encountered at 33 feet.										
 65	35				8/12								
	00		Bottom of borehole at Approx. 35 feet.			1	1						



PAGE 1 OF 1

CLIENT: Marketwise, LLC

JOBN	IO .: <u>1</u>	9-0040		PRO	JECT L	ОСАТК	DN: _Er	ie, CO					
00 Elevation (ft)	o Depth (ff)	Graphic Log	Material Descriptions and Drilling Notes	Sample Type	Blow Count	Natural Moisture Content (%)	Natural Dry Density (<i>pcf</i>)	Percent Passing No. 200 Sieve	Lidnid Limit	Plasticity Index Index	Swell/Consolidation (%) at Surcharge Pressure (<i>psf</i>)	Unconfined Compressive Strength (ksf)	nscs
		<u></u>	TOPSOIL										
 <u>95</u>	 _ 5		CLAY : Sandy, medium plastic, fine grained, dry to slightly moist, hard, and gray-brown in color with iron staining and local caliche staining.		23/12	_							
					20/12								
			FAT CLAY : Highly plastic, fine grained, slightly moist to wet, medium stiff to hard, and gray-brown in color with iron staining an local caliche staining.	_									
_ 90 _	10				41/12	14.3	118.7	92	54	27	74 @ 4000		СН
 <u>85</u>	 15				41/12	14.3	110.7	92	34	21	7.1 @ 1000		
 <u>80</u> 	20				33/12	-							
 	25 25 25 25		Groundwater encountered at 27 feet 1 hour after drilling. Groundwater encountered at 27 feet.										
 - 70 	 												
	35		SAND and GRAVEL: Clayey and fine to coarse grained with gravel, medium plastic, wet, medium dense to dense, and gray brown in color.		2-11- 20	-							

Bottom of borehole at Approx. 37 feet.



PAGE 1 OF 1

CLIENT: Marketwise, LLC

JOB N	IO .: _1	9-0040		PRO	JECT L	OCATIO	DN: _Er	ie, CO			1		I
uo	F	Log		[ype	ount	oisture (%)	Dry (pcf)	assing Sieve	Lii	erberg mits	olidation charge (<i>psf</i>)	ned ssive th	0
Elevation (ff)	Depth (ff)	Graphic Log	Material Descriptions and Drilling Notes	Sample Type	Blow Count	Natural Moisture Content (%)	Natural Dry Density (<i>pcf</i>)	Percent Passing No. 200 Sieve	Liquid Limit	Plasticity Index	Swell/Consolidation (%) at Surcharge Pressure (<i>psf</i>)	Unconfined Compressive Strength (<i>kst</i>)	nscs
100	0	<u>ZIN. ZIN. Z</u>	TOPSOIL								ى ا		
· _	-		FILL: Predominantly sandy clay with some local gravel and claystone materials, were medium to highly plastic, fine grained with trace gravel, dry to moist, and red-brown to gray-brown to brown in color with iron staining.		17/10		0.5	50			-		
95 _	5		CLAY: Sandy, medium plastic, fine grained, dry to slightly moist, hard, and gray-brown in color with iron staining and local caliche staining.		17/12	7.3	SD	50	NV	NP	-		SM
90	_ 10				42/12	10.3	124.2	83	50	28	6.9 @ 1000		CL
· -	-				42/12								
85	_ 15												
80	20		FAT CLAY : Highly plastic, fine grained, slightly moist to wet, medium stiff to hard, and gray-brown in color with iron staining an local caliche staining.										
75	_ 25				8/12								
	35		Bottom of borehole at Approx. 36 feet.		19/12								



PAGE 1 OF 1

CLIENT: Marketwise, LLC

JOB N	IO.: 1	9-0040		PRO	JECT L	OCATIO	DN: _Er	ie, CO					
Elevation 0 (ff)	o Depth (ff)	Graphic Log	Material Descriptions and Drilling Notes	Sample Type	Blow Count	Natural Moisture Content (%)	Natural Dry Density (<i>pcf</i>)	Percent Passing No. 200 Sieve	Liquid Limit	Blasticity Index Index	Swell/Consolidation (%) at Surcharge Pressure (<i>psf</i>)	Unconfined Compressive Strength <i>(kst)</i>	NSCS
			TOPSOIL	-									
	 		CLAY: Sandy, medium plastic, fine grained, dry to slightly moist, hard, and gray-brown in color with iron staining and local caliche staining.										
95	5				44/12	11.1	120.5	77	47	20	7.2 @ 500		CL
					49/12								
<u>90</u> 													
 			CLAYSTONE BEDROCK: Slightly sandy, fine grained, dry to moist, moderately to highly plastic, medium hard to very hard and resistant, and gray-brown in color with iron staining.		37/12								
_ 80 	20												
 					43/12	18.0	111.7	95	65	33		14.05	СН
 	30												
			Bottom of borehole at Approx. 34 feet.		50/1								



PAGE 1 OF 1

CLIENT: Marketwise, LLC

JOB N	IO.: _1	9-0040		PRO	JECT L	-	DN: _Er						
ion	£.	Log		Type	ount	oisture : (%)	Dry (pcf)	assing Sieve	Liı	rberg nits	olidation charge : (<i>psf</i>)	ined ssive jth	S
Elevation (#)	Depth (ft)	Graphic Log	Material Descriptions and Drilling Notes	Sample Type	Blow Count	Natural Moisture Content (%)	Natural Dry Density (<i>pcf</i>)	Percent Passing No. 200 Sieve	Liquid Limit	Plasticity Index	Swell/Consolidation (%) at Surcharge Pressure (<i>psf</i>)	Unconfined Compressive Strength (kst)	nscs
100	0	<u>21 12 </u>									ο Ο		
	L -		TOPSOIL FILL: Predominantly sandy clay with some local	_									
			gravel and claystone materials, were medium to highly plastic, fine grained with trace gravel, dry to moist, and red-brown to gray-brown to brown in color with iron staining.		46/12								
95	5		×										
			CLAY: Sandy, medium plastic, fine grained, dry to slightly moist, hard, and gray-brown in color with iron staining and local caliche staining.										
					37/12	11.4	124.1	87	46	26		39.31	CL
90	10												
			CLAYSTONE BEDROCK : Slightly sandy, fine grained, dry to moist, moderately to highly plastic, medium hard to very hard and resistant, and gray-brown in										
			color with iron staining.		35/12	17.8	107.6	78	60	30	8.1 @ 1500		СН
85	15												
					50/6	10.1	128.5	. 86	_41	_21_	1.5 @ 2000		CL
80	20												
75	25												
					50/12								
		,, <i>t</i>	Bottom of borehole at Approx. 28 feet.										1

PHASE III DRAINAGE REPORT

LOT 1 ERIE AIR PARK REPLAT D

Erie, Colorado

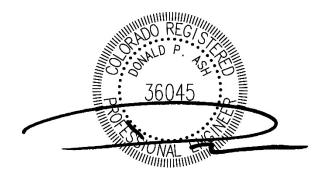
October 11, 2019 (Revised June 5, 2020) (Revised January 8, 2021) (Revised May 21, 2021)

Prepared for:

Nassar Development/ Real Investments, LLC

ENGINEER'S STATEMENT

I hereby certify that this **Phase III Drainage Report** for the design of the **Lot 1 Erie Air Park Replat D** was prepared by me (or under my direct supervision) in accordance with the provisions of the Town of Erie Standards and Specifications for Design and Construction for the owners thereof. I understand that the Town of Erie does not and will not assume liability for drainage facilities designed by others, including the designs presented in this report.



Donald P. Ash Registered Professional Engineer State of Colorado No. 36045

TOWN ACCEPTANCE

This report has been reviewed and found to be in general compliance with the Town of Erie Standards and Specifications for Design and Construction and other Town requirements. THE ACCURACY AND VALIDITY OF THE ENGINEERING DESIGN, DETAILS, DIMENSIONS, QUANTITIES, AND CONCEPTS IN THIS REPORT REMAINS THE SOLE RESPONSIBILITY OF THE PROFESSIONAL ENGINEER WHOSE STAMP AND SIGNATURE APPEAR HEREON.

Accepted By:

Town Engineer

Date

TABLE OF CONTENTS

<u>Page</u>

I.	GENERAL LOCATION AND DESCRIPTION
11.	DRAINAGE BASINS
III.	 DRAINAGE DESIGN CRITERIA
IV.	DRAINAGE FACILITY DESIGN
۷.	SUMMARY
VI.	REFERENCES12
VII.	APPENDICES A. DRAINAGE PLAN B. HYDROLOGIC CALCULATIONS C. WATER QUALITY CALCULATIONS D. HYDRAULIC CALCULATIONS E. RELEVANT DOCUMENTS

I. GENERAL LOCATION AND DESCRIPTION

A. <u>Location</u>

- 1. This report is submitted as the Phase III Drainage Report of the existing and proposed conditions for Lot 1 Erie Air Park Replat D, located at the Erie Air Park, in the Town of Erie.
- 2. The site is located in the Southwest 1/4 of Section 31, Township 1 North, Range 68 West of the 6th Prime Meridian, in the Town of Erie, Weld County, State of Colorado.
- 3. Major Drainage Facilities This site is located within the Town of Erie Outfall Systems Plan (OSP) prepared by Love & Associates, Inc dated 2007. Coal Creek is located directly north and west of the subject property.
- 4. The site is bounded by Coal Creek to the north, an existing light industrial development to the east, Airport Drive and an undeveloped property to the south and an existing aircraft hangar facility to the west. A Vicinity Map is included with this report.
- B. <u>Description of Property</u>
- 1. The existing 10.340-acre site is currently undeveloped.
- 2. Existing ground cover consists of native grasses. There are numerous trees located along Airport Drive and the south side of the site. These trees were recently planted by the current owner concurrently with the recent development to the east.

The majority of the site generally slopes to the north at an approximate slope of 2%. The eastern half of the lot drains east and north. The western half of the lot drains west and north. Existing drainage patterns are shown on the Drainage Plan that is included with this report.

The United States Department of Agriculture (USGS) Natural Resources Conservation Service (NRCS) Soil Survey for the site identifies the existing site soils as Midway-Shingle Complex, Ulm Clay Loam and Colombo Clay Loam with a hydrologic soil group of C and D.

- 3. Coal Creek is located directly north of the subject property.
- 4. The project will consist of five (5) light industrial buildings, with associated driveway, parking and landscaping improvements.
- 5. There are no irrigation facilities located on or near the site.
- 6. The proposed land use will be light industrial. A Planned Unit Development (PUD) Zoning overlay will control the specific zoning on the subject property.
- 7. There are no wetland areas located on the property. Coal Creek is located directly north of the site and is not affected by the proposed improvements.

8. There is a drainage easement located along the north side of the property. This easement is for the conveyance of drainage from Tract E-1. There is also a 30' utility easement that runs through the center of the site. These existing easements will be unaffected by the proposed improvements.

II. DRAINAGE BASINS

A. <u>Major Basin Description</u>

- Based on the FEMA Flood Insurance Rate Map (FIRM) Map Number 08013C0443K dated August 15, 2019, portions of the site are located within Zone X (Shaded) areas of the 500-year floodplain. The rest of the site is located with Zone X.
- 2. There are no irrigation facilities located on or near the site.
- 3. There are no lakes or ponds which influence or may be influenced by the local drainage. There are no dams on or adjacent to the subject property. There is one (1) existing water quality pond located at the north west corner of the site, which provides water quality for Lot 1 Erie Air Park Replat D and Lot 2 Erie Air Park Replat A.
- 4. There are no irrigation ditches or facilities which will be affect by the proposed development.
- B. <u>Sub-Basin Description</u>
- 1. For the purposes of this report, the existing site has been broken into two (2) historic sub-basins.

Basin HA1 consists of the western half of the undeveloped site. Runoff within this basin is conveyed via overland flow towards the west and north, to the northwest corner of the site, and then east into the existing water quality pond. The proposed drainage Swale HA-1 located along the west and north property lines will direct water into the pond. The runoff is then released through a water quality release structure, where is it conveyed underneath of the existing taxiway and eventually discharges into Coal Creek.

Basin HA2 consists of the eastern half of the undeveloped site. Runoff within this basin is conveyed via overland flow towards the east and north, to the northeast corner of the site, and then north into the existing water quality pond. The proposed drainage Swale HA-2 located along the east property line will direct water north into the pond. The runoff is then released through a water quality release structure, where is it conveyed underneath of the existing taxiway and eventually discharges into Coal Creek.

2. There are five (5) offsite drainage basins that affect the site.

Drainage from Basin OS1 consists of a portion of the undeveloped land south of the site known as Tract D, which is located south and east of Airport Drive, north of Baseline Road. This drainage is conveyed via overland flow and into the roadside drainage swale that is located along the east and south sides of Airport Drive. The offsite drainage is then conveyed north through a 24" corrugated metal pipe (CMP) culvert underneath of Airport Drive. The runoff is then conveyed through a drainage swale which is located along the east side of Tract E-1. The drainage is then conveyed underneath of the existing taxiway through another 24" CMP culvert, where it flows north and eventually discharges into Coal Creek.

Drainage from Basin OS2 consists of the northern portion of Airport Drive. This drainage is conveyed via overland flow and into the existing drainage swale that is located along the east side of Tract E-1. The drainage is then conveyed underneath of the existing taxiway through another 24" CMP culvert, where it flows north and eventually discharges into Coal Creek.

Drainage from Basin OS3 through OS5 consists of the northern portions of Airport Drive located adjacent to and directly south of the subject property. This drainage is conveyed via overland flow and into Basin A. Drainage is then conveyed north where it drains into the existing water quality pond.

Drainage from Basin C1 consists of the developed land east of the site, including a portion of Lot 2 Erie Air Park Subdivision Replat A. This drainage is conveyed via overland flow and into the offsite drainage system on Lot 2. The runoff is then conveyed through a 24" CMP storm sewer, underneath of the existing taxiway, and into the existing water quality pond. This pond was designed as part of the Lot 2 development and has been sized to accept the offsite drainage from this basin.

The roof drainage from Basin C1 has been collected in an existing storm sewer system, which is located along the east side of the site. PVC roof drains from Lot 2 Erie Air Park Subdivision Replat A is connected to this system, which is conveyed north and into the existing water quality pond.

Drainage from Basin B1 consists of the eastern portions of the developed land west of the site, including portions of Tract E-1 Erie Air Park Tract E Minor Subdivision. This basin includes the hangar buildings, apron and site improvements. This drainage is conveyed via overland flow into the drainage swale which is located on the east side of Tract E-1. The drainage is then conveyed underneath of the existing taxiway through the 24" CMP culvert, where it flows north and eventually discharges into Coal Creek. The existing drainage patterns from this offsite basin will continue to drain through the subject property during developed conditions. This offsite runoff will be unaffected by the proposed development.

3. The runoff from the existing site is summarized in Table 1. Existing runoff calculations have been included in Appendix B.

III. DRAINAGE DESIGN CRITERIA

A. <u>Development Criteria Reference and Constraints</u>

- 1. There are no previous drainage master plans or drainage studies that influence or are influences by the proposed drainage facilities.
- 2. There is one (1) previous study that has been completed for the site. The "Final Drainage Report for the Erie Convair Hangar Complex" was prepared by Scott, Cox & Associates, Inc. (SCA Report) dated March 23, 2009 and contains the overall site drainage and water quality requirements for both Lot 2 Erie Air Park Replat A and the subject property.
- 3. The site drainage was generally constrained by the adjacent developments. Grading was constrained by the existing grades along the east and west property lines. The site was also constrained by the existing curb and gutter elevations along Boxelder Street, and the existing grades along the north property line.
- 4. There are no wetland areas located on the property. Coal Creek is located directly north of the site and is not affected by the proposed improvements.
- 5. The following reports, files and drawings form the basis of this report: 1) Town of Erie Unified Development Code (UDC); 2) Town of Erie Standards and Specifications for Design and Construction of Public Improvements (STANDARDS); and 3) Mile High Flood District (MHFD) Urban Storm Drainage Criteria Manual, Volumes 1-3 (USDCM). Relevant sections, as required, can be found in the Appendix located at the back of this report.
- 6. This drainage plan is in general conformance with the Town Standards and Specifications, the MHFD Storm Drainage Criteria Manual and the Outfall Systems Plan.
- B. <u>Hydrological Criteria</u>
- 1. The design rainfall data used in this study was taken from the STANDARDS, Section 813.06 – Rainfall Intensity Duration Curves for the Town of Erie. Onehour rainfall depth was taken from Table 800-2 and used in conjunction with the intensity equation listed under Section 813.06.

As required in the STANDARDS, for all land uses, hydrologic information was developed for an initial storm return period of 5-years and major storm return period of 100-years. The criteria and methodology used in determining the storm runoff peaks and volumes were those outlined in the USDCM as directed by the STANDARDS.

2. Runoff calculations were obtained using the Rational Method as outlined in the Manual for basins having less than 130 acres.

Rational Formula is:

Q = CIA

Where: Q = Peak Discharge (cfs) C = Runoff Coefficient (USDCM) I = Rainfall Intensity (in/hr) (USDCM) A = Drainage Basin Tributary Area (acres)

C. <u>Hydraulic Criteria</u>

- 1. The entire site drains north into the Coal Creek major drainageway. The major drainageway has the ability to handle the drainage from the subject property.
- 2. Storm sewer systems have been designed using the Autodesk Storm and Sanitary Sewer Analysis. Storm sewer plans, calculations and profiles have been included for the 5 and 100-year storm events. Storm sewer inlets have been designed using the MHFD street and inlet worksheets.
- 3. Water quality volumes, discharges and storage calculations are based on the USDCM Volume 2, Storage. Water quality facilities have been designed in accordance with the USDCM Volume 3, Best Management Practices. The UDFCD detention worksheets were used for calculations of the detention and water quality facilities.

D. <u>Adaptions from Criteria</u>

1. There are no adaptions or variances requested from the Criteria.

IV. DRAINAGE FACILITY DESIGN

- A. <u>General Concepts</u>
- 1. The site is currently undeveloped.
- 2. Proposed swales and drainage facilities have been designed in order to convey existing drainage to the existing stormwater quality facility.

- 3. Future development of the subject property would likely consist of a series of storm inlets, which would be designed to conveyed developed runoff to the existing stormwater quality facility located on the north east corner of the site.
- 4. The existing drainage patterns from offsite basin will continue to drain through the subject property during developed conditions. This offsite runoff will be unaffected by the proposed development.
- 5. Proposed drainage patterns are shown on the Drainage Plan. Proposed runoff calculations for Basin A have also been enclosed in Appendix B. Proposed runoff from the site is shown in Table 1.
- 6. The proposed stormwater quality facilities have been designed in accordance with the previously referenced SCA Report.
- B. <u>Specific Details</u>
- 1. The Drainage Plan shows the proposed Site Plan, on-site grading and overland flow directions. Under the proposed conditions, the site will be broken into two (2) sub-basins.

Basin A-1 consists of the western half of the undeveloped site. Runoff within this basin is conveyed via overland flow towards the west and north, to the northwest corner of the site, and then east into the existing water quality pond. The proposed drainage Swale HA-1 located along the west and north property lines will direct existing drainage into the pond. The runoff is then released through a water quality release structure, where is it conveyed underneath of the existing taxiway and eventually discharges into Coal Creek.

Basin A-2 consists of the eastern half of the undeveloped site. Runoff within this basin is conveyed via overland flow towards the east and north, to the northeast corner of the site, and then north into the existing water quality pond. The proposed drainage Swale HA-2 located along the east property line will direct existing drainage into the pond. The runoff is then released through a water quality release structure, where is it conveyed underneath of the existing taxiway and eventually discharges into Coal Creek.

Drainage from Basin C1 consists of the developed land east of the site, including a portion of Lot 2 Erie Air Park Subdivision Replat A. This drainage is conveyed via overland flow and into the offsite drainage system on Lot 2. The runoff is then conveyed through a 24" CMP storm sewer, underneath of the existing taxiway, and into the existing water quality pond. This pond was designed as part of the Lot 2 development and has been sized to accept the offsite drainage from this basin.

The roof drainage from Basin C1 (Basins C1-1 thought C1-4) will be collected in the proposed 18" storm sewer system, which is located adjacent to the existing taxiway located on the east side of the site. The existing PVC roof drains from Lot 2 Erie Air Park Subdivision Replat A will be connected to the proposed system, which will be conveyed north and into the existing water quality pond.

The existing and proposed conditions for the entire site were analyzed for the 5 and 100-year storm events. The results are shown in the following Table 1 and the relevant calculation sheets are provided in Appendix B.

Drainage Basin	Design Point	Area	C₅	C100	5-Year Peak Runoff (cfs)	100-Year Peak Runoff (cfs)
HA1	1	6.659	2.40	5.78	0.05	0.49
HA2	1	3.682	2.48	5.98	0.05	0.49
A1	1	6.659	2.40	5.78	0.69	0.81
A2	1	3.682	2.48	5.98	0.69	0.81
B1	3	11.808	2.22	5.35	0.51	0.72
B2	2	2.340	2.42	5.83	0.44	0.68
B3	3	1.856	2.82	6.81	0.29	0.61
C1	1	5.170	2.51	6.05	0.69	0.81
C1-1	1	0.436	3.76	9.09	0.77	0.85
C1-2	1	0.689	3.76	9.09	0.77	0.85
C1-3	1	0.574	3.76	9.09	0.77	0.85
C1-4	1	0.689	3.76	9.09	0.77	0.85
C1-5	1	0.574	3.76	9.09	0.77	0.85
OS1	4	10.453	1.70	4.10	0.05	0.49
OS2	4	0.372	3.63	8.76	0.85	0.89
OS3	5	0.081	3.76	9.09	0.85	0.89
OS4	5	0.175	3.76	9.09	0.85	0.89
OS5	5	0.065	3.76	9.09	0.85	0.89

TABLE 1 RUNOFF CALCULATIONS SUMMARY

Onsite storm drainage conforms to the Drainage Study and Plan required per the SCA Report. There are no impacts to the existing storm sewer infrastructure or the major drainage conveyance into Coal Creek.

- 2. The proposed drainage swales will direct existing runoff to the existing water quality pond.
- 3. The existing storm sewer located along the east side of the site currently conveys the roof drainage from Lot 1 Erie Air Park Replat A. Roof downspouts are connected to the existing PVC pipe at various locations. The pipe will be removed and replaced, as required, in order to facilitate building improvements on the subject property. This work may be phased concurrent with the building construction to be located on the subject property.
- 4. Future developed runoff from the proposed site and building improvements will be directed into the proposed water quality pond that is located at the north east corner of the site. Details of this plan will be submitted during the Site Plan Review process and will be subject to a subsequent Phase III Drainage Report.
- 5. As noted in the SCA Report, the runoff for the initial and major storm events from the tributary basin can be conveyed directly to the major drainage system without adversely impacting upstream, surrounding, or downstream properties and facilities. Due to the location of the site relative to the floodplain, the site was previously approved for providing only water quality for the proposed developed areas. No detention is proposed for this site.

A water quality pond has been designed to provide the recommended structural Best Management Practices (BMPs) outlined in the Mile High Flood District (MHFD), Urban Storm Drainage Criteria Manual, Volume 3. The calculations for the water quality pond and the limited release structure are enclosed in Appendix C. In addition, sections and details for the pond and limited release outlet structure are shown on the enclosed plan. This pond has been designed to accommodate the anticipated water quality requirements for the developed conditions of both Basins A and C1.

A limited release orifice plate provides the required 40-hour drain time for the water quality capture volume. The orifice plate meets the requirements for an Extended Detention Basin and the 40-hour drain time as specified in the MHFD Manual.

We have updated the water quality plans and calculations based on current Town STANDARDS. We used the new MHFD Detention spreadsheet to recalculate the required pond volume. The required pond volume has actually decreased slightly, largely due to changes that were made to the assumed basin area in 2009 SCA report, and changes in the WQCV formula. The required pond volume has been reduced from 36,645 CF to 25,700 CF. The pond was surveyed in 2018. The as-built contour elevations were used in the pond analysis. The new water quality volume provided will be 42,917 CF.

The imperviousness used in the previous WQ pond design was 95%. The Town of Erie Light Industrial imperviousness per Table 800-3 is 80%. Therefore, the pond is slightly overdesigned and will accommodate subsequent land use changes. Rainfall data was updated based on the current Town of Erie One-Hour Rainfall Depth per Table 800-2.

The existing outlet structure will be sufficient for the proposed use. Although the holes in the existing perforated plate were slightly smaller than required to allow for the 40 hour drain time used on the new MHFD spreadsheet. This might have been due to calculation differences between the different spreadsheets. Regardless, we are proposing to modify the existing perforated plate to provide a higher drain time. New 1" diameter holes will be drilled into the existing 3/4" holes in order to meet current standards.

The adjacent taxiway and roadways around the pond will provide approximately 1.0 feet of freeboard above the WQCV water surface elevation. In the event the pond was to overflow, the flow is directed to overtop at the outlet structure and spill north and east across the existing taxiway and directly into the Coal Creek drainageway. The spillway is sized to convey two times (2X) the runoff from the full basin developed conditions during the 100-year storm from the basin.

		Releas	e Rate	Volu	vired	Water Surface Elevation				
Pond	Basin Area (ac)	EURV (CFS)	100-yr (CFS)	WQCV (CF)	EURV (CF)	100-yr (CF)	WQCV WSEL (FT)	EURV WSEL (FT)	100-yr WSEL (FT)	
А	15.82	n/a	n/a	25,853	n/a	n/a	5094.0	n/a	n/a	

TABLE 2 WATER POND SUMMARY

6. Maintenance of the water quality pond will be provided by the home owners association.

7. There is an existing drainage easement located on the north side of the site. This easement provides conveyance to the offsite drainage from Basins B1, OS1 and OS2. The drainage easement also includes the existing water quality facility. There are no other drainage easements needed for the proposed development.

- 8. By maintaining this WQCV, it is our conclusion that the runoff for the initial and major storm events from the tributary basin can be conveyed directly to the major drainage system without adversely impacting upstream, surrounding, or downstream properties and facilities.
- 9. The proposed drainage facilities will not impact the 100-year floodplain which is located adjacent to the site.

V. <u>SUMMARY</u>

A. <u>Compliance with Standards</u>

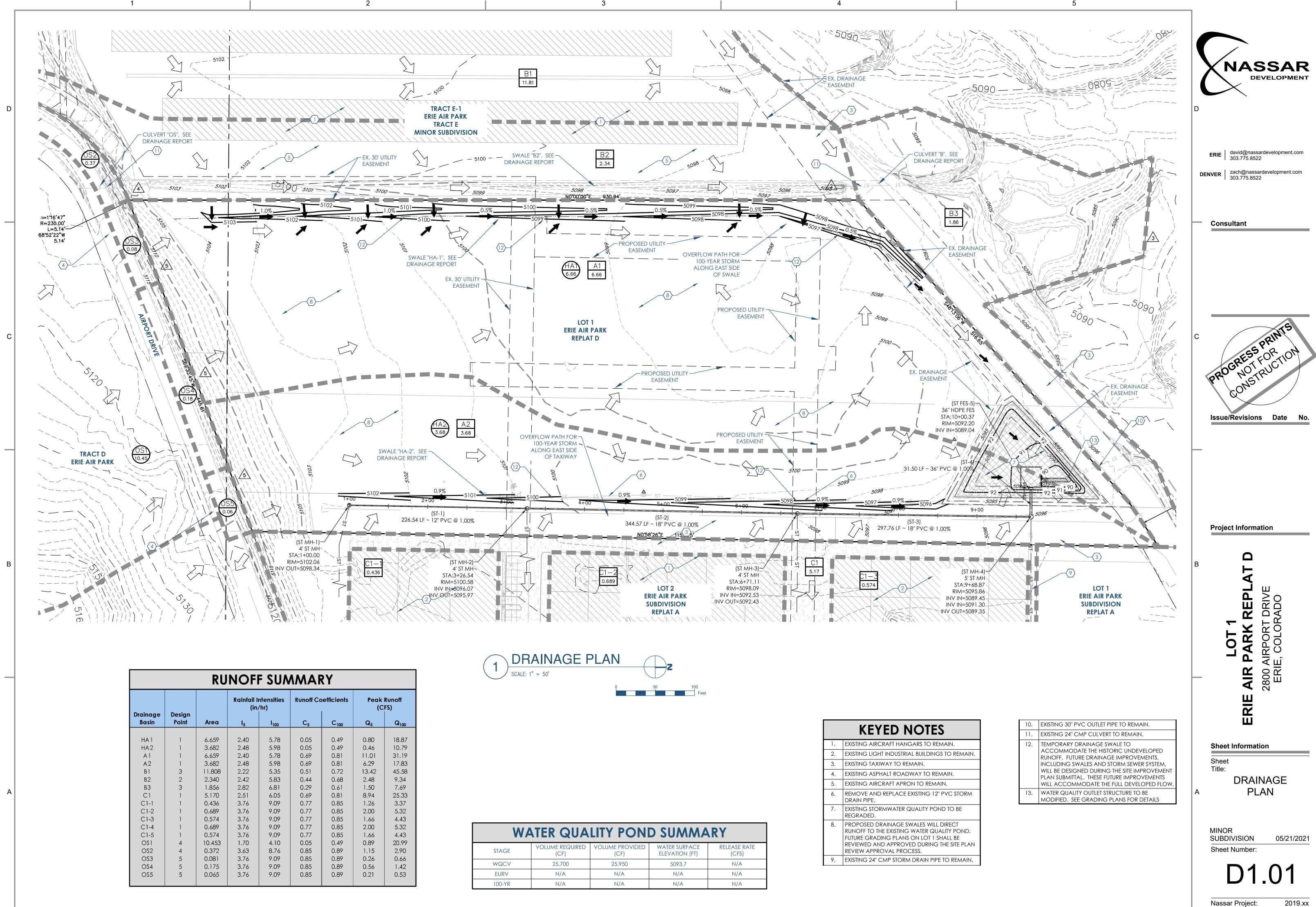
- 1. This drainage report and plan are in general conformance with the Town of Erie Standards and Specifications for Design and Construction of Public Improvements (STANDARDS).
- 2. This drainage report and plan are in general conformance with the Town of Erie Outfall Systems Plan.
- 3. This drainage report and plan are in general conformance with the Town of Erie Unified Development Code (UDC).
- 4. This drainage report and plan are in general conformance with the Mile High Flood District (MHFD) Urban Storm Drainage Criteria Manual.
- 5. This drainage report and plan are in general conformance with the "Final Drainage Report for the Erie Convair Hangar Complex" prepared by Scott, Cox & Associates, Inc. (SCA Report) dated March 23, 2009.
- B. <u>Drainage Concept</u>
- 1. The primary consideration for this project was to design a drainage plan to offset the impact of the proposed construction. The drainage plan accommodates on-site runoff and off-site flows. The proposed site grading and storm sewers will direct water towards the water quality facility. The drainage will not negatively affect any upstream or downstream properties.
- 2. Onsite storm drainage conforms to the SCA Report. There are no impacts to the existing storm sewer infrastructure in the Erie Air Park or the major drainage conveyance into Coal Creek.

VI. <u>REFERENCES</u>

- 1. Town of Erie Unified Development Code (UDC) dated December 2019.
- 2. Town of Erie Standards and Specifications for Design and Construction of Public Improvements dated January 2021.
- 3. Mile High Flood District (MHFD) Urban Storm Drainage Criteria Manual, Volumes 1-3, dated August 2018.
- 4. Final Drainage Report for the Erie Convair Hangar Complex prepared by Scott, Cox & Associates, Inc. (SCA Report) dated March 23, 2009.

APPENDIX A

DRAINAGE PLAN

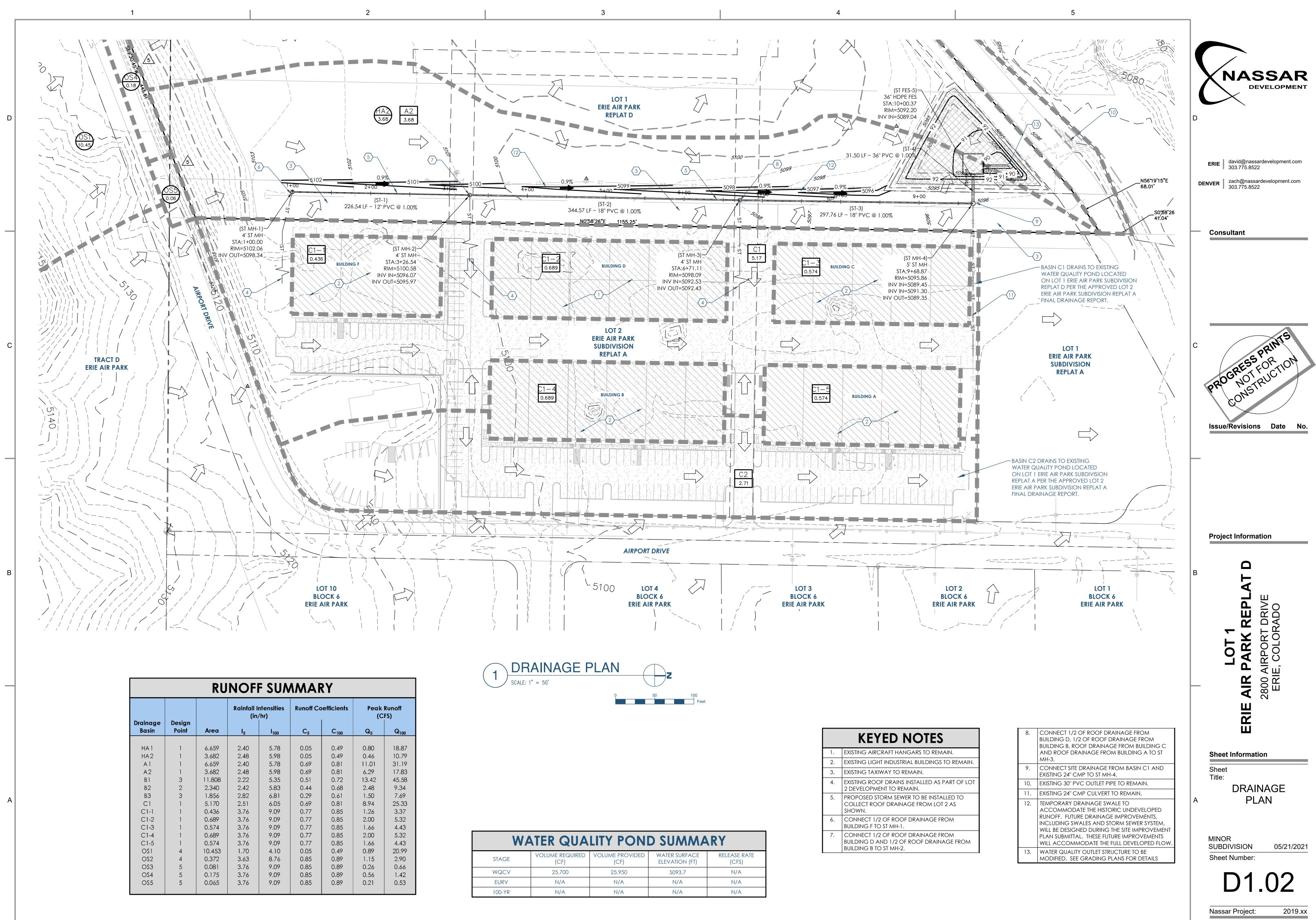


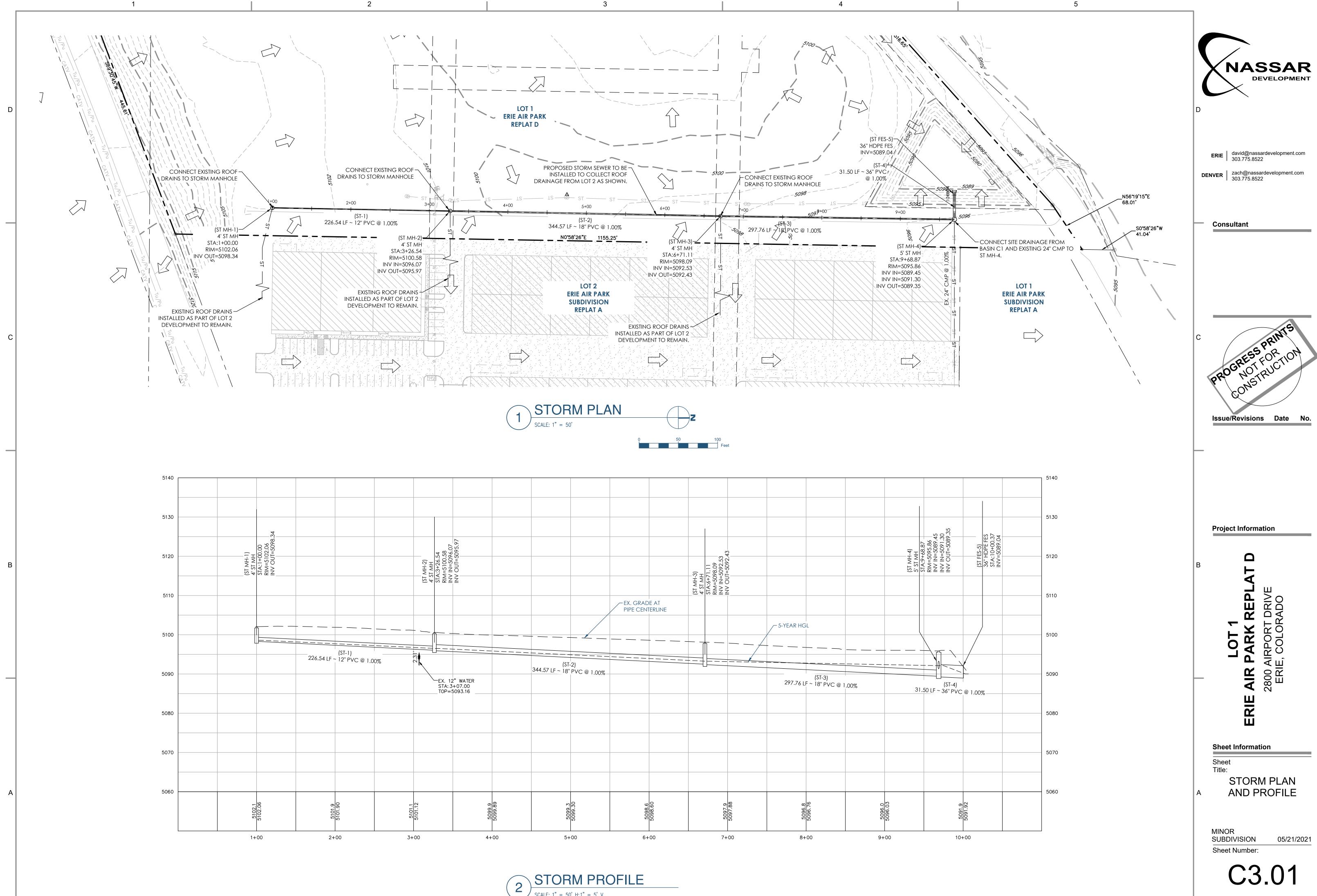
Drainage	Design			ntensities /hr)	Runoff Co	oefficients	Peak Runoff (CFS)		
Basin	Point	Area	ا ₅	I ₁₀₀	C₅	C ₁₀₀	Q_5	Q ₁₀₀	
HA 1	1	6.659	2.40	5.78	0.05	0.49	0.80	18.87	
HA2	1	3.682	2.48	5.98	0.05	0.49	0.46	10.79	
A 1	1	6.659	2.40	5.78	0.69	0.81	11.01	31.19	
A2	1	3.682	2.48	5.98	0.69	0.81	6.29	17.83	
B1	3	11.808	2.22	5.35	0.51	0.72	13.42	45.58	
B2	2	2.340	2.42	5.83	0.44	0.68	2.48	9.34	
BЗ	3	1.856	2.82	6.81	0.29	0.61	1.50	7.69	
C1	1	5.170	2.51	6.05	0.69	0.81	8.94	25.33	
C1-1	1	0.436	3.76	9.09	0.77	0.85	1.26	3.37	
C1-2	1	0.689	3.76	9.09	0.77	0.85	2.00	5.32	
C1-3	1	0.574	3.76	9.09	0.77	0.85	1.66	4.43	
C1-4	1	0.689	3.76	9.09	0.77	0.85	2.00	5.32	
C1-5	1	0.574	3.76	9.09	0.77	0.85	1.66	4.43	
OS1	4	10.453	1.70	4.10	0.05	0.49	0.89	20.99	
OS2	4	0.372	3.63	8.76	0.85	0.89	1.15	2.90	
OS3	5	0.081	3.76	9.09	0.85	0.89	0.26	0.66	
OS4	5	0.175	3.76	9.09	0.85	0.89	0.56	1.42	
OS5	5	0.065	3.76	9.09	0.85	0.89	0.21	0.53	

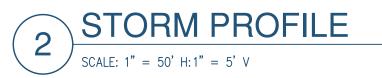
	KEYED
1.	EXISTING AIRCRAFT H
2.	EXISTING LIGHT INDUS
3.	EXISTING TAXIWAY TC
4.	EXISTING ASPHALT RC
5.	EXISTING AIRCRAFT A
6.	REMOVE AND REPLAC DRAIN PIPE.
7.	EXISTING STORMWATE REGRADED.
8.	PROPOSED DRAINAG RUNOFF TO THE EXISTI FUTURE GRADING PLA REVIEWED AND APPR REVIEW APPROVAL P
9.	EXISTING 24" CMP STO

STAGEVOLUME REQUIRED (CF)VOLUME PROVIDED (CF)WATER SURFACE ELEVATION (FT)RELEASE RATE (CFS)WQCV25,70025,9505093.7N/AEURVN/AN/AN/AN/A	WATER QUALITY POND SUMMARY						
	STAGE				-		
EURV N/A N/A N/A N/A	WQCV	25,700	25,950	5093.7	N/A		
	EURV	N/A	N/A	N/A	N/A		
100-YR N/A N/A N/A N/A	100-YR	N/A	N/A	N/A	N/A		

STAGE	
WQCV	
EURV	

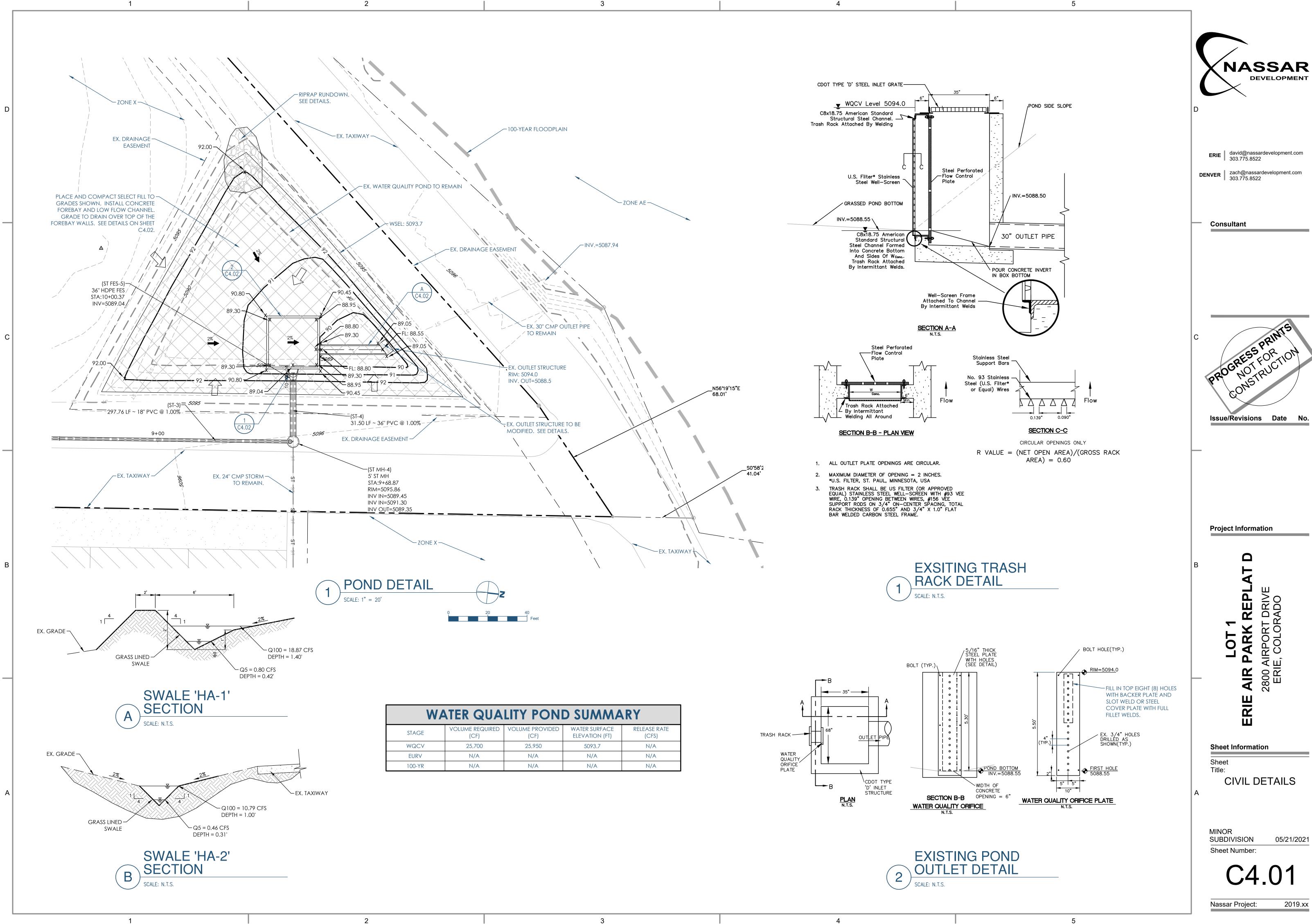




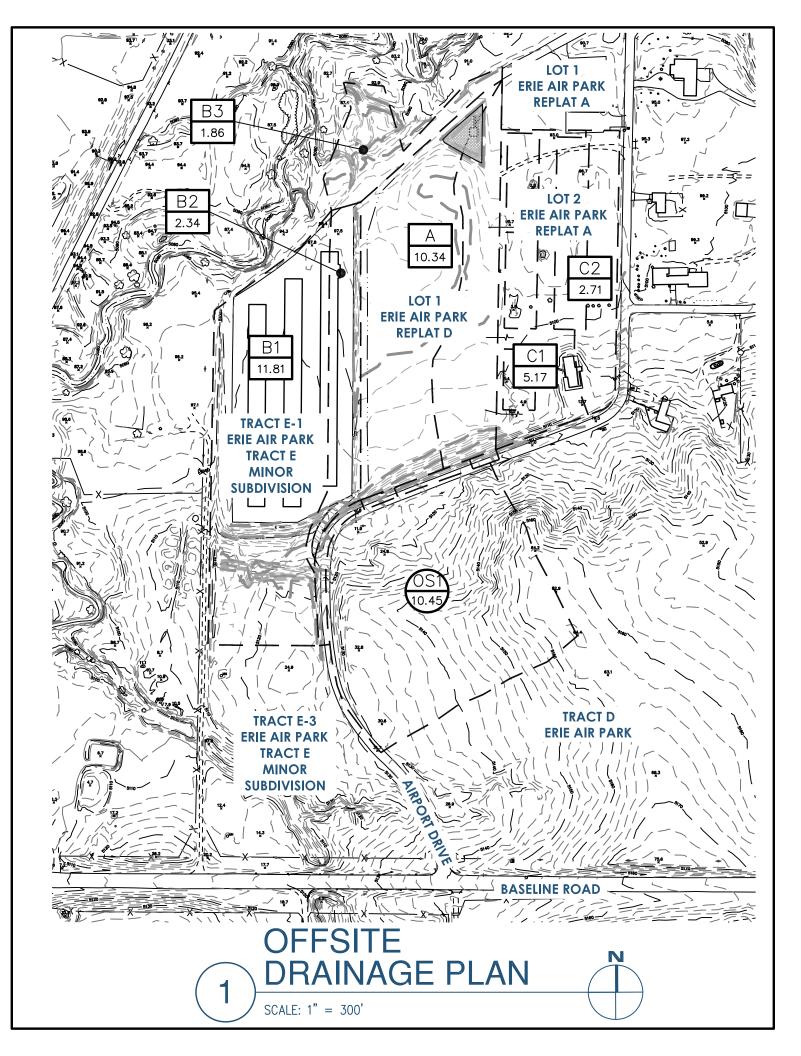


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Nassar Project:



WATER QUALITY POND SUMMARY							
STAGE	VOLUME REQUIRED (CF)	VOLUME PROVIDED (CF)	WATER SURFACE ELEVATION (FT)	RELEASE RATE (CFS)			
WQCV	25,700	25,950	5093.7	N/A			
EURV	N/A	N/A	N/A	N/A			
100-YR	N/A	N/A	N/A	N/A			



APPENDIX B

HYDROLOGIC CALCULATIONS

Runoff Summary

Lot 1 - Erie Airpark Replat D

2800 Airport Drive Erie, Colorado **Summary Sheet**

Project No: 1075 By: Dash Date: 05/21/21

Drainage	Design		Rainfall Intensities (in/hr)		Runoff Co	oefficients		Runoff FS)
Basin	Point	Area	I ₅	I ₁₀₀	C₅	C ₁₀₀	Q₅	Q ₁₀₀
	_							
HA1	1	6.659	2.40	5.78	0.05	0.49	0.80	18.87
HA2	1	3.682	2.48	5.98	0.05	0.49	0.46	10.79
A1	1	6.659	2.40	5.78	0.69	0.81	11.01	31.19
A2	1	3.682	2.48	5.98	0.69	0.81	6.29	17.83
B1	3	11.808	2.22	5.35	0.51	0.72	13.42	45.58
B2	2	2.340	2.42	5.83	0.44	0.68	2.48	9.34
B3	3	1.856	2.82	6.81	0.29	0.61	1.50	7.69
C1	1	5.170	2.51	6.05	0.69	0.81	8.94	25.33
C1-1	1	0.436	3.76	9.09	0.77	0.85	1.26	3.37
C1-2	1	0.689	3.76	9.09	0.77	0.85	2.00	5.32
C1-3	1	0.574	3.76	9.09	0.77	0.85	1.66	4.43
C1-4	1	0.689	3.76	9.09	0.77	0.85	2.00	5.32
C1-5	1	0.574	3.76	9.09	0.77	0.85	1.66	4.43
OS1	4	10.453	1.70	4.10	0.05	0.49	0.89	20.99
OS2	4	0.372	3.63	8.76	0.85	0.89	1.15	2.90
OS3	5	0.081	3.76	9.09	0.85	0.89	0.26	0.66
OS4	5	0.175	3.76	9.09	0.85	0.89	0.56	1.42
OS5	5	0.065	3.76	9.09	0.85	0.89	0.21	0.53

Lot 1 - Erie Airpark Replat D

2800 Airport Drive Erie, Colorado

Existing Conditions - West Side of Lot 1

Runoff Coefficents

(Ref. MHFD Table 6-4)

Project No: 1075 By: Dash Date: 05/21/21

Design Point= 1

NRCS Soil Type= C/D

Area	Imp.		Runoff Co	oefficient	5
(AC)	(%)	C ₂	C ₅	C ₁₀	C ₁₀₀
0.000	80%	0.65	0.69	0.72	0.81
0.000	100%	0.83	0.85	0.87	0.89
0.000	90%	0.74	0.77	0.79	0.85
0.000	90%	0.74	0.77	0.79	0.85
6.659	2%	0.01	0.05	0.15	0.49
6.659	2%	0.01	0.05	0.15	0.49
	(AC) 0.000 0.000 0.000 0.000 6.659	(AC) (%) 0.000 80% 0.000 100% 0.000 90% 0.000 90% 0.000 2%	(AC)(%)C20.00080%0.650.000100%0.830.00090%0.740.00090%0.746.6592%0.01	(AC) (%) C₂ C₅ 0.000 80% 0.65 0.69 0.000 100% 0.83 0.85 0.000 90% 0.74 0.77 0.000 90% 0.74 0.77 6.659 2% 0.01 0.05	(AC)(%)C2C5C100.00080%0.650.690.720.000100%0.830.850.870.00090%0.740.770.790.00090%0.740.770.796.6592%0.010.050.15

Time of Concentration

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Initial Overland Time († _i)	ti=0.395(1.1-C5)L1/2S-1/3	3 Travel Time (t_t)	t _t =L/(V*60)
Overland Flow (Lo) (ft)= Slope (ft/ft)= t _i (min)=	= 0.034	Length (ft)= Slope (ft/ft)= Cv= Velocity (ft/s)=	700 0.014 15 1.79
t_c Urbanized Check	t _c =(L/180)+10 (min)	t _t (min)=	6.51
Total Length (ft)= t _c (min)=		t _c Computed (t _i + t _t)= t _c Mininum= t_c Final (min)=	35.10 5.00 <u>16.67</u>

Rainfall Intensity (I)

(Ref. MHFD Volume 2, Section 5, Chapter 4 and Town of Erie Precipitation Data)

l₂ (in/hr)	l₅ (in/hr)	I ₁₀ (in/hr)	I ₁₀₀ (in/hr)
1.75	2.40	3.00	5.78

<u>Runoff (Q)</u>

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Q ₂ (cfs)	Q ₅ (cfs)	Q ₁₀ (cfs)	Q ₁₀₀ (cfs)
0.12	0.80	3.00	18.87

Basin HA1

Lot 1 - Erie Airpark Replat D

2800 Airport Drive Erie, Colorado

Existing Conditions - East Side of Lot 1

Runoff Coefficents

(Ref. MHFD Table 6-4)

Project No: 1075 By: Dash Date: 05/21/21

Design Point= 1

NRCS Soil Type= C/D

	Area	Imp.		Runoff Co	oefficient	5
Description	(AC)	(%)	C ₂	C ₅	C ₁₀	C ₁₀₀
Industrial - Light	0.000	80%	0.65	0.69	0.72	0.81
Streets - Paved	0.000	100%	0.83	0.85	0.87	0.89
Drive and walks	0.000	90%	0.74	0.77	0.79	0.85
Roofs	0.000	90%	0.74	0.77	0.79	0.85
Lawns, clayey soil	3.682	2%	0.01	0.05	0.15	0.49
TOTAL	3.682	2%	0.01	0.05	0.15	0.49

Time of Concentration

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Initial Overland Time (t_i)	ti=0.395(1.1-C5)L1/2S-1/3	3 Travel Time (t_t)	t _t =L/(V*60)
Overland Flow (Lo) (ft)= Slope (ft/ft)= t _i (min)=	= 0.034	Length (ft)= Slope (ft/ft)= Cv=	500 0.020 15
t _c Urbanized Check	t _c =(L/180)+10 (min)	Velocity (ft/s)= t _t (min)=	2.12 3.93
Total Length (ft)= t _c (min)=		t _c Computed (t _i + t _t)= t _c Mininum= t_c Final (min)=	32.52 5.00 <u>15.56</u>

Rainfall Intensity (I)

(Ref. MHFD Volume 2, Section 5, Chapter 4 and Town of Erie Precipitation Data)

l₂ (in/hr)	l₅ (in/hr)	I ₁₀ (in/hr)	I ₁₀₀ (in/hr)
1.81	2.48	3.10	5.98

<u>Runoff (Q)</u>

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Q ₂ (cfs)	Q ₅ (cfs)	Q ₁₀ (cfs)	Q ₁₀₀ (cfs)
0.07	0.46	1.71	10.79

Lot 1 - Erie Airpark Replat D

2800 Airport Drive Erie, Colorado

Proposed Conditions - West Side of Lot 1

Runoff Coefficents

Time of Concentration

(Ref. MHFD Table 6-4)

Project No: 1075 By: Dash Date: 05/21/21

> Design Point= 1 NRCS Soil Type= C/D

> > $t_{t} = L/(V^{*}60)$

	Area	Imp.	Runoff Coefficients		5	
Description	(AC)	(%)	C ₂	C ₅	C ₁₀	C ₁₀₀
Industrial - Light	6.659	80%	0.65	0.69	0.72	0.81
Streets - Paved	0.000	100%	0.83	0.85	0.87	0.89
Drive and walks	0.000	90%	0.74	0.77	0.79	0.85
Roofs	0.000	90%	0.74	0.77	0.79	0.85
Lawns, clayey soil	0.000	2%	0.01	0.05	0.15	0.49
TOTAL	6.659	80%	0.65	0.69	0.72	0.81

Initial Overland Time (t_i) ti=0.395(1.1-C5)L1/2S-1/3

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Travel Time (t_t)

Overland Flow (Lo) (ft)= Slope (ft/ft)= t _i (min)=	500 0.020 13.32	Length (ft)= Slope (ft/ft)= Cv= Velocity (ft/s)=	700 0.010 20 2.00
t _c Urbanized Check t _c	e=(L/180)+10 (min)	t _t (min)=	5.83
Total Length (ft)= t _c (min)=	1,200 16.67	t _c Computed (t _i + t _t)= t _c Mininum= t_c Final (min)=	19.16 5.00 <u>16.67</u>

Rainfall Intensity (I)

(Ref. MHFD Volume 2, Section 5, Chapter 4 and Town of Erie Precipitation Data)

l₂ (in/hr)	l₅ (in/hr)	I ₁₀ (in/hr)	I ₁₀₀ (in/hr)
1.75	2.40	3.00	5.78

Runoff (Q)

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Q ₂ (cfs)	Q ₅ (cfs)	Q ₁₀ (cfs)	Q ₁₀₀ (cfs)
7.57	11.01	14.38	31.19

Basin A1

Lot 1 - Erie Airpark Replat D

2800 Airport Drive Erie, Colorado

Proposed Conditions - East Side of Lot 1

Runoff Coefficents

(Ref. MHFD Table 6-4)

Project No: 1075 By: Dash Date: 05/21/21

Design Point= 1

NRCS Soil Type= C/D

	Area	Imp.		Runoff Co	oefficients	5
Description	(AC)	(%)	C ₂	C ₅	C ₁₀	C ₁₀₀
Industrial - Light	3.682	80%	0.65	0.69	0.72	0.81
Streets - Paved	0.000	100%	0.83	0.85	0.87	0.89
Drive and walks	0.000	90%	0.74	0.77	0.79	0.85
Roofs	0.000	90%	0.74	0.77	0.79	0.85
Lawns, clayey soil	0.000	2%	0.01	0.05	0.15	0.49
TOTAL	3.682	80%	0.65	0.69	0.72	0.81

Time of Concentration

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Initial Overland Time (t_i)	ti=0.395(1.1-C5)L1/2S-1/3	3 Travel Time († _†)	t _t =L/(V*60)
Overland Flow (Lo) (ft)= Slope (ft/ft)= t _i (min)=	= 0.020	Length (ft)= Slope (ft/ft)= Cv=	500 0.017 20
t _c Urbanized Check	t _c =(L/180)+10 (min)	Velocity (ft/s)= t _t (min)=	2.61 3.20
Total Length (ft)= t _c (min)=		t _c Computed (t _i + t _t)= t _c Mininum= t_c Final (min)=	16.52 5.00 <u>15.56</u>

Rainfall Intensity (I)

(Ref. MHFD Volume 2, Section 5, Chapter 4 and Town of Erie Precipitation Data)

l₂ (in/hr)	l₅ (in/hr)	I₁₀ (in/hr)	I ₁₀₀ (in∕hr)
1.81	2.48	3.10	5.98

Runoff (Q)

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Q ₂ (cfs)	Q ₅ (cfs)	Q ₁₀ (cfs)	Q ₁₀₀ (cfs)
4.33	6.29	8.22	17.83

Lot 1 - Erie Airpark Replat D

2800 Airport Drive Erie, Colorado

Existing Conditions - Developed portions of Tract E-1

Runoff Coefficents

(Ref. MHFD Table 6-4)

Project No: 1075 By: Dash Date: 05/21/21

Design Point= 3

NRCS Soil Type= C/D

	Area	Imp.		Runoff Co	oefficients	5
Description	(AC)	(%)	C ₂	C ₅	C ₁₀	C ₁₀₀
Industrial - Light	0.000	80%	0.65	0.69	0.72	0.81
Streets - Paved	0.000	100%	0.83	0.85	0.87	0.89
Drive and walks	5.067	90%	0.74	0.77	0.79	0.85
Roofs	2.527	90%	0.74	0.77	0.79	0.85
Lawns, clayey soil	4.215	2%	0.01	0.05	0.15	0.49
TOTAL	11.808	59%	0.48	0.51	0.56	0.72

Time of Concentration

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Initial Overland Time (t_i)	ti=0.395(1.1-C5)L1/2S-1/	3 Travel Time (t_t)	t _t =L/(V*60)
Overland Flow (Lo) (ft): Slope (ft/ft): t _i (min):	= 0.03	Length (ft)= Slope (ft/ft)= Cv= Velocity (ft/s)=	1,200 0.005 20 1.41
t_c Urbanized Check	t _c =(L/180)+10 (min)	t _t (min)=	14.14
Total Length (ft): t _c (min):		t _c Computed (t _i + t _t)= t _c Mininum= t_c Final (min)=	30.45 5.00 <u>19.44</u>

Rainfall Intensity (I)

(Ref. MHFD Volume 2, Section 5, Chapter 4 and Town of Erie Precipitation Data)

l₂ (in/hr)	l₅ (in/hr)	I ₁₀ (in/hr)	I ₁₀₀ (in/hr)
1.62	2.22	2.77	5.35

Runoff (Q)

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Q ₂ (cfs)	Q ₅ (cfs)	Q ₁₀ (cfs)	Q ₁₀₀ (cfs)
9.15	13.42	18.40	45.58

Basin B1

Lot 1 - Erie Airpark Replat D

2800 Airport Drive Erie, Colorado

Existing Conditions - Eastern developed portions of Tract E-1

Runoff Coefficents

Time of Concentration

(Ref. MHFD Table 6-4)

Project No: 1075 By: Dash Date: 05/21/21

> Design Point= 2 NRCS Soil Type= C/D

> > t_t=L/(V*60)

850

	Area	Imp.		Runoff Co	oefficients	5
Description	(AC)	(%)	C ₂	C ₅	C ₁₀	C ₁₀₀
Industrial - Light	0.000	80%	0.65	0.69	0.72	0.81
Streets - Paved	0.000	100%	0.83	0.85	0.87	0.89
Drive and walks	0.819	90%	0.74	0.77	0.79	0.85
Roofs	0.446	90%	0.74	0.77	0.79	0.85
Lawns, clayey soil	1.075	2%	0.01	0.05	0.15	0.49
TOTAL	2.340	50%	0.40	0.44	0.50	0.68

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Travel Time (t_t)

Length (ft)=

Slope (ft/ft) = 0.01059

Initial Overland Time († _i)	ti=0.395(1.1-C5)L1/2S-1/3
Overland Flow (Lo) (ft)= Slope (ft/ft)=	
t _i (min)=	12.54

t _i (min)=	= 12.54	Cv=	20
		Velocity (ft/s)=	2.06
t _c Urbanized Check	t _c =(L/180)+10 (min)	t _t (min)=	6.88
Total Length (ft)=	= 1,150	t_c Computed ($t_i + t_t$)=	19.43
t _c (min)=	= 16.39	t _c Mininum=	5.00
		t _c Final (min)=	<u>16.39</u>

Rainfall Intensity (I)

(Ref. MHFD Volume 2, Section 5, Chapter 4 and Town of Erie Precipitation Data)

l₂ (in/hr)	l₅ (in/hr)	I₁₀ (in/hr)	I ₁₀₀ (in/hr)
1.76	2.42	3.02	5.83

Runoff (Q)

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Q ₂ (cfs)	Q ₅ (cfs)	Q ₁₀ (cfs)	Q ₁₀₀ (cfs)
1.67	2.48	3.51	9.34

Basin B2

Lot 1 - Erie Airpark Replat D

2800 Airport Drive Erie, Colorado

Existing Conditions - Uneveloped portions of Tract E-1

Runoff Coefficents

(Ref. MHFD Table 6-4)

Project No: 1075 By: Dash Date: 05/21/21

Design Point= 3

NRCS Soil Type= C/D

	Area	Imp.	Runoff Coefficients		5	
Description	(AC)	(%)	C ₂	C ₅	C ₁₀	C ₁₀₀
Industrial - Light	0.000	80%	0.65	0.69	0.72	0.81
Streets - Paved	0.000	100%	0.83	0.85	0.87	0.89
Drive and walks	0.611	90%	0.74	0.77	0.79	0.85
Roofs	0.000	90%	0.74	0.77	0.79	0.85
Lawns, clayey soil	1.246	2%	0.01	0.05	0.15	0.49
TOTAL	1.856	31%	0.25	0.29	0.36	0.61

Time	of	Concentration
	U .	

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Initial Overland Time (t_i)	ti=0.395(1.1-C5)L1/2S-1/	3 Travel Time (t_t)	t _t =L/(V*60)
Overland Flow (Lo) (ft)= Slope (ft/ft)= t _i (min)=	= 0.03	Length (ft)= Slope (ft/ft)= Cv= Velocity (ft/s)=	0 0.0075 20 1.73
t_c Urbanized Check	t _c =(L/180)+10 (min)	t _t (min)=	0.00
Total Length (ft)= t _c (min)=		t _c Computed (t _i + t _t)= t _c Mininum= t_c Final (min)=	17.27 5.00 <u>11.67</u>

Rainfall Intensity (I)

(Ref. MHFD Volume 2, Section 5, Chapter 4 and Town of Erie Precipitation Data)

l₂ (in/hr)	l₅ (in/hr)	I ₁₀ (in/hr)	I ₁₀₀ (in/hr)
2.06	2.82	3.53	6.81

Runoff (Q)

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Q ₂ (cfs)	Q ₅ (cfs)	Q ₁₀ (cfs)	Q ₁₀₀ (cfs)
0.96	1.50	2.36	7.69

Basin B3

Lot 1 - Erie Airpark Replat D

2800 Airport Drive Erie, Colorado

Existing Conditions - Western developed portions of Lot 2

Runoff Coefficents

(Ref. MHFD Table 6-4)

Project No: 1075 By: Dash Date: 05/21/21

Design Point= 1

NRCS Soil Type= C/D

Area	Imp.	Runoff Coefficients			S
(AC)	(%)	C ₂	C ₅	C ₁₀	C ₁₀₀
5.170	80%	0.65	0.69	0.72	0.81
0.000	100%	0.83	0.85	0.87	0.89
0.000	90%	0.74	0.77	0.79	0.85
0.000	90%	0.74	0.77	0.79	0.85
0.000	2%	0.01	0.05	0.15	0.49
5.170	80%	0.65	0.69	0.72	0.81
	(AC) 5.170 0.000 0.000 0.000 0.000	(AC) (%) 5.170 80% 0.000 100% 0.000 90% 0.000 90% 0.000 2%	(AC) (%) C2 5.170 80% 0.65 0.000 100% 0.83 0.000 90% 0.74 0.000 2% 0.01	(AC) (%) C2 C5 5.170 80% 0.65 0.69 0.000 100% 0.83 0.85 0.000 90% 0.74 0.77 0.000 90% 0.74 0.77 0.000 2% 0.01 0.05	(AC) (%) C2 C5 C10 5.170 80% 0.65 0.69 0.72 0.000 100% 0.83 0.85 0.87 0.000 90% 0.74 0.77 0.79 0.000 90% 0.74 0.77 0.79 0.000 2% 0.01 0.05 0.15

<u>Time</u>	of	Concentration	

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Initial Overland Time († _i)	ti=0.395(1.1-C5)L1/2S-1/3	3 Travel Time († _t)	t _t =L/(V*60)
Overland Flow (Lo) (ft)= Slope (ft/ft)= t _i (min)=	= 0.02	Length (ft)= Slope (ft/ft)= Cv= Velocity (ft/s)=	1,025 0.0056 20 1.50
$t_{\rm c}$ Urbanized Check	t _c =(L/180)+10 (min)	t _t (min)=	11.41
Total Length (ft)= t _c (min)=		t _c Computed (t _i + t _t)= t _c Mininum= t_c Final (min)=	15.18 5.00 <u>15.18</u>

Rainfall Intensity (I)

(Ref. MHFD Volume 2, Section 5, Chapter 4 and Town of Erie Precipitation Data)

l₂ (in/hr)	l₅ (in/hr)	I ₁₀ (in/hr)	I ₁₀₀ (in/hr)
1.83	2.51	3.14	6.05

Runoff (Q)

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Q ₂ (cfs)	Q ₅ (cfs)	Q ₁₀ (cfs)	Q ₁₀₀ (cfs)
6.14	8.94	11.68	25.33

Basin C1

Lot 1 - Erie Airpark Replat D

2800 Airport Drive Erie, Colorado

Proposed Conditions - Building F

Runoff Coefficents

(Ref. MHFD Table 6-4)

Project No: 1075 By: Dash Date: 05/21/21

Design Point= 1

NRCS Soil Type= C/D

	Area	Imp.	Runoff Coefficients			5
Description	(AC)	(%)	C ₂	C ₅	C ₁₀	C ₁₀₀
Industrial - Light	0.000	80%	0.65	0.69	0.72	0.81
Streets - Paved	0.000	100%	0.83	0.85	0.87	0.89
Drive and walks	0.000	90%	0.74	0.77	0.79	0.85
Roofs	0.436	90%	0.74	0.77	0.79	0.85
Lawns, clayey soil	0.000	2%	0.01	0.05	0.15	0.49
TOTAL	0.436	90%	0.74	0.77	0.79	0.85

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Initial Overland Time († _i)	ti=0.395(1.1-C5)L1/2S-1	/3 Travel Time (t_t)	t _t =L/(V*60)
Overland Flow (Lo) (ft)= Slope (ft/ft)= t _i (min)=	= 0.020	Length (ft)= Slope (ft/ft)= Cv=	0 0.000 20
t _c Urbanized Check	t _c =(L/180)+10 (min)	Velocity (ft/s)= t _t (min)=	0.02
Total Length (ft)= t _c (min)=		t _c Computed (t _i + t _t)= t _c Mininum= t_c Final (min)=	4.80 5.00 <u>5.00</u>

Rainfall Intensity (I)

(Ref. MHFD Volume 2, Section 5, Chapter 4 and Town of Erie Precipitation Data)

l₂ (in/hr)	l₅ (in/hr)	I₁₀ (in/hr)	I ₁₀₀ (in/hr)
2.75	3.76	4.71	9.09

Runoff (Q)

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Q ₂ (cfs)	Q ₅ (cfs)	Q ₁₀ (cfs)	Q ₁₀₀ (cfs)
0.89	1.26	1.62	3.37

Basin C1-1

Lot 1 - Erie Airpark Replat D

2800 Airport Drive Erie, Colorado

Proposed Conditions - Building D

Runoff Coefficents

(Ref. MHFD Table 6-4)

Project No: 1075 By: Dash Date: 05/21/21

Design Point= 1

NRCS Soil Type= C/D

	Area	Imp.	Runoff Coefficients			5
Description	(AC)	(%)	C ₂	C ₅	C ₁₀	C ₁₀₀
Industrial - Light	0.000	80%	0.65	0.69	0.72	0.81
Streets - Paved	0.000	100%	0.83	0.85	0.87	0.89
Drive and walks	0.000	90%	0.74	0.77	0.79	0.85
Roofs	0.689	90%	0.74	0.77	0.79	0.85
Lawns, clayey soil	0.000	2%	0.01	0.05	0.15	0.49
TOTAL	0.689	90%	0.74	0.77	0.79	0.85
-						

Time of Concentration

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Initial Overland Time († _i)	ti=0.395(1.1-C5)L1/2S-1	/3 Travel Time (t_t)	t _t =L/(V*60)
Overland Flow (Lo) (ft)= Slope (ft/ft)= t _i (min)=	= 0.020	Length (ft)= Slope (ft/ft)= Cv=	0 0.000 20
t _c Urbanized Check	t _c =(L/180)+10 (min)	Velocity (ft/s)= t _t (min)=	0.02
Total Length (ft)= t _c (min)=		t _c Computed (t _i + t _t)= t _c Mininum= t_c Final (min)=	4.80 5.00 <u>5.00</u>

Rainfall Intensity (I)

(Ref. MHFD Volume 2, Section 5, Chapter 4 and Town of Erie Precipitation Data)

l₂ (in/hr)	l₅ (in/hr)	l ₁₀ (in/hr)	I ₁₀₀ (in/hr)
2.75	3.76	4.71	9.09

Runoff (Q)

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Q ₂ (cfs)	Q ₅ (cfs)	Q ₁₀ (cfs)	Q ₁₀₀ (cfs)
1.40	2.00	2.57	5.32

Basin C1-2

Lot 1 - Erie Airpark Replat D

2800 Airport Drive Erie, Colorado

Proposed Conditions - Building C

Runoff Coefficents

h

S C R L T

(Ref. MHFD Table 6-4)

Project No: 1075 By: Dash Date: 05/21/21

	Area	lmp.	Runoff Coefficients			5
Description	(AC)	(%)	C ₂	C ₅	C ₁₀	C ₁₀₀
Industrial - Light	0.000	80%	0.65	0.69	0.72	0.81
Streets - Paved	0.000	100%	0.83	0.85	0.87	0.89
Drive and walks	0.000	90%	0.74	0.77	0.79	0.85
Roofs	0.574	90%	0.74	0.77	0.79	0.85
Lawns, clayey soil	0.000	2%	0.01	0.05	0.15	0.49
TOTAL	0.574	90%	0.74	0.77	0.79	0.85
Time of Concentration	(Ref MHED Volum		ion (Ch	aptor 2)		

lime	OT	Concentration

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Initial Overland Time (t_i)	ti=0.395(1.1-C5)L1/2S-1/2	3 Travel Time († _†)	t _t =L/(V*60)
Overland Flow (Lo) (ft)= Slope (ft/ft)=	- 0.020	Length (ft)= Slope (ft/ft)=	0 0.000
t _i (min)=		Cv= Velocity (ft/s)=	20 0.02
t _c Urbanized Check	t _c =(L/180)+10 (min)	t _t (min)=	0.00
Total Length (ft)=	= 100	t_c Computed $(t_i + t_t) =$	4.80
t _c (min)=	= 10.56	t _c Mininum= t_c Final (min)=	5.00 <u>5.00</u>

Rainfall Intensity (I)

(Ref. MHFD Volume 2, Section 5, Chapter 4 and Town of Erie Precipitation Data)

l₂ (in/hr)	l₅ (in/hr)	I ₁₀ (in/hr)	I ₁₀₀ (in/hr)
2.75	3.76	4.71	9.09

Runoff (Q)

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Q ₂ (cfs)	Q ₅ (cfs)	Q ₁₀ (cfs)	Q ₁₀₀ (cfs)
1.17	1.66	2.14	4.43

Basin C1-3

Design Point= 1 NRCS Soil Type= C/D

Lot 1 - Erie Airpark Replat D

2800 Airport Drive Erie, Colorado

Proposed Conditions - Building B

Runoff Coefficents

(Ref. MHFD Table 6-4)

Project No: 1075 By: Dash Date: 05/21/21

Design Point= 1

NRCS Soil Type= C/D

	Area	Imp.	Runoff Coefficients		5	
Description	(AC)	(%)	C ₂	C ₅	C ₁₀	C ₁₀₀
Industrial - Light	0.000	80%	0.65	0.69	0.72	0.81
Streets - Paved	0.000	100%	0.83	0.85	0.87	0.89
Drive and walks	0.000	90%	0.74	0.77	0.79	0.85
Roofs	0.689	90%	0.74	0.77	0.79	0.85
Lawns, clayey soil	0.000	2%	0.01	0.05	0.15	0.49
TOTAL	0.689	90%	0.74	0.77	0.79	0.85

Time of Concentration

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Initial Overland Time († _i)	ti=0.395(1.1-C5)L1/2S-1	/3 Travel Time (t_t)	t _t =L/(V*60)
Overland Flow (Lo) (ft)= Slope (ft/ft)= t _i (min)=	= 0.020	Length (ft)= Slope (ft/ft)= Cv=	0 0.000 20
t _c Urbanized Check	t _c =(L/180)+10 (min)	Velocity (ft/s)= t _t (min)=	0.02
Total Length (ft)= t _c (min)=		t _c Computed (t _i + t _t)= t _c Mininum= t_c Final (min)=	4.80 5.00 <u>5.00</u>

Rainfall Intensity (I)

(Ref. MHFD Volume 2, Section 5, Chapter 4 and Town of Erie Precipitation Data)

l₂ (in/hr)	l₅ (in/hr)	I ₁₀ (in/hr)	I ₁₀₀ (in/hr)
2.75	3.76	4.71	9.09

Runoff (Q)

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Q ₂ (cfs)	Q ₅ (cfs)	Q ₁₀ (cfs)	Q ₁₀₀ (cfs)
1.40	2.00	2.57	5.32

Basin C1-4

Lot 1 - Erie Airpark Replat D

2800 Airport Drive Erie, Colorado

Proposed Conditions - Building A

Runoff Coefficents

(Ref. MHFD Table 6-4)

Project No: 1075 By: Dash Date: 05/21/21

Design Point= 1

NRCS Soil Type= C/D

	Area	Imp.	Runoff Coefficients			
Description	(AC)	(%)	C ₂	C ₅	C ₁₀	C ₁₀₀
Industrial - Light	0.000	80%	0.65	0.69	0.72	0.81
Streets - Paved	0.000	100%	0.83	0.85	0.87	0.89
Drive and walks	0.000	90%	0.74	0.77	0.79	0.85
Roofs	0.574	90%	0.74	0.77	0.79	0.85
Lawns, clayey soil	0.000	2%	0.01	0.05	0.15	0.49
TOTAL	0.574	90%	0.74	0.77	0.79	0.85
	-	-	÷		•	-

Time of Concentration

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Initial Overland Time († _i)	ti=0.395(1.1-C5)L1/2S-1	/3 Travel Time (t_t)	t _t =L/(V*60)
Overland Flow (Lo) (ft)= Slope (ft/ft)= t _i (min)=	= 0.020	Length (ft)= Slope (ft/ft)= Cv=	0 0.000 20
t _c Urbanized Check	t _c =(L/180)+10 (min)	Velocity (ft/s)= t _t (min)=	0.02
Total Length (ft)= t _c (min)=		t _c Computed (t _i + t _t)= t _c Mininum= t_c Final (min)=	4.80 5.00 <u>5.00</u>

Rainfall Intensity (I)

(Ref. MHFD Volume 2, Section 5, Chapter 4 and Town of Erie Precipitation Data)

l₂ (in/hr)	l₅ (in/hr)	I ₁₀ (in/hr)	I ₁₀₀ (in/hr)
2.75	3.76	4.71	9.09

Runoff (Q)

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Q ₂ (cfs)	Q ₅ (cfs)	Q ₁₀ (cfs)	Q ₁₀₀ (cfs)
1.17	1.66	2.14	4.43

Basin C1-5

Lot 1 - Erie Airpark Replat D

2800 Airport Drive Erie, Colorado

Existing Conditions - Tract 4 Offsite Basin

Runoff Coefficents

Time of Concentration

(Ref. MHFD Table 6-4)

Project No: 1075 By: Dash Date: 05/21/21

Design Point= 4

NRCS Soil Type= C/D

	Area	Imp.	Runoff Coefficients			5
Description	(AC)	(%)	C ₂	C ₅	C ₁₀	C ₁₀₀
Industrial - Light	0.000	80%	0.65	0.69	0.72	0.81
Streets - Paved	0.000	100%	0.83	0.85	0.87	0.89
Drive and walks	0.000	90%	0.74	0.77	0.79	0.85
Roofs	0.000	90%	0.74	0.77	0.79	0.85
Lawns, clayey soil	10.453	2%	0.01	0.05	0.15	0.49
TOTAL	10.453	2%	0.01	0.05	0.15	0.49

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Initial Overland Time (t_i)	ti=1.8(1.1-C5)L1/2S-1/3	3 Travel Time (t _t)	t _t =L/(V*60)
Overland Flow (Lo) (ft): Slope (ft/ft): t _i (min):	= 0.053	Length (ft)= Slope (ft/ft)= Cv=	1,000 0.028 15
t _c Urbanized Check	t _c =(L/180)+10 (min)	Velocity (ft/s)= t _t (min)=	2.51 6.64
Total Length (ft): t _c (min):		t _c Computed (t _i + t _t)= t _c Mininum= t_c Final (min)=	31.34 5.00 <u>31.34</u>

Rainfall Intensity (I)

(Ref. MHFD Volume 2, Section 5, Chapter 4 and Town of Erie Precipitation Data)

l₂ (in/hr)	l₅ (in/hr)	I ₁₀ (in/hr)	I ₁₀₀ (in/hr)
1.24	1.70	2.13	4.10

Runoff (Q)

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Q ₂ (cfs)	Q ₅ (cfs)	Q ₁₀ (cfs)	Q ₁₀₀ (cfs)
0.13	0.89	3.33	20.99

Lot 1 - Erie Airpark Replat D

2800 Airport Drive Erie, Colorado

Existing Conditions - Airport Drive Offsite Basin

Runoff Coefficents

(Ref. MHFD Table 6-4)

Project No: 1075 By: Dash Date: 05/21/21

Design Point= 4

NRCS Soil Type= C/D

t_t=L/(V*60)

400

0.02

15

2.12

3.14

Length (ft)=

Slope (ft/ft)=

Velocity (ft/s)=

Cv=

t_t (min)=

	Area	Imp.	Runoff Coefficients			S
Description	(AC)	(%)	C ₂	C ₅	C ₁₀	C ₁₀₀
Industrial - Light	0.000	80%	0.65	0.69	0.72	0.81
Streets - Paved	0.372	100%	0.83	0.85	0.87	0.89
Drive and walks	0.000	90%	0.74	0.77	0.79	0.85
Roofs	0.000	90%	0.74	0.77	0.79	0.85
Lawns, clayey soil	0.000	2%	0.01	0.05	0.15	0.49
TOTAL	0.372	100%	0.83	0.85	0.87	0.89
Time of Concentration	(Ref. MHFD Volun	ne 2, Sect	ion 6, Ch	apter 2)		

Initial Overland Time (t _i)	ti=1.8(1.1-C5)L1/2S-1/3	Travel Time (t_t)
Overland Flow (Lo) (ft)= 50	Length (ft
Slope (ft/ft)= 0.02	Slope (ft/ft)
t _i (min)= 2.57	C
		Velocity (ft/s)
t _c Urbanized Check	t _c =(L/180)+10 (min)	t _t (min)

	t _c Final (min)=	5.71
t _c (min)= n/a	t _c Mininum=	5.00
Total Length (ft)= n/a	t_c Computed $(t_i + t_t)$ =	5.71

Rainfall Intensity (I)

(Ref. MHFD Volume 2, Section 5, Chapter 4 and Town of Erie Precipitation Data)

l₂ (in/hr)	l₅ (in/hr)	I ₁₀ (in/hr)	I ₁₀₀ (in/hr)
2.65	3.63	4.55	8.76

Runoff (Q)

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Q ₂ (cfs)	Q ₅ (cfs)	Q ₁₀ (cfs)	Q ₁₀₀ (cfs)
0.82	1.15	1.47	2.90

Lot 1 - Erie Airpark Replat D

2800 Airport Drive Erie, Colorado

Existing Conditions - Airport Drive Offsite Basin

Runoff Coefficents

(Ref. MHFD Table 6-4)

Project No: 1075 By: Dash Date: 05/21/21

Design Point= 5

NRCS Soil Type= C/D

	Area	Imp.	Runoff Coefficients			5
Description	(AC)	(%)	C ₂	C ₅	C ₁₀	C ₁₀₀
Industrial - Light	0.000	80%	0.65	0.69	0.72	0.81
Streets - Paved	0.081	100%	0.83	0.85	0.87	0.89
Drive and walks	0.000	90%	0.74	0.77	0.79	0.85
Roofs	0.000	90%	0.74	0.77	0.79	0.85
Lawns, clayey soil	0.000	2%	0.01	0.05	0.15	0.49
TOTAL	0.081	100%	0.83	0.85	0.87	0.89
Time of Concentration	(Ref. MHFD Volur	ne 2, Sect	tion 6, Ch	apter 2)		

Initial Overland Time (t_i)	ti=1.8(1.1-C5)L1/2S-1/3	3 Travel Time (t_{t})	t _t =L/(V*60)
Overland Flow (Lo) (ft)= Slope (ft/ft)=		Length (ft)= Slope (ft/ft)=	0 0.02
t _i (min)=	= 2.57	Cv=	15
		Velocity (ft/s)=	2.12
t_c Urbanized Check	t _c =(L/180)+10 (min)	t _t (min)=	0.00
Total Length (ft)=	= n/a	t_c Computed $(t_i + t_t)$ =	2.57
t _c (min)=	= n/a	t _c Mininum=	5.00
		t _c Final (min)=	5.00

Rainfall Intensity (I)

(Ref. MHFD Volume 2, Section 5, Chapter 4 and Town of Erie Precipitation Data)

l₂ (in/hr)	l₅ (in/hr)	I ₁₀ (in/hr)	I ₁₀₀ (in/hr)
2.75	3.76	4.71	9.09

Runoff (Q)

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Q ₂ (cfs)	Q ₅ (cfs)	Q ₁₀ (cfs)	Q ₁₀₀ (cfs)
0.19	0.26	0.33	0.66

Lot 1 - Erie Airpark Replat D

2800 Airport Drive Erie, Colorado

Existing Conditions - Airport Drive Offsite Basin

Runoff Coefficents

(Ref. MHFD Table 6-4)

Project No: 1075 By: Dash Date: 05/21/21

Design Point= 5

NRCS Soil Type= C/D

	Area	Imp.	Runoff Coefficients			5		
Description	(AC)	(%)	C ₂	C ₅	C ₁₀	C ₁₀₀		
Industrial - Light	0.000	80%	0.65	0.69	0.72	0.81		
Streets - Paved	0.175	100%	0.83	0.85	0.87	0.89		
Drive and walks	0.000	90%	0.74	0.77	0.79	0.85		
Roofs	0.000	90%	0.74	0.77	0.79	0.85		
Lawns, clayey soil	0.000	2%	0.01	0.05	0.15	0.49		
TOTAL	0.175	100%	0.83	0.85	0.87	0.89		
Time of Concentration	(Ref. MHFD Volume 2, Section 6, Chapter 2)							

Initial Overland Time (t _i)	ti=1.8(1.1-C5)L1/2S-1/3	3 Travel Time († _†)	t _t =L/(V*60)
Overland Flow (Lo) (ft Slope (ft/ft)		Length (ft)= Slope (ft/ft)=	0 0.02
t _i (min))= 2.57	Cv=	15
		Velocity (ft/s)=	2.12
$t_{\rm c}$ Urbanized Check	t _c =(L/180)+10 (min)	t _t (min)=	0.00
Total Length (ft)= n/a	t_c Computed $(t_i + t_t)$ =	2.57
t _c (min))= n/a	t _c Mininum=	5.00
		t _c Final (min)=	5.00

Rainfall Intensity (I)

(Ref. MHFD Volume 2, Section 5, Chapter 4 and Town of Erie Precipitation Data)

l₂ (in/hr)	l₅ (in/hr)	I ₁₀ (in/hr)	I ₁₀₀ (in/hr)
2.75	3.76	4.71	9.09

Runoff (Q)

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Q ₂ (cfs)	Q₅ (cfs)	Q ₁₀ (cfs)	Q ₁₀₀ (cfs)
0.40	0.56	0.72	1.42

Lot 1 - Erie Airpark Replat D

2800 Airport Drive Erie, Colorado

Existing Conditions - Airport Drive Offsite Basin

<u>Runoff Coefficents</u>

(Ref. MHFD Table 6-4)

Project No: 1075 By: Dash Date: 05/21/21

Design Point= 5

NRCS Soil Type= C/D

	Area	Imp.	Runoff Coefficients					
Description	(AC)	(%)	C ₂	C ₅	C ₁₀	C ₁₀₀		
Industrial - Light	0.000	80%	0.65	0.69	0.72	0.81		
Streets - Paved	0.065	100%	0.83	0.85	0.87	0.89		
Drive and walks	0.000	90%	0.74	0.77	0.79	0.85		
Roofs	0.000	90%	0.74	0.77	0.79	0.85		
Lawns, clayey soil	0.000	2%	0.01	0.05	0.15	0.49		
TOTAL	0.065	100%	0.83	0.85	0.87	0.89		
Time of Concentration	(Ref. MHFD Volume 2, Section 6, Chapter 2)							

Initial Overland Time (t_i)	ti=1.8(1.1-C5)L1/2S-1/3	3 Travel Time († _t)	t _t =L/(V*60)
Overland Flow (Lo) (ft) Slope (ft/ft)	= 0.02	Length (ft)= Slope (ft/ft)=	0 0.02
t _i (min) t _c Urbanized Check	= 2.57 $t_c = (L/180) + 10 \text{ (min)}$	Cv= Velocity (ft/s)= t _t (min)=	15 2.12 0.00
Total Length (ft)		t_c Computed $(t_i + t_t) =$	2.57
t _c (min)	= n/a	t _c Mininum= t_c Final (min)=	5.00 5.00

Rainfall Intensity (I)

(Ref. MHFD Volume 2, Section 5, Chapter 4 and Town of Erie Precipitation Data)

l₂ (in/hr)	l₅ (in/hr)	I ₁₀ (in/hr)	I ₁₀₀ (in/hr)
2.75	3.76	4.71	9.09

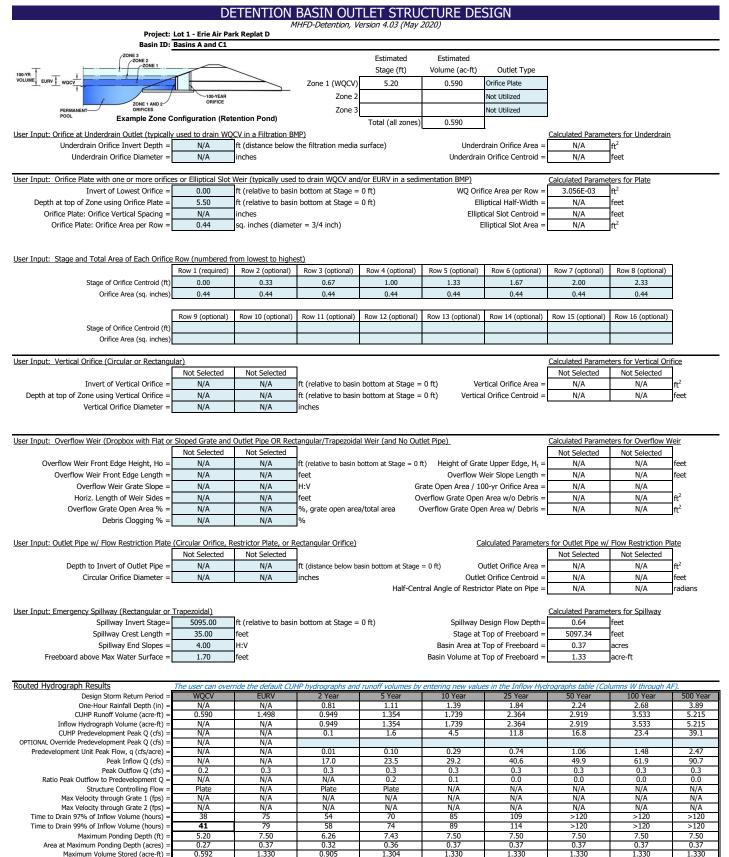
Runoff (Q)

(Ref. MHFD Volume 2, Section 6, Chapter 2)

Q ₂ (cfs)	Q ₅ (cfs)	Q ₁₀ (cfs)	Q ₁₀₀ (cfs)
0.15	0.21	0.27	0.53

APPENDIX C

WATER QUALITY CALCULATIONS



1.304

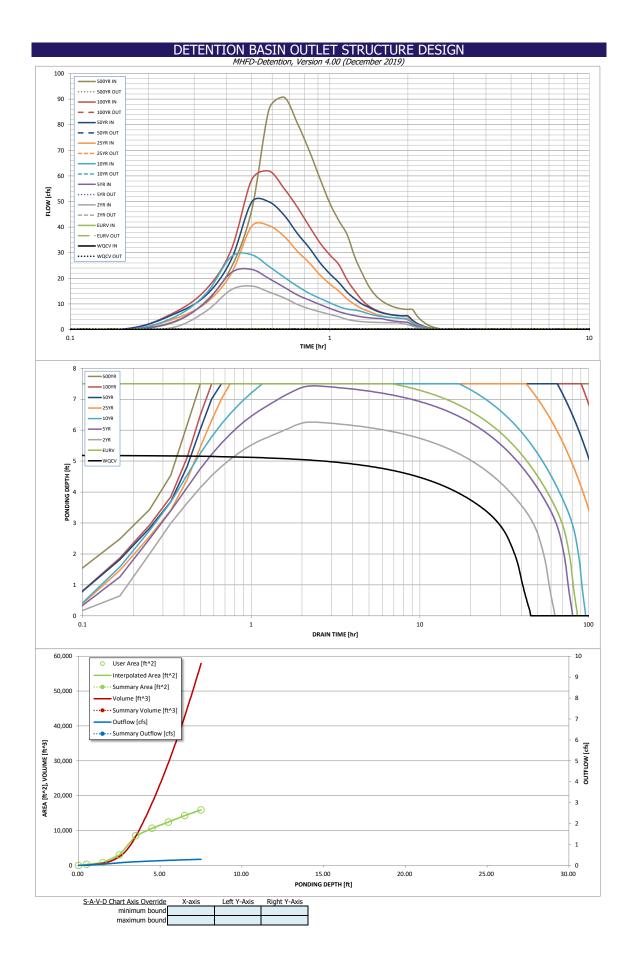
1.330

Area at Maximum Ponding Depth (acres) Maximum Volume Stored (acre-ft) :

1.330

1.330

1.330



DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

	The user can o		lated inflow hyd	lrographs from t	his workbook w	ith inflow hydrog	graphs develope	d in a separate p	rogram.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.38	0.36	2.81
	0:15:00	0.00	0.00	0.84	3.02	4.71	4.06	5.94	6.50	11.08
	0:20:00	0.00	0.00	7.15	10.77	14.03	10.37	13.39	15.67	24.18
	0:25:00	0.00	0.00	15.55	22.20	28.40	21.79	27.24	31.09	46.67
	0:30:00 0:35:00	0.00	0.00	16.98	23.47	29.20	40.35	49.80	58.53	86.07
	0:40:00	0.00	0.00	14.64 12.37	19.90 16.53	24.62 20.46	40.57 36.39	49.88 44.68	61.92 55.09	90.73 80.63
	0:45:00	0.00	0.00	9.82	13.51	16.92	30.57	37.51	47.79	69.87
	0:50:00	0.00	0.00	8.11	11.53	14.16	26.05	31.93	40.35	58.93
	0:55:00	0.00	0.00	6.93	9.78	12.19	21.32	26.11	33.85	49.39
	1:00:00	0.00	0.00	5.91	8.27	10.46	17.80	21.78	29.17	42.56
	1:05:00	0.00	0.00	4.99	6.98	8.98	15.02	18.39	25.39	37.04
	1:10:00	0.00	0.00	3.94	6.09	7.97	11.92	14.60	19.33	28.22
	1:15:00 1:20:00	0.00	0.00	3.38	5.43 4.92	7.60	9.77	11.98 9.94	15.00	21.94
	1:25:00	0.00	0.00	2.90	4.92	6.96 6.10	8.11 7.07	9.94 8.66	11.42 9.12	16.73 13.37
	1:30:00	0.00	0.00	2.90	4.39	5.51	6.06	7.42	7.69	11.29
	1:35:00	0.00	0.00	2.74	4.23	5.10	5.37	6.58	6.74	9.89
	1:40:00	0.00	0.00	2.68	3.74	4.82	4.94	6.05	6.11	8.97
	1:45:00	0.00	0.00	2.65	3.38	4.63	4.64	5.68	5.69	8.35
	1:50:00	0.00	0.00	2.64	3.14	4.50	4.45	5.45	5.44	7.99
	1:55:00	0.00	0.00	2.23	2.97	4.26	4.34	5.31	5.35	7.86
	2:00:00 2:05:00	0.00	0.00	1.93	2.76	3.81	4.27	5.23	5.31	7.80
	2:10:00	0.00	0.00	1.32 0.88	1.88	2.60 1.75	2.92	3.58 2.40	3.66 2.47	5.38 3.63
	2:15:00	0.00	0.00	0.58	0.82	1.16	1.30	1.61	1.65	2.43
	2:20:00	0.00	0.00	0.36	0.51	0.73	0.84	1.02	1.05	1.54
	2:25:00	0.00	0.00	0.21	0.32	0.46	0.53	0.65	0.67	0.98
	2:30:00	0.00	0.00	0.11	0.19	0.26	0.31	0.38	0.39	0.58
	2:35:00	0.00	0.00	0.05	0.09	0.12	0.15	0.18	0.19	0.28
	2:40:00	0.00	0.00	0.01	0.03	0.03	0.05	0.06	0.06	0.09
	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:50:00 2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00 3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00 4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00 4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00 4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00 5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00 5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00 5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.03 (May 2020)

Summary Stage-Area-Volume-Discharge Relationships The user can create a summary S-AV-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-AV-D table to the full S-AV-D table in the chart to confirm it captures all key transition points.

Stage - Storage Description	Stage	Area	Area	Volume	Volume	Total Outflow	
	[ft]	[ft ²]	[acres]	[ft ³]	[ac-ft]	[cfs]	
							For best results, include the
							stages of all grade slope changes (e.g. ISV and Floor)
							from the S-A-V table on
							Sheet 'Basin'.
	-						
	+						Also include the inverts of al outlets (e.g. vertical orifice,
							overflow grate, and spillway,
							where applicable).
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	Design Procedure Form:	Extended Detention Basin (EDB)
Designer:	UD-BMP	(Version 3.07, March 2018) Sheet 1 of 3
Company: Date:	May 24, 2021	
Project:	Lot 1 - Erie Air Park Replat D	
Location:	Erie, Colorado	
4 Decis Observab	february and the second s	
1. Basin Storage V		
	perviousness of Tributary Area, Ia	I _n = 95.0 %
	a's Imperviousness Ratio (i = $I_a/100$)	i = 0.950
	Watershed Area	Area = <u>15.830</u> ac
	neds Outside of the Denver Region, Depth of Average lucing Storm	d ₆ = in
E) Design Cond (Select EUR)	cept V when also designing for flood control)	Choose One Water Quality Capture Volume (WQCV) O Excess Urban Runoff Volume (EURV)
	me (WQCV) Based on 40-hour Drain Time 1.0 * (0.91 * i ³ - 1.19 * i ² + 0.78 * i) / 12 * Area)	V _{DESCA} =ac-ft
Water Quali	heds Outside of the Denver Region, ity Capture Volume (WQCV) Design Volume $_{R} = (4_{0}^{*}(V_{DESIGN}(0.43))$	VDESIGN OTHER= ac-ft
	of Water Quality Capture Volume (WQCV) Design Volume fferent WQCV Design Volume is desired)	VDESIGN USER= ac-ft
 i) Percenta ii) Percenta 	logic Soil Groups of Tributary Watershed ge of Watershed consisting of Type A Soils age of Watershed consisting of Type B Soils tage of Watershed consisting of Type C/D Soils	HSG A = % % % %
For HSG A: For HSG B:	in Runoff Volume (EURV) Design Volume : EURV _A = 1.68 $^{+1}$ ^{2.30} : EURV _B = 1.36 $^{+1}$ ^{0.60} (D. EURV _B = 1.20 $^{+1}$ ^{0.68} (D. EURV _B = 1.20 $^{+1}$ ^{0.68}	EURV _{DESION} = ac-f t
	f Excess Urban Runoff Volume (EURV) Design Volume ferent EURV Design Volume is desired)	EURV _{DESION USER} ac-f t
	ength to Width Ratio to width ratio of at least 2:1 will improve TSS reduction.)	L:W= 2.0 :1
3. Basin Side Slop	ies	
	num Side Slopes distance per unit vertical, 4:1 or flatter preferred)	Z = ft / ft
4. Inlet		
	eans of providing energy dissipation at concentrated	
inflow location		
5. Forebay		
A) Minimum Fo		V _{FMIN} = 0.018 ac-ft
	= <u>3%</u> of the WQCV)	
B) Actual Foreb C) Ecrobary Dop		V _F = ac-ft
C) Forebay Dep (D _F		D _F = 18.0 in
D) Forebay Disc	charge	
i) Undetaine	ed 100-year Peak Discharge	Q ₁₀₀ = 75.21 cfs
ii) Forebay (Q _F = 0.02	Discharge Design Flow 2 * Q ₁₀₀)	Q _F = ofs
E) Forebay Disc		Choose One O Berm With Pipe Wall with Rect. Notch O Wall with V-Notch Weir
F) Discharge Pi	pe Size (minimum 8-inches)	Calculated D _P =in
G) Rectangular	Notch Width	Calculated $W_N = 6.6$ in

BMP Worksheet 2021-05-21, EDB

5/24/2021, 7:51 PM

Design	Procedure Form: Extended Detention Basin (EDB) Sheet 2 of
Designer: DASH	Sheet 2 of
Company:	
Date: May 24, 2021	
Project: Lot 1 - Erie Air Park Replat D	
Location: Erie, Colorado	
	Choose One
6. Trickle Channel	Concrete
A) Type of Trickle Channel	O Soft Bottom
	O SOR BORON
F) Slope of Trickle Channel	S =ft / ft
7. Micropool and Outlet Structure	
A) Depth of Micropool (2.5-feet minimum)	D _M = ft
B) Surface Area of Micropool (10 ft ² minimum)	A _M = 10 sq ft
C) Outlet Type	
	Choose One
	O Other (Describe):
D) Smallest Dimension of Orifice Opening Based on Hydrograph I	
(Use UD-Detention)	D _{orifice} = 0.75 inches
E) Total Outlet Area	A _{ct} = 3.52 square inches
8. Initial Surcharge Volume	
 A) Depth of Initial Surcharge Volume (Minimum recommended depth is 4 inches) 	D _{IS} = in
B) Minimum Initial Surcharge Volume (Minimum volume of 0.3% of the WQCV)	V _{IS} = <u>77</u> cu ft
C) Initial Surcharge Provided Above Micropool	V _s = <u>3.3</u> cu ft
9. Trash Rack	
A) Water Quality Screen Open Area: $A_t = A_{ot} * 38.5*(e^{-0.095D})$	A _t = <u>126</u> square inches
B) Type of Screen (If specifying an alternative to the materials reco	
in the USDCM, indicate "other" and enter the ratio of the total oper total screen are for the material specified.)	en are to the
Other (Y/N): N	J
C) Ratio of Total Open Area to Total Area (only for type 'Other')	User Ratio =
D) Total Water Quality Screen Area (based on screen type)	A _{tobal} = 210 sq. in.
E) Depth of Design Volume (EURV or WQCV) (Based on design concept chosen under 1E)	H=feet
F) Height of Water Quality Screen (H _{TR})	H _{TR} = 90.4 inches
G) Width of Water Quality Screen Opening (W _{opening})	W _{opening} = 12.0 inches VALUE LESS THAN RECOMMENDED MIN. WIDTH.
(Minimum of 12 inches is recommended)	Wopening = 12.0 Inches VALUE LESS THAN RECOMMENDED MIN. WIDTH. WIDTH HAS BEEN SET TO 12 INCHES.

	Design Procedure Form:	Extended Detention Basin (EDB)	
Designer: Company:	DASH	Sheet 3	of 3
Date:	May 24, 2021		
Project:	Lot 1 - Erie Air Park Replat D		
Location:	Erie, Colorado		
			_
10. Overflow Emba	ankment		
A) Describe er	nbankment protection for 100-year and greater overtopping:	Buried riprap	
	verflow Embankment distance per unit vertical, 4:1 or flatter preferred)	Ze = 10.00 ft / ft	
11. Vegetation		Choose One Irrigated O Not Irrigated IN THE BOTTOM OF THE BASIN	
12. Access			
A) Describe Se	ediment Removal Procedures		
Notes:			_

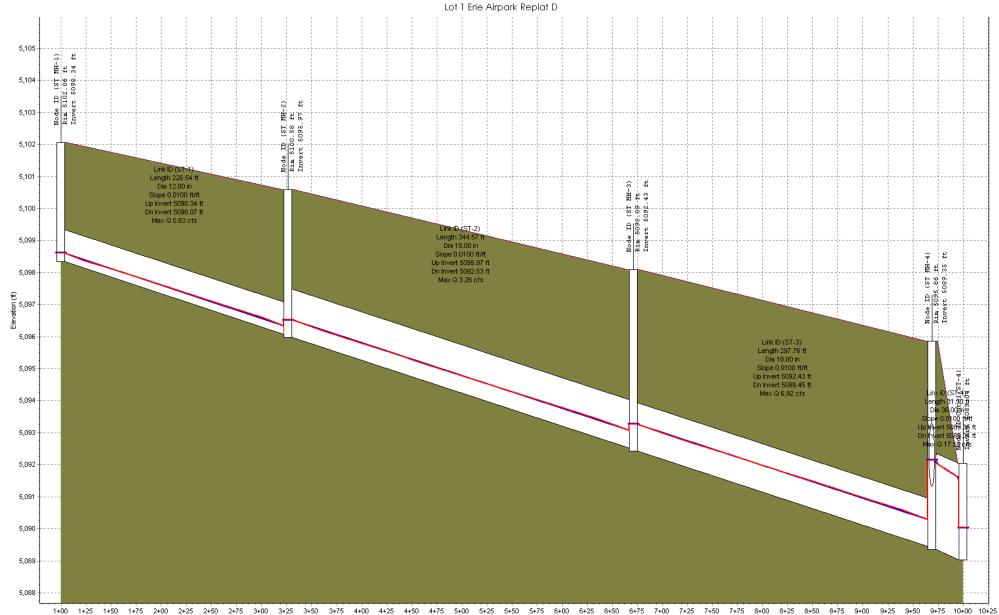
<u>APPENDIX D</u>

HYDRAULIC CALCULATIONS



Autodesk Storm and Sanitary Analysis

Profile Plot - 5-Year Storm



Station (ft)

Node ID:	(ST N		(ST N	1H-2)	(ST)	(ST MH-4)⊉ut-1(ST-4)			
Rim (ft):	510	2.06	510).58	509	8.09	5095.86		
Invert (ft):	509	3.34	5095	5.97	509	2.43	5089.35 5089.04		
Min Pipe Cover (ft):	2.	72	3.1	11	4.	07	2.56		
Max HGL (ft):	509	3.61	509	6.52	503	3.27	5092.14 5090.04		
Link ID:		(S1	-1)	(ST	(ST-2)				
Length (ft):		226	.54	344.	57	297	76 3	31.50	
Dia (in):		12.	00	18.00		18.	00 3	36.00	
Slope (ft/ft):		0.01	00	0.01	0.01		00 0	.0100	
Up Invert (ft):		5098	3.34	5095	5095.97		.43 50	089.35	
Dn Invert (ft):		5096	5.07	5092	.53	.45 50	089.04		
Max Q (cfs):		0.6	33	3.2	26	32 1	7.53		
Max Vel (ft/s):		3.6		5.5			8.42		
Max Depth (ft):		0.2	27	0.5	5	0.8	34	1.01	

Project Description

C:\Users\Dash\AppData\Local\Temp\C2 Overall Plans_1_32432_bc64b9a7.sv\$

Project Options

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	. EPA SWMM
EPA SWMM Infiltration Method	Horton
Link Routing Method	. Steady Flow
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	YES

Analysis Options

Start Analysis On End Analysis On Start Reporting On Antecedent Dry Days Runoff (Dry Weather) Time Step Runoff (Wet Weather) Time Step	Jan 06, 2021 Jan 05, 2021 0 0 01:00:00	00:00:00
Runoff (Wet Weather) Time Step Reporting Time Step		days hh:mm:ss days hh:mm:ss
Routing Time Step		seconds

Number of Elements

	Qty
Rain Gages	0
Subbasins	0
Nodes	8
Junctions	7
Outfalls	1
Flow Diversions	0
Inlets	0
Storage Nodes	0
Links	7
Channels	0
Pipes	7
Pumps	0
Orifices	0
Weirs	0
Outlets	0
Pollutants	0
Land Uses	0

Node Summary

SN	Element ID	Element Type	Invert Elevation	Ground/Rim (Max)	Initial Water	Surcharge Elevation				Max Surcharge	Min Freeboard	Time of Peak	Total Flooded	Total Time Flooded
		.)		()	Elevation				Attained	Depth	Attained	Flooding		
										Attained		Occurrence		
			(ft)	(ft)	(ft)	(ft)	(ft ²)	(cfs)	(ft)	(ft)	(ft)	(days hh:mm)	(ac-in)	(min)
1	(ST MH-1) (P-STRM)	Junction	5097.26	5102.05	5097.26	5102.05	0.00	0.63	5097.55	0.00	4.50	0 00:00	0.00	0.00
2	(ST MH-2) (P-STRM)	Junction	5095.52	5101.27	5095.52	5101.27	0.00	1.26	5095.93	0.00	5.34	0 00:00	0.00	0.00
3	(ST MH-3) (P-STRM)	Junction	5094.73	5100.30	5094.73	5100.30	0.00	3.26	5095.30	0.00	5.00	0 00:00	0.00	0.00
4	(ST MH-4) (P-STRM)	Junction	5093.52	5099.43	5093.52	5099.43	0.00	3.26	5094.09	0.00	5.33	0 00:00	0.00	0.00
5	(ST MH-5) (P-STRM)	Junction	5091.70	5098.21	5091.70	5098.21	0.00	5.26	5092.46	0.00	5.75	0 00:00	0.00	0.00
6	(ST MH-6) (P-STRM)	Junction	5091.19	5097.79	5091.19	5097.79	0.00	6.92	5092.08	0.00	5.70	0 00:00	0.00	0.00
7	(ST MH-7) (P-STRM)	Junction	5089.53	5096.10	5089.53	5096.10	0.00	8.58	5090.56	0.00	5.54	0 00:00	0.00	0.00
8	(ST MH-8) (P-STRM)	Outfall	5088.99					8.58	5090.02					

Link Summary

SN Element ID	Element Type	From (Inlet) Node	To (Outlet) Node	Length	Inlet Invert Elevation	Invert	Slope	Diameter or Height	Manning's Roughness		Design Flow Capacity	Peak Flow/ Design Flow Ratio	Velocity
				(ft)	(ft)	(ft)	(%)	(in)		(cfs)	(cfs)		(ft/sec
1 {P-STRM}.(ST-1)	(P-STRM) Pipe	(ST MH-1) (P-STRM) (ST MH-2) (P-STRM)	174.04	5097.26	5095.52	1.0000	12.000	0.0130	0.63	3.56	0.18	3.41
2 {P-STRM}.(ST-2)	(P-STRM) Pipe	(ST MH-2) (P-STRM) (ST MH-3) (P-STRM)	79.34	5095.52	5094.73	1.0000	12.000	0.0130	1.26	3.56	0.35	4.14
3 {P-STRM}.(ST-3)	(P-STRM) Pipe	(ST MH-3) (P-STRM) (ST MH-4) (P-STRM)	120.83	5094.73	5093.52	1.0000	18.000	0.0130	3.26	10.50	0.31	5.24
4 {P-STRM}.(ST-4)	(P-STRM) Pipe	(ST MH-4) (P-STRM	(ST MH-5) (P-STRM)	181.48	5093.52	5091.70	1.0000	18.000	0.0130	3.26	10.51	0.31	5.24
5 {P-STRM}.(ST-5)	(P-STRM) Pipe	(ST MH-5) (P-STRM	(ST MH-6) (P-STRM)	51.06	5091.70	5091.19	1.0000	18.000	0.0130	5.26	10.50	0.50	5.94
6 (P-STRM).(ST-6)	(P-STRM) Pipe	(ST MH-6) (P-STRM) (ST MH-7) (P-STRM)	166.73	5091.19	5089.53	1.0000	18.000	0.0130	6.92	10.50	0.66	6.34
7 (P-STRM).(ST-7)	(P-STRM) Pipe	(ST MH-7) (P-STRM) (ST MH-8) (P-STRM)	53.74	5089.53	5088.99	1.0000	18.000	0.0130	8.58	10.50	0.82	6.62

Junction Input

SN Element ID	Invert Elevation	Ground/Rim (Max)	Ground/Rim (Max)	Initial Water	Initial Water	Surcharge Elevation	Surcharge Depth	Ponded Area	Minimum Pipe
	Lioradon	Elevation	()	Elevation		Lioration	Dopui	7.000	Cover
	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft²)	(in)
1 (ST MH-1) (P-STRM	5097.26	5102.05	4.79	5097.26	0.00	5102.05	0.00	0.00	45.48
2 (ST MH-2) (P-STRM	5095.52	5101.27	5.75	5095.52	0.00	5101.27	0.00	0.00	56.99
3 (ST MH-3) (P-STRM	5094.73	5100.30	5.57	5094.73	0.00	5100.30	0.00	0.00	48.88
4 (ST MH-4) (P-STRM	5093.52	5099.43	5.91	5093.52	0.00	5099.43	0.00	0.00	52.86
5 (ST MH-5) (P-STRM	5091.70	5098.21	6.50	5091.70	0.00	5098.21	0.00	0.00	60.02
6 (ST MH-6) (P-STRM	5091.19	5097.79	6.59	5091.19	0.00	5097.79	0.00	0.00	61.09
7 (ST MH-7) (P-STRM	5089.53	5096.10	6.57	5089.53	0.00	5096.10	0.00	0.00	60.85

Junction Results

SN	Element ID	Peak Inflow		Max HGL Elevation		Max Surcharge		0	Average HGL Depth	Time of Max HGL	Time of Peak	Total Flooded	Total Time Flooded
			Inflow	Attained	Attained	Depth	Attained	Attained	Attained	Occurrence	Flooding	Volume	
						Attained					Occurrence		
		(cfs)	(cfs)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(days hh:mm)	(days hh:mm)	(ac-in)	(min)
1	(ST MH-1) (P-STRM)	0.63	0.63	5097.55	0.29	0.00	4.50	5097.55	0.29	0 00:00	0 00:00	0.00	0.00
2	(ST MH-2) (P-STRM)	1.26	0.63	5095.93	0.41	0.00	5.34	5095.93	0.41	0 00:00	0 00:00	0.00	0.00
3	(ST MH-3) (P-STRM)	3.26	2.00	5095.30	0.57	0.00	5.00	5095.30	0.57	0 00:00	0 00:00	0.00	0.00
2	(ST MH-4) (P-STRM)	3.26	0.00	5094.09	0.57	0.00	5.33	5094.09	0.57	0 00:00	0 00:00	0.00	0.00
5	(ST MH-5) (P-STRM)	5.26	2.00	5092.46	0.76	0.00	5.75	5092.46	0.76	0 00:00	0 00:00	0.00	0.00
6	(ST MH-6) (P-STRM)	6.92	1.66	5092.08	0.89	0.00	5.70	5092.08	0.89	0 00:00	0 00:00	0.00	0.00
7	(ST MH-7) (P-STRM)	8.58	1.66	5090.56	1.03	0.00	5.54	5090.56	1.03	0 00:00	0 00:00	0.00	0.00

Pipe Input

SN	Element	Length	Inlet	Inlet	Outlet	Outlet	Total	Average Pipe	Pipe	Pipe	Manning's	Entrance	Exit/Bend	Additional
	ID		Invert	Invert	Invert	Invert	Drop	Slope Shape	Diameter or	Width	Roughness	Losses	Losses	Losses
			Elevation	Offset	Elevation	Offset			Height					
		(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(%)	(in)	(in)				
1	{P-STRM}.(ST-1) (P-STRM)	174.04	5097.26	0.00	5095.52	0.00	1.74	1.0000 CIRCULAR	12.000	12.000	0.0130	0.5000	0.5000	0.0000
2	{P-STRM}.(ST-2) (P-STRM)	79.34	5095.52	0.00	5094.73	0.00	0.79	1.0000 CIRCULAR	12.000	12.000	0.0130	0.5000	0.5000	0.0000
3	{P-STRM}.(ST-3) (P-STRM)	120.83	5094.73	0.00	5093.52	0.00	1.21	1.0000 CIRCULAR	18.000	18.000	0.0130	0.5000	0.5000	0.0000
4	{P-STRM}.(ST-4) (P-STRM)	181.48	5093.52	0.00	5091.70	0.00	1.82	1.0000 CIRCULAR	18.000	18.000	0.0130	0.5000	0.5000	0.0000
5	{P-STRM}.(ST-5) (P-STRM)	51.06	5091.70	0.00	5091.19	0.00	0.51	1.0000 CIRCULAR	18.000	18.000	0.0130	0.5000	0.5000	0.0000
6	{P-STRM}.(ST-6) (P-STRM)	166.73	5091.19	0.00	5089.53	0.00	1.67	1.0000 CIRCULAR	18.000	18.000	0.0130	0.5000	0.5000	0.0000
7	{P-STRM}.(ST-7) (P-STRM)	53.74	5089.53	0.00	5088.99	0.00	0.54	1.0000 CIRCULAR	18.000	18.000	0.0130	0.5000	0.5000	0.0000

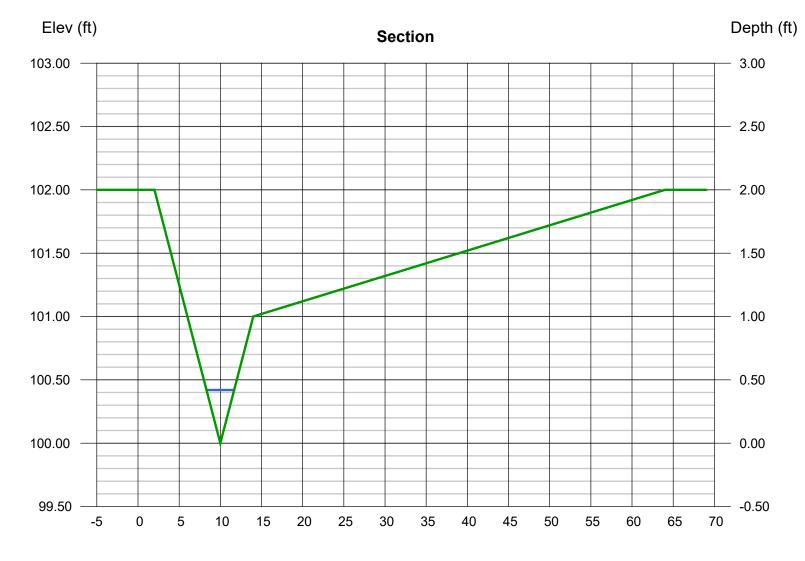
Pipe Results

SN Element	Peak	Time of	Design Flow	Peak Flow/	Peak Flow	Travel	Peak Flow	Peak Flow	Total Time	Froude Reported
ID	Flow	Peak Flow	Capacity	Design Flow	Velocity	Time	Depth	Depth/	Surcharged	Number Condition
		Occurrence		Ratio				Total Depth		
								Ratio		
	(cfs)	(days hh:mm)	(cfs)		(ft/sec)	(min)	(ft)		(min)	
1 {P-STRM}.(ST-1) (P-STRM)	0.63	0 00:00	3.56	0.18	3.41	0.85	0.29	0.29	0.00	Calculated
2 {P-STRM}.(ST-2) (P-STRM)	1.26	0 00:00	3.56	0.35	4.14	0.32	0.41	0.41	0.00	Calculated
3 {P-STRM}.(ST-3) (P-STRM)	3.26	0 00:00	10.50	0.31	5.24	0.38	0.57	0.38	0.00	Calculated
4 {P-STRM}.(ST-4) (P-STRM)	3.26	0 00:00	10.51	0.31	5.24	0.58	0.57	0.38	0.00	Calculated
5 {P-STRM}.(ST-5) (P-STRM)	5.26	0 00:00	10.50	0.50	5.94	0.14	0.75	0.50	0.00	Calculated
6 {P-STRM}.(ST-6) (P-STRM)	6.92	0 00:00	10.50	0.66	6.34	0.44	0.89	0.59	0.00	Calculated
7 {P-STRM}.(ST-7) (P-STRM)	8.58	0 00:00	10.50	0.82	6.62	0.14	1.03	0.69	0.00	Calculated

Tuesday, May 18 2021

Basin HA-1 Swale - 5-yr Storm Event

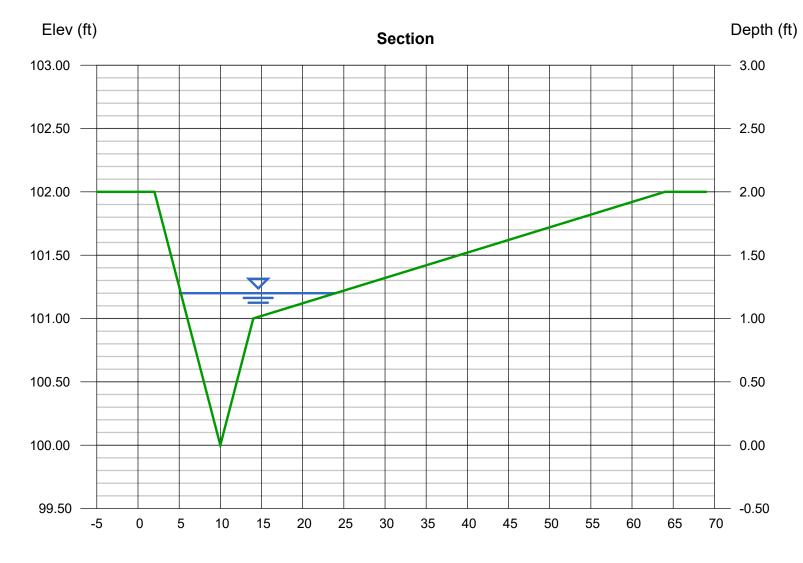
User-defined		Highlighted	
Invert Elev (ft)	= 100.00	Depth (ft)	= 0.42
Slope (%)	= 0.50	Q (cfs)	= 0.800
N-Value	= 0.032	Area (sqft)	= 0.71
		Velocity (ft/s)	= 1.13
Calculations		Wetted Perim (ft)	= 3.46
Compute by:	Known Q	Crit Depth, Yc (ft)	= 0.31
Known Q (cfs)	= 0.80	Top Width (ft)	= 3.36
		EGL (ft)	= 0.44



Tuesday, May 18 2021

Basin HA-1 Swale - 100-yr Storm Event

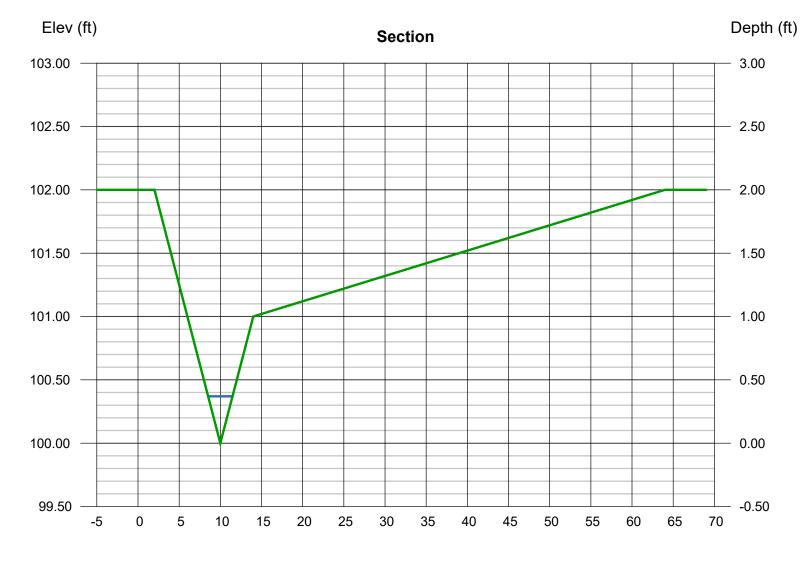
User-defined		Highlighted	
Invert Elev (ft)	= 100.00	Depth (ft)	= 1.20
Slope (%)	= 0.50	Q (cfs)	= 18.87
N-Value	= 0.032	Area (sqft)	= 6.68
		Velocity (ft/s)	= 2.82
Calculations		Wetted Perim (ft)	= 19.07
Compute by:	Known Q	Crit Depth, Yc (ft)	= 1.14
Known Q (cfs)	= 18.87	Top Width (ft)	= 18.80
		EGL (ft)	= 1.32



Tuesday, May 18 2021

Basin HA-1 Swale - 5-yr Storm Event

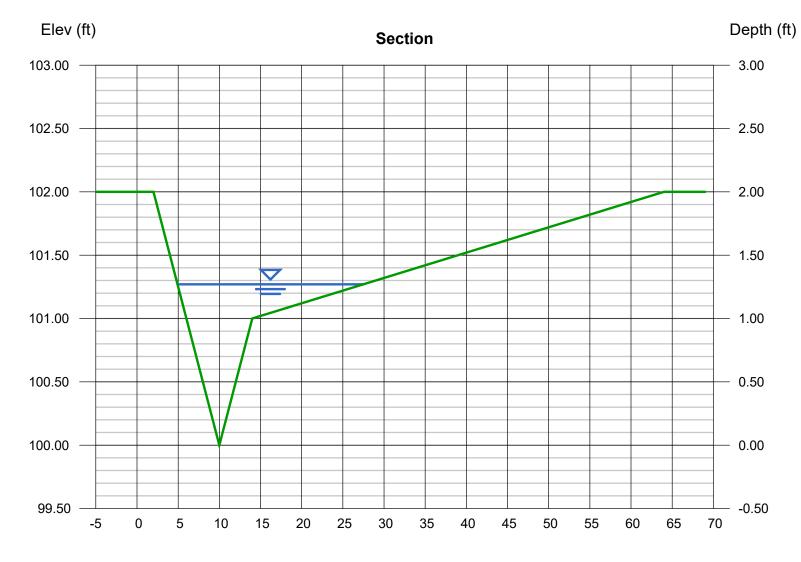
User-defined		Highlighted	
Invert Elev (ft)	= 100.00	Depth (ft)	= 0.37
Slope (%)	= 1.00	Q (cfs)	= 0.800
N-Value	= 0.032	Area (sqft)	= 0.55
		Velocity (ft/s)	= 1.46
Calculations		Wetted Perim (ft)	= 3.05
Compute by:	Known Q	Crit Depth, Yc (ft)	= 0.31
Known Q (cfs)	= 0.80	Top Width (ft)	= 2.96
		EGL (ft)	= 0.40



Tuesday, May 18 2021

Basin HA-1 Swale - 100-yr Storm Event

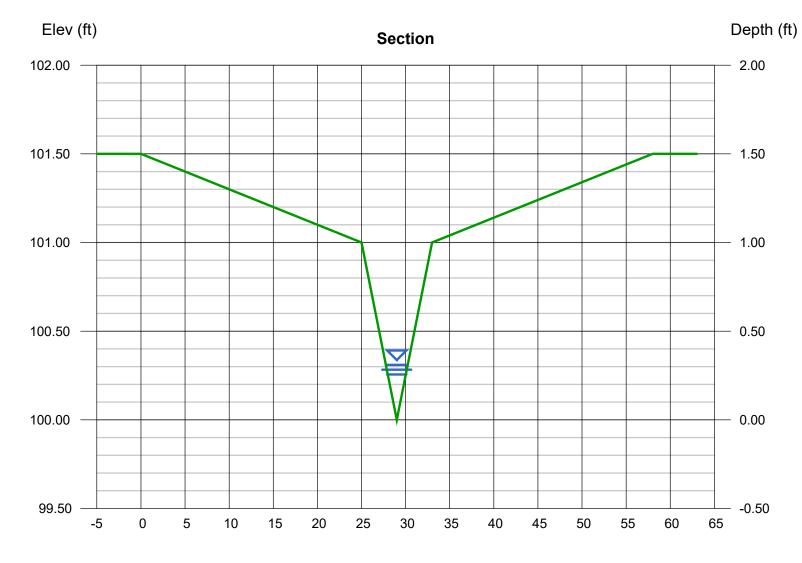
User-defined		Highlighted	
Invert Elev (ft)	= 100.00	Depth (ft)	= 1.27
Slope (%)	= 1.00	Q (cfs)	= 18.87
N-Value	= 0.032	Area (sqft)	= 8.13
		Velocity (ft/s)	= 2.32
Calculations		Wetted Perim (ft)	= 22.86
Compute by:	Known Q	Crit Depth, Yc (ft)	= 1.14
Known Q (cfs)	= 18.87	Top Width (ft)	= 22.58
		EGL (ft)	= 1.35



Friday, May 21 2021

Basin HA-2 Swale - 5-yr Storm Event

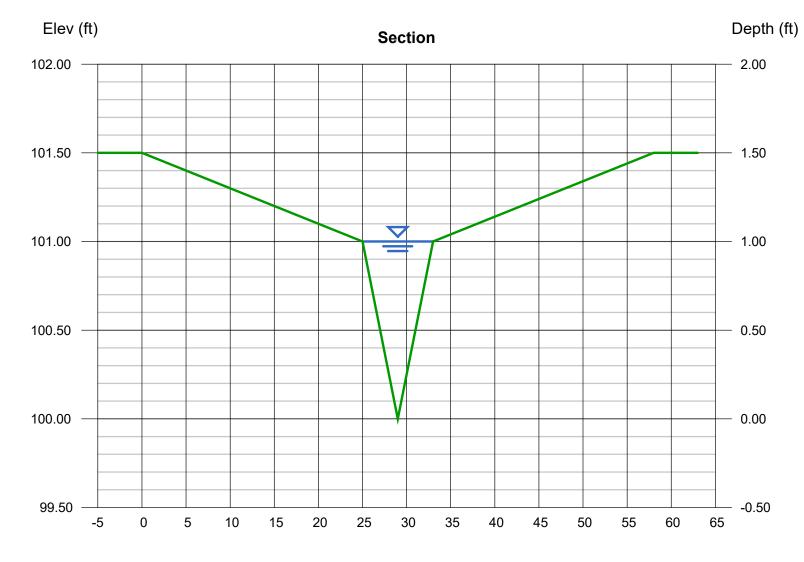
User-defined		Highlighted	
Invert Elev (ft)	= 100.00	Depth (ft)	= 0.31
Slope (%)	= 0.90	Q (cfs)	= 0.460
N-Value	= 0.032	Area (sqft)	= 0.38
		Velocity (ft/s)	= 1.20
Calculations		Wetted Perim (ft)	= 2.56
Compute by:	Known Q	Crit Depth, Yc (ft)	= 0.25
Known Q (cfs)	= 0.46	Top Width (ft)	= 2.48
		EGL (ft)	= 0.33



Friday, May 21 2021

Basin HA-2 Swale - 100-yr Storm Event

User-defined		Highlighted	
Invert Elev (ft)	= 100.00	Depth (ft)	= 1.00
Slope (%)	= 0.90	Q (cfs)	= 10.79
N-Value	= 0.032	Area (sqft)	= 4.00
		Velocity (ft/s)	= 2.70
Calculations		Wetted Perim (ft)	= 8.25
Compute by:	Known Q	Crit Depth, Yc (ft)	= 0.86
Known Q (cfs)	= 10.79	Top Width (ft)	= 8.00
		EGL (ft)	= 1.11



HYDRAULIC CALCULATIONS (EXISTING IMPROVEMENTS)

Culvert Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Thursday, Oct 10 2019

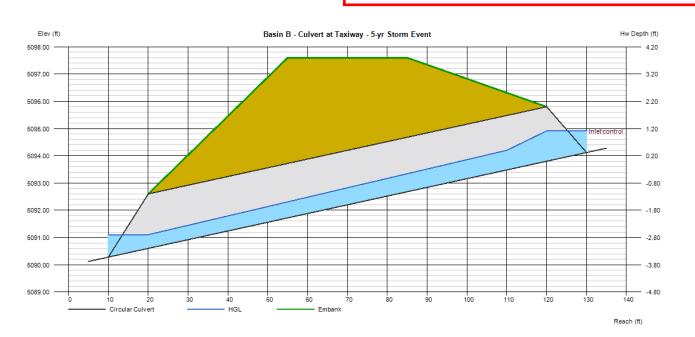
Basin B - Culvert at Taxiway - 5-yr Storm Event

Invert Elev Dn (ft)	= 5090.60	Calculations	
Pipe Length (ft)	= 100.00	Qmin (cfs)	= 4.52
Slope (%)	= 3.20	Qmax (cfs)	= 4.52
Invert Èlev Up (ft)	= 5093.80	Tailwater Élev (ft)	= 0.00
Rise (in)	= 24.0		
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 4.52
No. Barrels	= 1	Qpipe (cfs)	= 4.52
n-Value	= 0.016	Qovertop (cfs)	= 0.00
Culvert Type	 Circular Corrugate Metal Pipe 	Veloc Dn (ft/s)	= 7.31
Culvert Entrance	= Mitered to slope (C)	Veloc Up (ft/s)	= 4.22
Coeff. K,M,c,Y,k	= 0.021, 1.33, 0.0463, 0.75, 0.7	HGL Dn (ft)	= 5091.10
		HGL Up (ft)	= 5094.55
Embankment		Hw Elev (ft)	= 5094.91
Top Elevation (ft)	= 5097.60	Hw/D (ft)	= 0.56
Top Width (ft)	= 30.00	Flow Regime	= Inlet Control

Crest Width (ft)

=	5097.6
=	30.00
=	60.00

Existing culvert. NE corner of Tract E-1



Culvert Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Thursday, Oct 10 2019

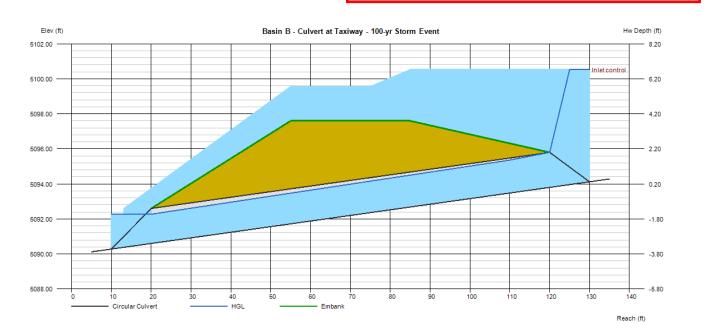
Basin B - Culvert at Taxiway - 100-yr Storm Event

Invert Elev Dn (ft)	= 5090.60	Calculations	
Pipe Length (ft)	= 100.00	Qmin (cfs)	= 33.23
Slope (%)	= 3.20	Qmax (cfs)	= 33.23
Invert Elev Up (ft)	= 5093.80	Tailwater Elev (ft)	= 0.00
Rise (in)	= 24.0		
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 33.23
No. Barrels	= 1	Qpipe (cfs)	= 33.23
n-Value	= 0.016	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Corrugate Metal Pipe	Veloc Dn (ft/s)	= 11.86
Culvert Entrance	= Mitered to slope (C)	Veloc Up (ft/s)	= 10.77
Coeff. K,M,c,Y,k	= 0.021, 1.33, 0.0463, 0.75, 0.7	HGL Dn (ft)	= 5092.27
		HGL Up (ft)	= 5095.70
Embankment		Hw Elev (ft)	= 5100.53
Top Elevation (ft)	= 5097.60	Hw/D (ft)	= 3.36
Top Width (ft)	= 30.00	Flow Regime	= Inlet Control
· · · · · · · · · · · · · · · · · · ·		~	

Crest Width (ft)

= 200.00

Existing culvert. NE corner of Tract E-1



Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

= 4.52

Thursday, Oct 10 2019

Basin B1 Swale - 5-yr Storm Event

Triangular

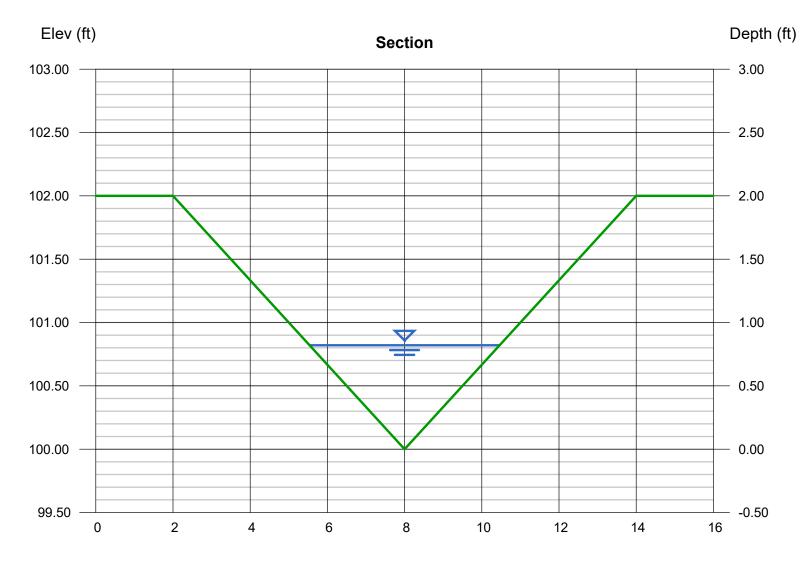
Side Slopes (z:1)	= 3.00, 3.00
Total Depth (ft)	= 2.00
Invert Elev (ft)	= 100.00
Slope (%)	= 1.00
N-Value	= 0.035
Calculations Compute by:	Known Q

Compute by: Known Q (cfs)

Highlighted

Depth (ft)	= 0.82
Q (cfs)	= 4.520
Area (sqft)	= 2.02
Velocity (ft/s)	= 2.24
Wetted Perim (ft)	= 5.19
Crit Depth, Yc (ft)	= 0.68
Top Width (ft)	= 4.92
EGL (ft)	= 0.90

Existing swale East side of Tract E-1



Reach (ft)

Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Thursday, Oct 10 2019

Basin B1 Swale - 100-yr Storm Event

= 33.23

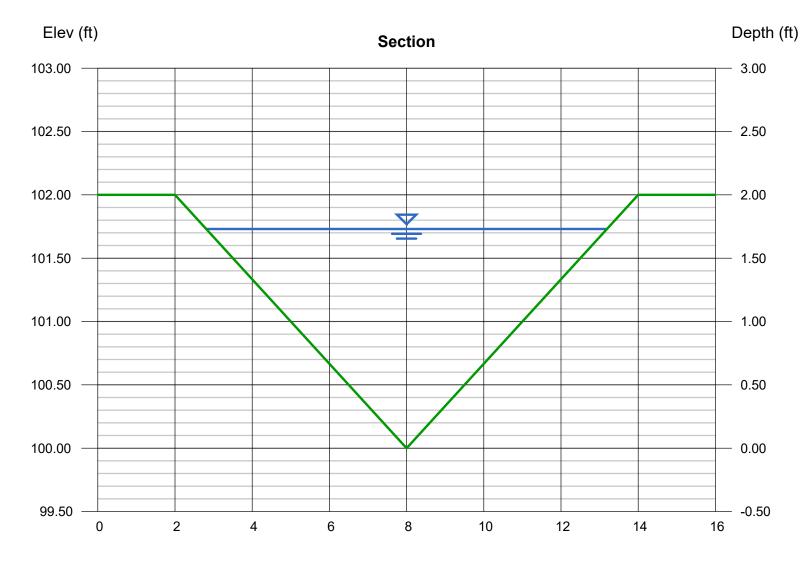
Triangular

Side Slopes (z:1)	= 3.00, 3.00
Total Depth (ft)	= 2.00
Invert Elev (ft)	= 100.00
Slope (%)	= 1.00
N-Value	= 0.035
Calculations Compute by:	Known Q

Compute by: Known Q (cfs)

Highlighted		
Depth (ft)	=	1.73
Q (cfs)	=	33.23
Area (sqft)	=	8.98
Velocity (ft/s)	=	3.70
Wetted Perim (ft)	=	10.94
Crit Depth, Yc (ft)	=	1.51
Top Width (ft)	=	10.38
EGL (ft)	=	1.94

Existing swale East side of Tract E-1



Culvert Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Thursday, Oct 10 2019

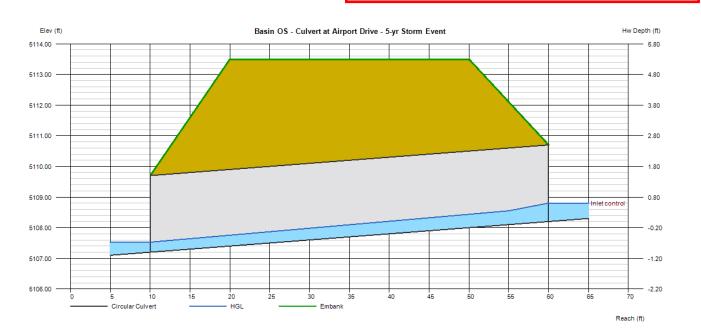
Basin OS - Culvert at Airport Drive - 5-yr Storm Event

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft)	= 5107.20 = 50.00 = 2.00 = 5108.20	Calculations Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 2.03 = 2.03 = 0.00
Rise (in)	= 30.0		- 0.00
Shape	= Circular	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 2.03
No. Barrels	= 1	Qpipe (cfs)	= 2.03
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	 Circular Concrete 	Veloc Dn (ft/s)	= 5.37
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 3.23
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 5107.53
		HGL Up (ft)	= 5108.67
Embankment		Hw Elev (ft)	= 5108.80
Top Elevation (ft)	= 5113.50	Hw/D (ft)	= 0.24
Top Width (ft)	= 30.00	Flow Regime	= Inlet Control

Top Width (ft) Crest Width (ft)

=	5113.50
=	30.00
=	100.00

Existing culvert SE corner of Tract E-1



Culvert Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Thursday, Oct 10 2019

Basin OS - Culvert at Airport Drive - 100-yr Storm Event

Invert Elev Dn (ft)	= 5107.20	Calculations	
Pipe Length (ft)	= 50.00	Qmin (cfs)	= 23.89
Slope (%)	= 2.00	Qmax (cfs)	= 23.89
Invert Elev Up (ft)	= 5108.20	Tailwater Elev (ft)	= 0.00
Rise (in)	= 30.0	. ,	
Shape	= Circular	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 23.89
No. Barrels	= 1	Qpipe (cfs)	= 23.89
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 10.13
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 6.89
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 5108.41
		HGL Up (ft)	= 5109.86
Embankment		Hw Elev (fť)	= 5110.81
Top Elevation (ft)	= 5113.50	Hw/D (ft)	= 1.04
Top Width (ft)	= 30.00	Flow Regime	= Inlet Control
		0	

p wiain (ii) Crest Width (ft)

=	5113.50
=	30.00
=	100.00

Existing culvert SE corner of Tract E-1



<u>APPENDIX E</u>

RELEVANT DOCUMENTS

Land Use or	Percentage Imperviousness		
Surface Characteristics	(%)		
Business:			
Downtown Areas	95		
Suburban Areas	75		
Residential lots (lot area only):			
Single-family			
2.5 acres or larger	12		
0.75 – 2.5 acres	20		
0.25 – 0.75 acres	30		
0.25 acres or less	45		
Apartments	75		
Industrial:			
Light areas	80		
Heavy areas	90		
Parks, cemeteries	10		
Playgrounds	25		
Schools	55		
Railroad yard areas	50		
Undeveloped Areas:	·		
Historic flow analysis	2		
Greenbelts, agricultural	2		
Off-site flow analysis (when land use not defined)	45		
Streets:			
Paved	100		
Gravel (packed)	40		
Drive and walks	90		
Roofs	90		
Lawns, sandy soil	2		
Lawns, clayey soil	2		

Table 6-3. Recommended percentage imperviousness values

	Chapter	6
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Table 0-3. Kunon coemcients, c (continueu)							
Total or Effective		NRCS Hydrologic Soil Group C					
% Impervious	2-Year	5-Year	10-Year	25-Year	50-Year	100-Year	500-Year
2%	0.01	0.05	0.15	0.33	0.40	<mark>0.49</mark>	<mark>0.59</mark>
5%	0.03	0.08	0.17	0.35	0.42	0.5	0.6
10%	0.06	0.12	0.21	0.37	0.44	0.52	0.62
15%	0.1	0.16	0.24	0.4	0.47	0.55	0.64
20%	0.14	0.2	0.28	0.43	0.49	0.57	0.65
25%	0.18	0.24	0.32	0.46	0.52	0.59	0.67
30%	0.22	0.28	0.35	0.49	0.54	0.61	0.68
35%	0.26	0.32	0.39	0.51	0.57	0.63	0.7
40%	0.3	0.36	0.43	0.54	0.59	0.65	0.71
45%	0.34	0.4	0.46	0.57	0.62	0.67	0.73
50%	0.38	0.44	0.5	0.6	0.64	0.69	0.75
55%	0.43	0.48	0.54	0.63	0.66	0.71	0.76
60%	0.47	0.52	0.57	0.65	0.69	0.73	0.78
65%	0.51	0.56	0.61	0.68	0.71	0.75	0.79
70%	0.56	0.61	0.65	0.71	0.74	0.77	0.81
75%	0.6	0.65	0.68	0.74	0.76	0.79	0.82
80%	<mark>0.65</mark>	<mark>0.69</mark>	0.72	<mark>0.77</mark>	<mark>0.79</mark>	0.81	<mark>0.84</mark>
85%	0.7	0.73	0.76	0.79	0.81	0.83	0.86
<mark>90%</mark>	<mark>0.74</mark>	<mark>0.77</mark>	<mark>0.79</mark>	0.82	<mark>0.84</mark>	0.85	<mark>0.87</mark>
95%	0.79	0.81	0.83	0.85	0.86	0.87	0.89
100%	0.83	0.85	0.87	0.88	0.89	0.89	0.9

 Table 6-5. Runoff coefficients, c (continued)

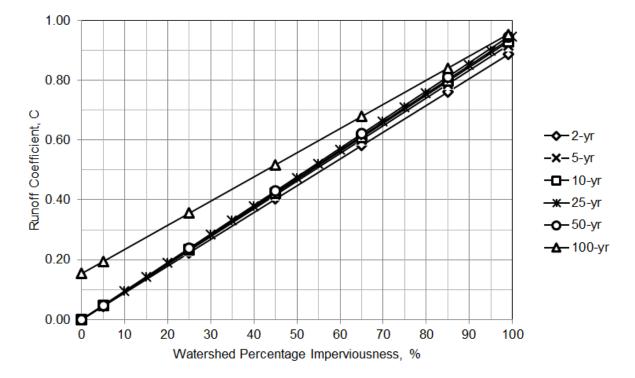


Figure 6-1. Runoff coefficient vs. watershed imperviousness NRCS HSG A

STORM DRAINAGE FACILITIES

existence or function of a ditch. If a variance is requested to the Town Engineer for use of a ditch as an outfall, it is the design engineer's responsibility to complete all studies and designs deemed necessary by the Town Engineer to support the use of the ditch as well as a secondary drainage design should the ditch cease to exist.

Expressed written approval must be obtained from the managing organization for irrigation ditches being considered for crossing or easements.

813.00 Design Methods

813.01 Initial and Major Design Storms

Every urban area has two separate and distinct drainage systems whether or not they are actually planned for and designed. One is the initial system corresponding to the initial (or ordinary) storm recurring at regular intervals. The other is the major system corresponding to the major (or extraordinary storm), which is unlikely to occur more often than once in 100 or more years. Since the effects and routing of storm waters for the major storm may not be the same as for the initial storm, all storm drainage plans submitted for acceptance will detail two separate systems; one indicating the effects of the initial storm and the other showing the effects of the major storm.

- A. *Initial storm provisions:* The objectives of such drainage system planning are to minimize inconvenience, to protect against recurring minor damage, to reduce rising maintenance costs, and to create an orderly drainage system. The initial storm drainage system may include such facilities as curb and gutter, storm sewer, swales, and other open drainageways and detention facilities.
- B. *Major storm provisions:* The major storm will be considered the 100-year storm. The objectives of the major storm planning are to eliminate substantial property damage or loss of life and will be as directed and accepted by the Town Engineer. Major drainage systems may include storm sewers, open drainageways and detention facilities. The correlation between the initial and major storm system will be analyzed to insure a well-coordinated drainage system.
- 813.02 Storm Return Periods

The initial and major storm design return periods will not be less than those found in Table 800-1:

Land Use or Zoning	Design Storm Return Period		
	Initial Storm	Major Storm	
Residential	2-year	100-year	
Commercial and Business	5-year	100-year	
Public Building Areas	5-year	100-year	
Parks, Greenbelts, etc.	2-year	100-year	

TABLE 800-1DESIGN STORM RETURN PERIODS

813.03 Runoff Computations, Colorado Urban Hydrograph Procedure (CUHP)

The CUHP method is generally applicable to drainage basins greater than 90 acres. However, the CUHP is required for watershed areas larger than 160-acres. The procedures for the CUHP, as explained in the Urban Storm Drainage Criteria Manual, shall be followed in the preparation of drainage reports and storm drainage facility designs in the Town. The CUHP program requires the input of a design storm, either as a detailed hyetograph or as a 1-hour rainfall depth. The program for the latter using the 2-hour storm distribution recommended in the Urban Storm Drainage Criteria Manual generates a detailed hyetograph distribution. The 1-hour rainfall depths for the Town of Erie are presented in Table 800-2.

Table 800-2 TOWN OF ERIE ONE-HOUR RAINFALL DEPTH						
Design Storm	1	Rainfall Dept	<mark>h (in.)</mark>			
2-Year		0.81				
5-Year		1.11				
10-Year		1.39				
25-Year		1.84				
50-Year		2.24				
100-Year		2.68				
500-Year		<mark>3.89</mark>				

The hydrograph from the CUHP program must be routed through any proposed conveyance facility using the Storm Water Management Model (SWMM) or a similar method approved by the Town Engineer.

813.04 Runoff Computations, Rational Method

The Rational Method will be utilized for sizing storm sewers and for determining runoff magnitude from un-sewered areas. The limit of application of the Rational Method is approximately 160 acres. When the drainage basin exceeds 160 acres, the CUHP method shall be used. The procedures for the Rational Method, as explained in the Urban Storm Drainage Criteria Manual, shall be followed in the preparation of drainage reports in the Town.

813.05 Runoff Coefficients

<u>Rational method runoff coefficients</u>: The runoff coefficient (C) to be used in conjunction with the Rational Method will be calculated using the percent imperviousness shown in Table 800-3 as explained in the Urban Storm Drainage Criteria Manual.

LAND USE OR SURFACE	PERCENT	
CHARACTERISTICS	IMPERVIOUS	
Business		
Commercial Areas	95 75	
Neighborhood Areas	75	
Residential Lots (Lot Area Only):		
Single-Family		
2.5 Acres or Larger	12	
0.75 – 2.49 Acres	20	
0.25 – 0.74 Acres	30	
0.24 Acres or Less	45	
Apartments	75	
Industrial:		
Light Areas	<mark>80</mark>	
Heavy Areas	90	
Parks, Cemeteries	10	
Playgrounds	25	
Schools	55	
Railroad Yard Areas	50	
Undeveloped Areas:		
Historic Flow Analysis	2	
Greenbelts, Agricultural	2 2 45	
Offsite Flow Analysis	45	
(when land use not defined)		
Streets:		
Paved	100	
Gravel (Packed)	40	
Drives and Walks	<mark>.90</mark>	
Roofs	<mark>.90</mark>	
Lawns, Sandy Soil	2	
Lawns, Clay Soil	2	

TABLE 800-3PERCENT IMPERVIOUS FOR RATIONAL METHOD

Note: These Rational Method coefficients may not be valid for large basins.

813.06 Rainfall Intensities

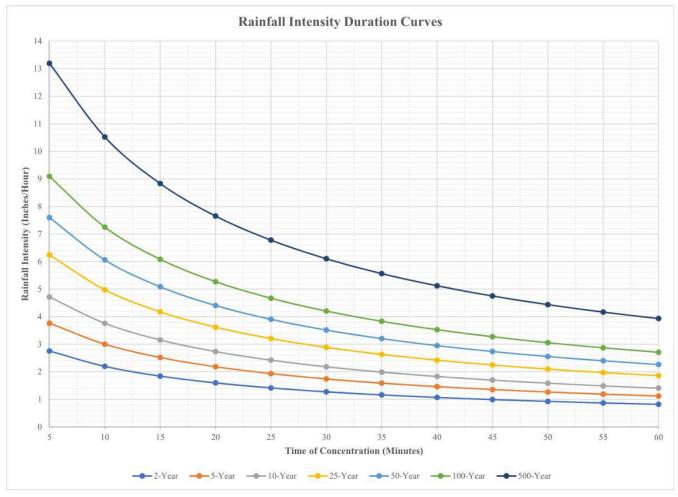
The rainfall intensities to be used in the computation of runoff using the Rational Method shall be obtained from the Rainfall Intensity Duration Curves for the Town of Erie, included in these STANDARDS AND SPECIFICATIONS, or can be computed using the following equation.

$$I = \frac{28.5 P_1}{(10 + T_d)^{0.786}}$$

Where:

I = rainfall intensity (inches per hour) $P_1 =$ 1-hour point rainfall depth (inches) $T_2 =$ storm duration (minutes)

 T_d = storm duration (minutes)



814.00 Detention

814.01 General

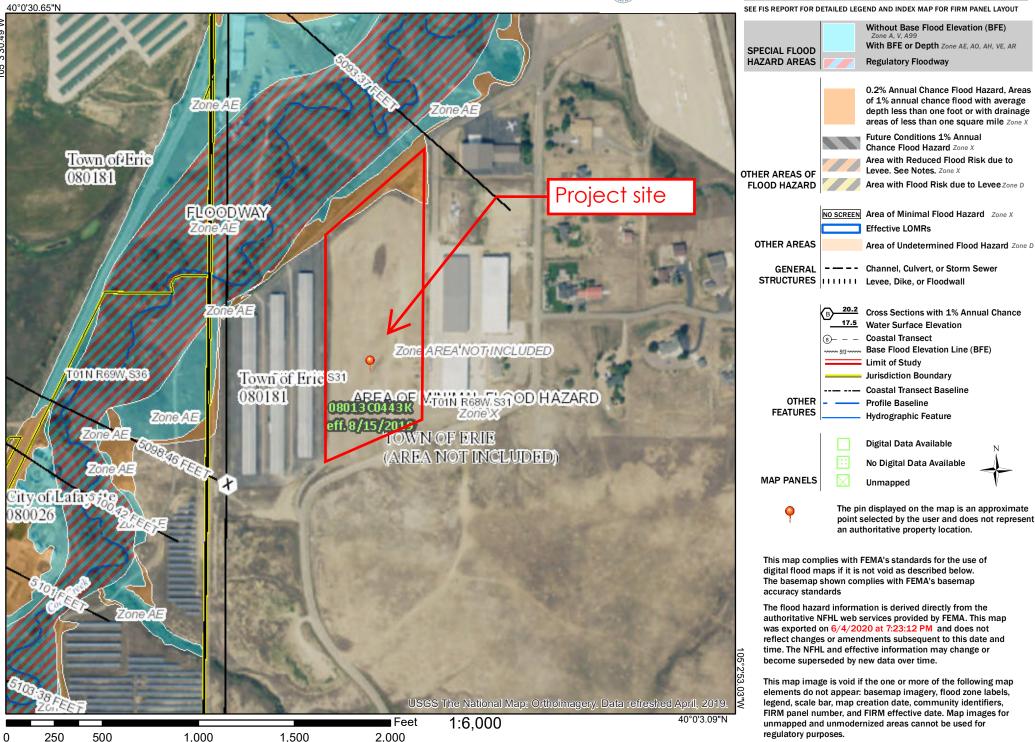
Onsite detention is required for all new development, expansion, and redevelopment. The required minimum detention volume and maximum release rates at these volumes shall be determined in accordance with the procedure and data set forth in these criteria.

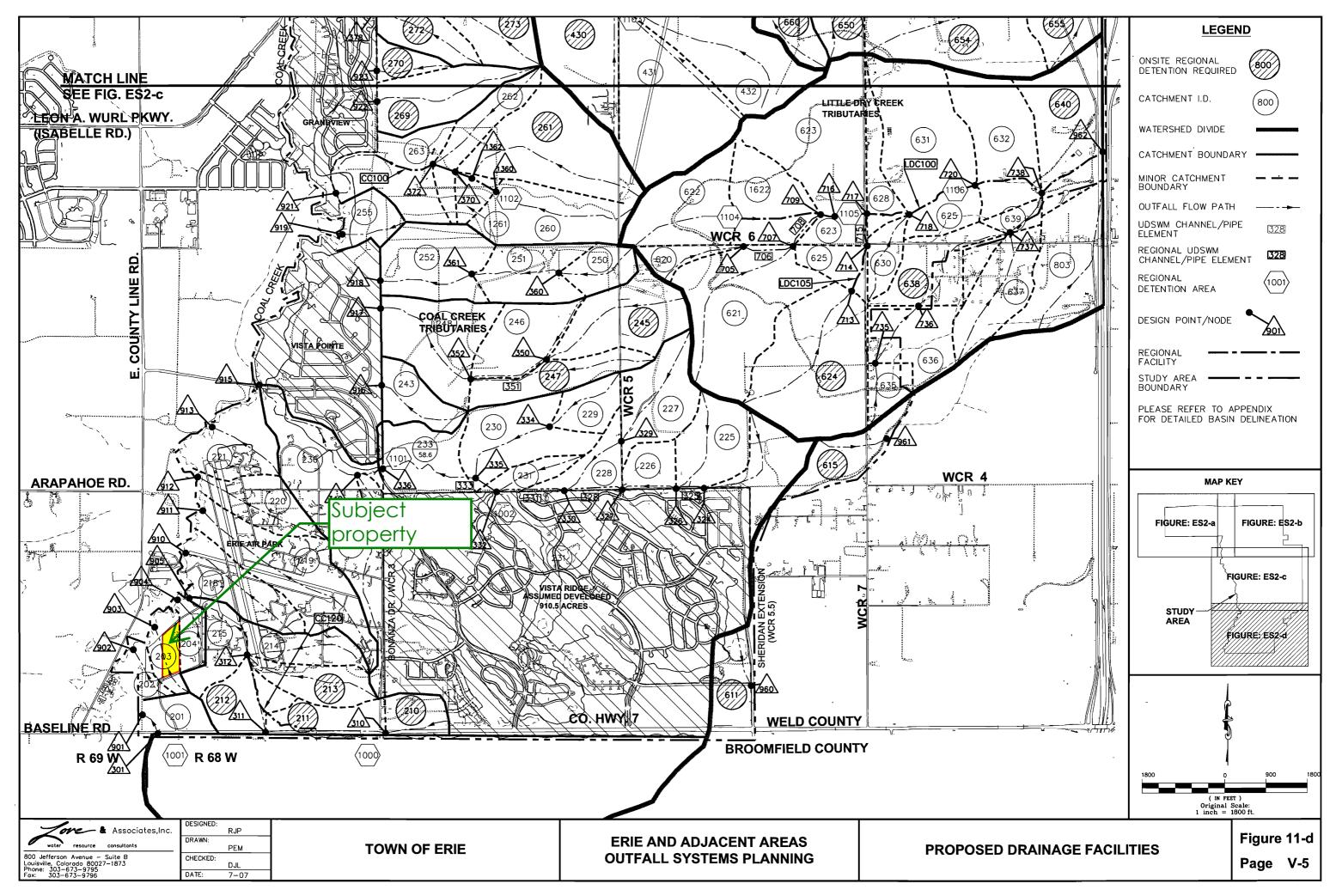
For lands where the Town has adopted a Master Drainage Plan or Outfall Systems Plan, detention facilities identified in the Master Drainage Plan or Outfall Systems Plan shall be constructed. For lands where there is no Master Drainage Plan or Outfall Systems Plan, detention is required for all

National Flood Hazard Layer FIRMette

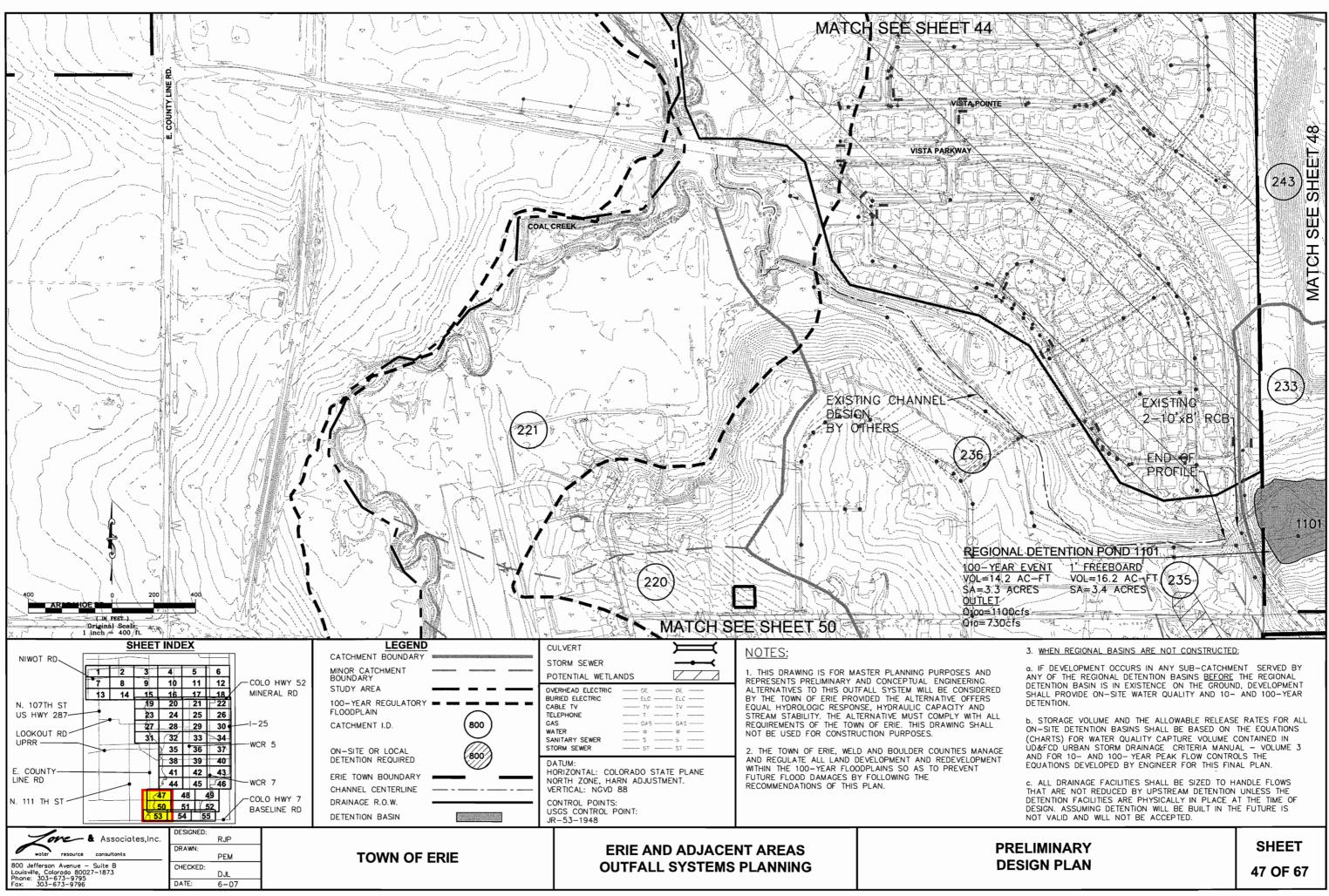


Legend





5:28:55 PM, LOVE & ASSOCIATES, INC. 8/8/2007 .dwg, ES-REV \Server\Data\PROJECTS - CURRENT\0603B\DRAWINGS\PRELIM BY SHEETS\PROP DRAINAGE FACILITI



COMMENTARY ON SHEET 48

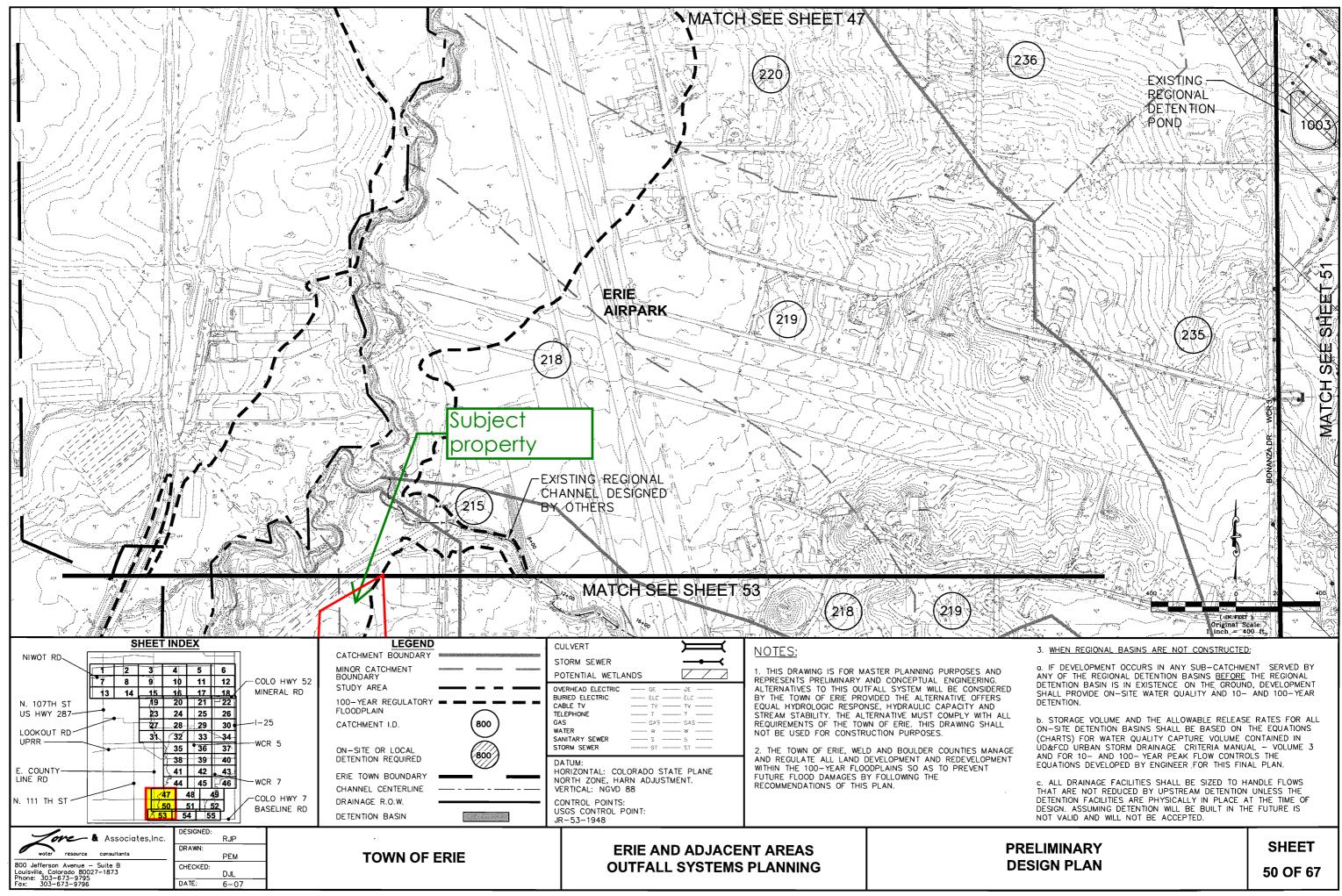
No Regional Outfall System improvements are required on this sheet. (See Sheet 47 for Regional Detention Facility 1101.)

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COMMENTARY ON SHEET 51

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No Regional Outfall System improvements are required on this sheet.

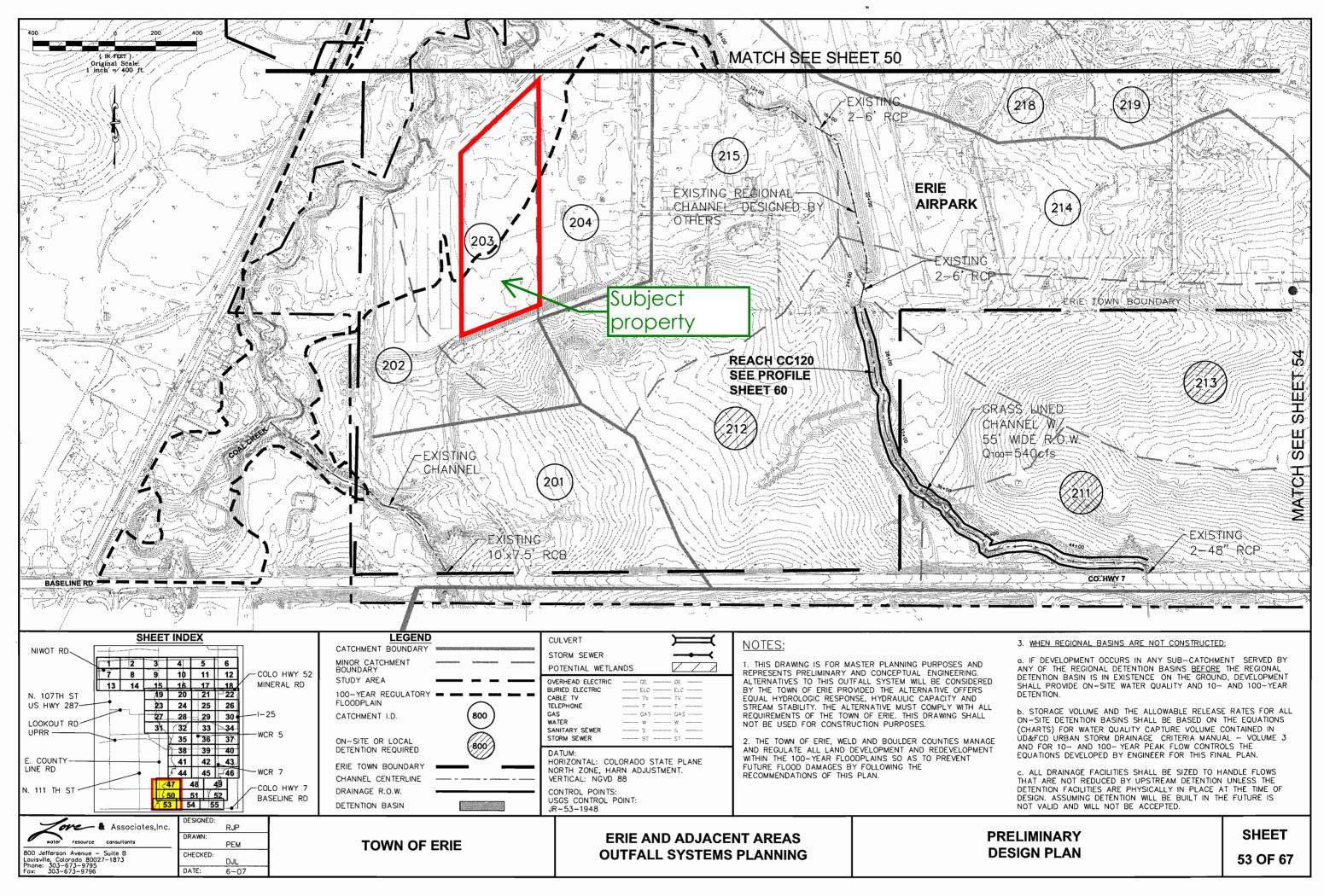
Existing Detention Facility 1102 designed and constructed by others is also shown on this sheet.

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COMMENTARY ON SHEET 54

No Regional Outfall System improvements are required on this sheet.

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FINAL DRAINAGE REPORT

ERIE CONVAIR HANGAR COMPLEX 3000 AIRPORT DRIVE ERIE, COLORADO

October 9, 2008 *Revised: March 23, 2009*

Prepared for:

Erie Convair LLC 3000 Airport Drive, Erie, Colorado

Prepared by:

SCOTT, COX & ASSOCIATES, INC.

consulting engineers - surveyors 1530 55th Street, Boulder, Colorado 303-444-3051

Project No. 06535F

ENGINEER'S STATEMENT

I hereby certify that this report for the final drainage design of the Erie Convair Hangar Complex was prepared under my direct supervision in accordance with the provisions of the Town of Erie Design and Development Standards for the owners thereof.

> Donald P. Ash, P.E. Registered Professional Engineer State of Colorado No. 36045

TABLE OF CONTENTS

Page Number

INTRODUCTION	1
DRAINAGE BASIN DESCRIPTION	1
OFFSITE DRAINAGE	1
PROPOSED ON-SITE DRAINAGE	2
DRAINAGE DESIGN CRITERIA	2
DETENTION STORAGE AND WATER QUALITY POND	3
STORM WATER QUALITY AND EROSION CONTROL	4
FLOOD STATEMENT	4
CONCLUSION	4
APPENDIX A - DRAINAGE BASIN RUNOFF CALCULATIONS	
APPENDIX B - HYDRAULIC CALCULATIONS	
APPENDIX C - WATER QUALITY POND CALCULATIONS	

INTRODUCTION

This report is submitted as the final drainage design study of the historic and developed conditions for the proposed and existing commercial airport development at 3000 Airport Drive. The site is located in the northwest quarter of the southwest quarter of Section 31, Township 1 North, Range 68 West of the 6th Principal Meridian in the Town of Erie, Weld County, State of Colorado. The area of the project site is approximately 7.88 acres. This project involves the construction of a water quality pond on the adjacent lot for the existing Convair Lot 2 development and a portion of the proposed Schofield Tract E development.

This drainage report analyzes the existing storm runoff and the storm runoff based on the existing and proposed improvements. This study meets the requirements set forth in the <u>Town of Erie Standards and Specifications for Design and Construction</u> <u>of Public Improvements</u>.

DRAINAGE BASIN DESCRIPTION

An existing commercial development to the north, existing aircraft hangars to the west, and Airport Drive to the east and south currently border the site. The western portion of the Lot 2 site (Basin A) currently slopes from the southeast towards the northwest, to an existing inlet that crosses the Taxiway DELTA. From there flows are directed into an existing sedimentation basin that discharges into the Coal Creek Drainageway. The location of this sedimentation basin will be the future location of the proposed water quality pond. The eastern portion of the Lot 2 site (Basin C) flows from the southwest to the northeast into the Airport Drive right-of-way, ultimately discharging into the existing water quality pond located on the Rocky Mountain Propeller site. The elevation differential across the site is approximately 5 feet.

OFFSITE DRAINAGE



The adjacent undeveloped property to the west (Basin B), contains approximately 10.94 acres, and currently flows via overland and channel flow into the existing sedimentation basin. The developed runoff from this basin will ultimately flow through the proposed site via overland and channel flow, into the proposed water quality pond. Developed runoff calculations for Basin B are provided in Appendix A. No other significant flows enter from offsite.

PROPOSED ON-SITE DRAINAGE

The Grading, Drainage and Erosion Control Plan shows the proposed on-site grading and drainage improvements. Under developed conditions, runoff from Basin A will be directed via sheet/gutter/channel flow and a storm pipe to the proposed water quality pond located at the northeast corner of Tract E. All roof drainage will be directed to the proposed water quality pond. Runoff from a portion of the Tract E development will also be conveyed to the north and east via overland and gutter flow to the proposed water quality pond. Runoff from Basin C will be directed northeast to the existing water quality pond located at the northeast corner of the Rocky Mountain Propeller site. Proposed runoff from the 5-year, 10-year and 100-year storms are provided in Appendix A.

DRAINAGE DESIGN CRITERIA

As required in the <u>Town of Erie Standards and Specifications for Design and</u> <u>Construction of Public Improvements</u> for all non-single family residential uses, hydrologic information was developed for an initial storm return period of 5-years and major storm return period of 100-years. The criteria and methodology used in determining the storm runoff peaks and volumes were those outlined in the Standards and Specifications.

The design rainfall data used in this study was taken from the time-intensityfrequency curve for the Town of Erie (Section 813.06) as developed by Urban Drainage and Flood Control District (UD&FCD). Runoff calculations were obtained using the Rational Method as outlined in the Standards and Specifications for basins having less than 160 acres.

The Rational Formula is:

Q = CIA

Where:

- Q = Peak Discharge (cfs)C = Runoff Coefficient (Table 7-2 CBDCS)
 - I = Rainfall Intensity (in/hr) (Figure 7-1 CBDCS)
 - A = Drainage Basin Tributary Area (acres)

The exiting and proposed conditions were analyzed for the 5-year, 10-year, and 100year storm events and runoffs were calculated. These results are shown in the following Table 1. Calculation sheets are provided in Appendix A. Open channels and drainage ways have been designed to convey the 10-year storm event and the storm pipe has been designed to convey the 5-year storm event.

<u>Drainage Basin</u>	<u>Area</u> (acres)	<u>5-year Peak</u> <u>Runoff</u> (cfs)	<u>10-year Peak</u> <u>Runoff</u> (cfs)	<u>100-year Peak</u> <u>Runoff</u> (cfs)		
Basin A – Undeveloped Basin A – Developed Basin B – Undeveloped <mark>Basin B – Developed</mark> Basin C – Developed	5.17 5.17 10.94 10.94 2.71	2.52 14.17 5.17 30.93 6.60	5.04 17.06 10.26 37.55 8.11	15.77 27.15 32.27 59.39 12.90		
DETENTION STORAGE AND WATER QUALITY POND property						

TABLE 1 RUNOFF CALCULATIONS SUMMARY

The increase in storm runoff due to the proposed improvements is relatively large as shown in Table 1 above. The runoff for the initial and major storm events from the tributary basin can be conveyed directly to the major drainage system without adverse impact upstream, surrounding, or downstream properties and facilities. Due to the location of the site relative to the floodplain, we will only be providing water quality for the proposed developed areas. No detention is proposed for this site.

A water quality pond has been designed to provide the recommended structural Best Management Practices (BMPs) outlined in the Urban Drainage and Flood Control District (UDFCD), Urban Storm Drainage Criteria Manual, Volume 3. The calculations for the water quality pond and the limited release structure are enclosed in Appendix C. In addition, sections and details for the pond and limited release outlet structure are shown on the enclosed plan. This pond has been designed to accommodate the anticipated water quality requirements for the developed conditions of both Basins A and B.

A limited release orifice plate provides the required 40-hour drain time for the water quality capture volume. The orifice plate meets the requirements for an Extended Detention Basin and the 40-hour drain time as specified in the UDFCD Manual.

The adjacent taxiway and roadways around the pond will provide approximately 1.0 feet of freeboard above the WQCV water surface elevation. In the event the pond was to overflow, the flow is directed to overtop at the outlet structure and spill north and east across Taxiway Delta and directly to the Coal Creek drainageway.

STORM WATER QUALITY AND EROSION CONTROL

The principal form of storm water quality runoff enhancement is the utilization of an Extended Detention Basin (EDB) as water quality enhancements. Surface drainage from the developed surfaces of the two sites will drain to the natural area at the water quality pond. Drainage from the pond will then be conveyed through the water quality outlet structure, into a proposed 30" CMP culvert, and into the Coal Creek drainage basin. The use of an EDB as a storm water quality runoff enhancement is consistent with the Urban Drainage and Flood Control District, Urban Storm Drainage Criteria Manual, Volume 3, <u>Best Management Practices</u>.

Erosion control measures will consist of hay bales at grass swales and inlets, tracking control measures at the access point to the site, riprap protection at all proposed culverts, and revegetation with appropriate plant species.

FLOOD STATEMENT

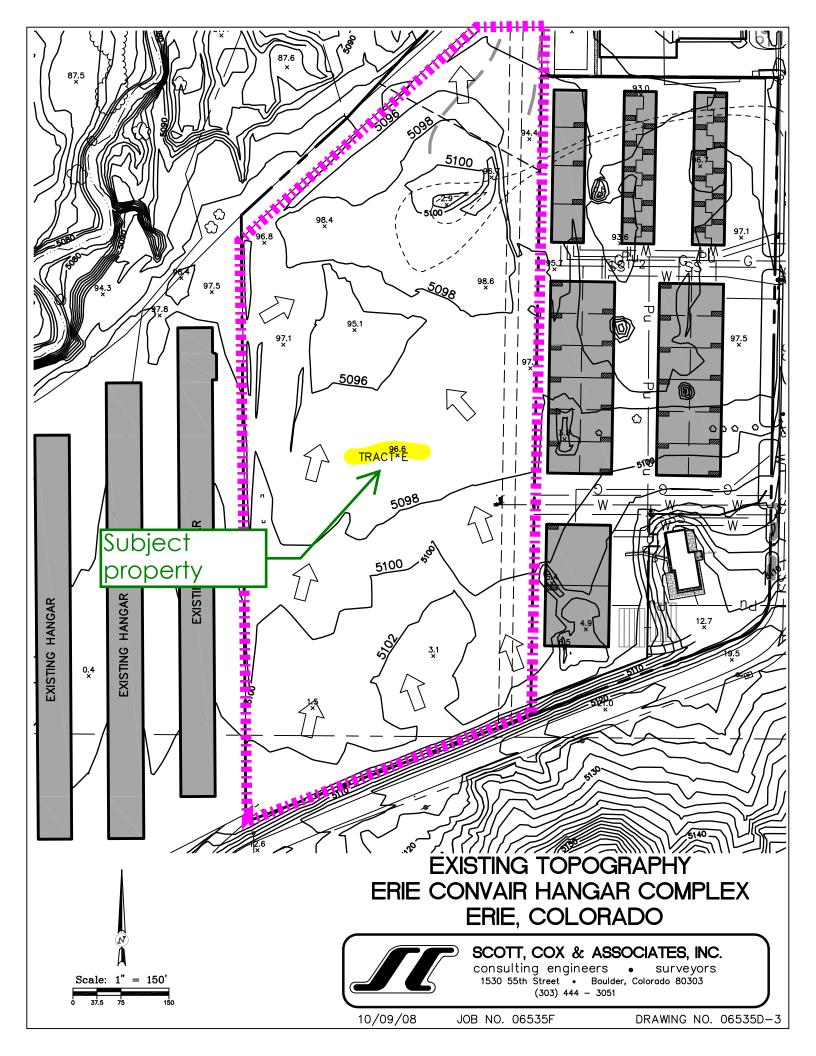
According to the National Flood Insurance Program Flood Insurance Rate Map, FIRM Panel 0801810018E dated December 2, 2004, a portion of the site is located in Zone AE, indicating that it is in an area determined to be inside of the 100-year floodplain. The limits of the floodplain are shown on the Grading, Drainage and Erosion Control Plan that is included in the back pocket of this report. The proposed building improvements have been located and designed to remain outside of the 100-year floodplain.

CONCLUSION

The primary consideration for this project was to design a final drainage plan for the site to mitigate runoff from the proposed development. The drainage plan accommodates runoff from 5-year, 10-year, and 100-year storm events. All analyses were performed in accordance with the <u>Town of Erie Standards and Specifications for Design and Construction of Public Improvements.</u>

APPENDIX A

DRAINAGE BASIN RUNOFF CALCULATIONS



FREQUENCY					
LAND USE OR SURFACE	PERCENT	2	5	10	100
CHARACTERISTICS	IMPERVIOUS				
Business					
Commercial Areas	95	.87	.87	.88	.89
Neighborhood Areas	70	.60	.65	.70	.80
Residential					
Single-Family	*	.40	.45	.50	.60
Multi-Unit (detached)	50	.45	.50	.60	.70
Multi-Unit (attached)	70	.60	.65	.70	.80
1/2 Acre Lot or Larger	*	.30	.35	.40	.60
Apartments	70	.65	.70	.70	.80
Industrial					
Light Areas	80	.71	.72	.76	.82
Heavy Areas	90	.80	.80	.85	.90
Parks, Cemeteries	7	.10	.18	.25	.45
Playgrounds	13	.15	.20	.30	.50
Schools	50	.45	.50	.60	.70
Railroad Yard Areas	20	.20	.25	.35	.45
Undeveloped Areas					
Historic Flow Analysis	2	(See "Lawns")			
Greenbelts, Agricultural					
Offsite Flow Analysis					
(when land use not defined)	45	.43	.47	.55	.65
Streets					
Paved	100	.87	.88	.90	.93
Gravel	40	.40	.45	.50	.60
Drives and Walks	96	.87	.87	.88	.89
Roofs	90	.80	.85	.90	.90
Lawns, Sandy Soil	0	.00	.01	.05	.20
Lawns, Clay Soil	0	.05	.15	.25	.50

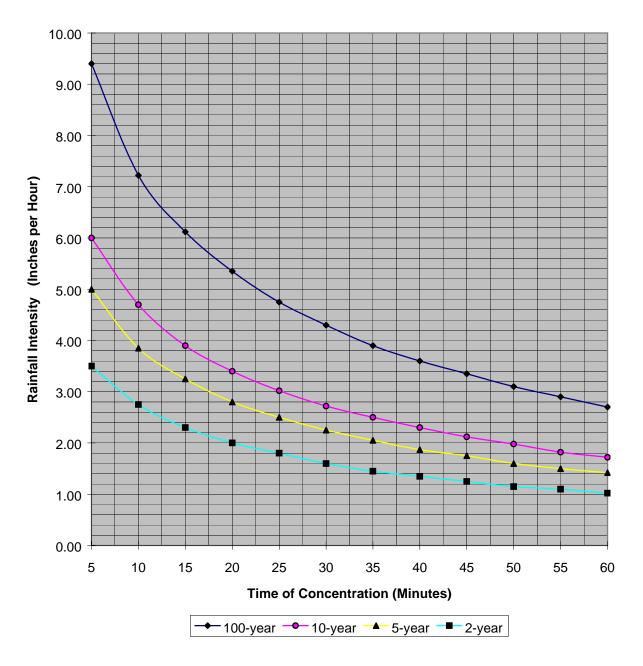
TABLE 800-3RUNOFF COEFFICIENTS (C) FOR RATIONAL METHOD

Note: These Rational Formula coefficients may not be valid for large basins.

* Refer to Urban Storm Drainage Criteria Manual for percent impervious values.

813.06 Rainfall Intensities

The rainfall intensities to be used in the computation of runoff using the Rational Method shall be obtained from the Rainfall Intensity Duration Curves for the Town of Erie, included in these STANDARDS AND SPECIFICATIONS.



Rainfall Intensity Duration Curves

814.00 Detention

814.01 General

On site detention is required for all new development, expansion, and redevelopment. The required minimum detention volume and maximum release rates at these volumes for the 10-year and 100-year storms shall be determined in accordance with the procedure and data set forth in this criteria.

consulting engineers - surveyors

PROJECT NO.: 06535D DATE: 3/19/2009 BY: WMK

STORM RUNOFF HYDROLOGY

Rational Method

Condition: EXISTING Land Use: UNDEVELOPED		Basin Identification: A Design Frequencies: 2, 5, 10 & 100 year				
Basin Area (A)		acres	_ De	Comments:	2, 5, 10 & 100	J year
Dasin Area (A)	<u> </u>	acres		Comments.		
Runoff Coefficie	nts (C) = From Tow	n of Erie Standa	rds for Lawns - Clay	Soil		
	2 year	5 year	10 year	100 year		
	0.05	0.15	0.25	0.50		
	Given					
	Overland flow length	ath (Lo)	210	feet (500 feet max	(imum)	
	Overland flow slop		5.2	%	(intern)	
	Channel travel ler		720.0	feet		
	Channel velocity (• • •	0.8	feet/second		
	Ti minimum fo			Ti =	14.3	min.
	Urban Basin			-		
	Ti = (Lo/180) +	10 min. (initial de	esign pt.)	Ti = _	15.2	min.
		F low: n-Urban Basins T = Lc/V(fps)*60 s	sec./min.	Tt = _	15.0	min.
	Tc, Time of Conc	entration (Tc = ⁻	Γi + Tt) Non-Urban	Tc =	29.3	min.
			Urban	Tc =	15.2	min.
			0	_		

Intensity (I)

From Intensity - Duration - Frequency Curve Town of Erie Standards and Specifications

2 year	5 year	10 year	100 year
2.30	3.25	3.90	6.10

2 year	5 year	10 year	100 year
0.59	2.52	5.04	15.77

SCOTT, COX & A consulting engine	SSOCIATES INC. ers - surveyors	Subjec proper stor	† †y M RUNOFF HYDR Rational Method			O.: 06535D E: 3/19/2009 Y: WMK
	n: EXISTING e: UNDEVELOPED			Basin Identification) vear
Basin Area (A)		es	L	Comments		o year
Runoff Coefficie	nts (C) = From Town of	Erie Standard	is for Lawns - Clay	y Soil		
	2 year	5 year	10 year	100 year	7	
	0.05	0.15	0.25	0.50]	
	Given Overland flow length (Overland flow slope (Channel travel length Channel velocity (V) Ti, Initial time of Cor Urban Basin Ti = 1.8*(1.1-C5)*(Ti minimum for N Greater of Calcula Urban Basin Ti = (Lo/180) + 10	S) (Lc) ncentration: Lo^0.5)/(S^0.33 on-Urban Basir ated Ti and 5 m	ninutes		= <u>38.2</u> = <u>38.2</u>	min. min. min.
	Tt, Travel time of Flo Urban and Non-Ur Travel time, Tt = I Tc, Time of Concent	ban Basins Lc/V(fps)*60 se ration (Tc = Ti		Tt = Tc = Tc =	43.7	min. min. min.
Intensity (I)	From Intensity - Durat		•			

From Intensity - Duration - Frequency Curve Town of Erie Standards and Specifications

2 year	5 year	10 year	100 year
2.20	3.15	3.75	5.90

2 year	5 year	10 year	100 year
1.20	5.17	10.26	32.27

consulting engineers - surveyors

PROJECT NO.: 06535D DATE: 3/19/2009 BY: WMK

STORM RUNOFF HYDROLOGY

Rational Method

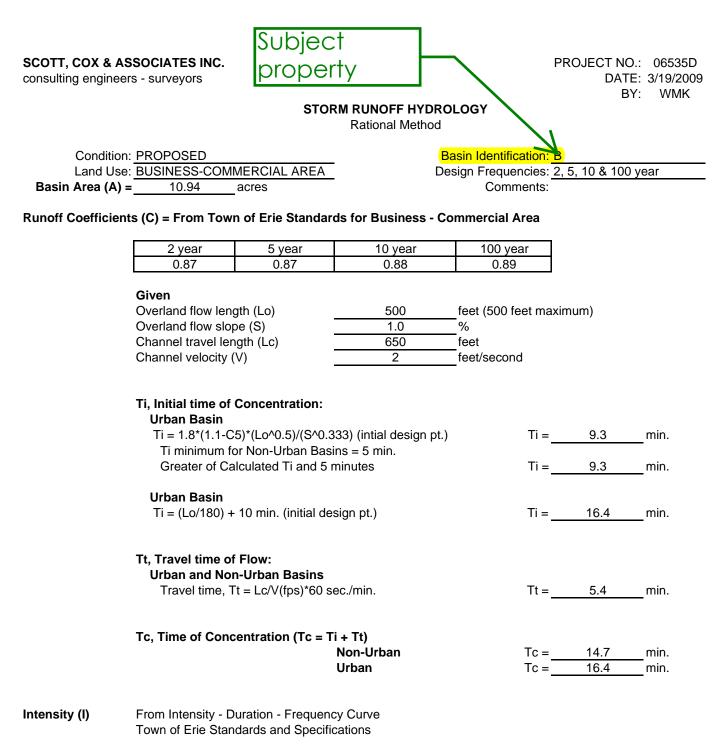
Condition: PROPOSED Land Use: BUSINESS-COMMERCIAL AREA			asin Identification: <u>A</u> esign Frequencies: <u>2,</u>	5, 10 & 100) year	
Basin Area (A	A) = <u>5.17</u> ac	res		Comments:		
unoff Coeffici	ents (C) = From Town o	f Erie Standards	for Business - Co	ommercial Area		
	2 year	5 year	10 year	100 year		
	0.87	0.87	0.88	0.89		
	Given					
	Overland flow length	(Lo)	40	feet (500 feet maxir	num)	
	Overland flow slope		2.0	- %		
	Channel travel length		1025	feet		
	Channel velocity (V)		1.5	feet/second		
	Greater of Calcu Urban Basin Ti = (Lo/180) + 10	ılated Ti and 5 mi) min. (initial desig		Ti = Ti =	5.0 15.9	min. min.
	Tt, Travel time of Fl Urban and Non-U Travel time, Tt =		./min.	Tt =	11.4	min.
	Tc, Time of Concen	•	- Tt) on-Urban	Tc =	16.4	min.

Intensity (I)

From Intensity - Duration - Frequency Curve Town of Erie Standards and Specifications

2 year	5 year	10 year	100 year
2.20	3.15	3.75	5.90

2 year	5 year	10 year	100 year
9.90	14.17	17.06	27.15



2 year	5 year	10 year	100 year
2.30	3.25	3.90	6.10

2 year	5 year	10 year	100 year
21.89	30.93	37.55	59.39

consulting engineers - surveyors

PROJECT NO.: 06535D DATE: 3/19/2009 BY: WMK

STORM RUNOFF HYDROLOGY

Rational Method

	: PROPOSED : BUSINESS-COM = 2.71	MERCIAL AREA acres		asin Identification: sign Frequencies: Comments:) year
Runoff Coefficien	ts (C) = From Tow	n of Erie Standard	s for Business - Co	ommercial Area		
	2 year	5 year	10 year	100 year		
	0.87	0.87	0.88	0.89		
	Given Overland flow len		130	_feet (500 feet ma	ximum)	
	Overland flow slop		2.0	%		
	Channel travel ler Channel velocity (• • • •	<u>640</u> 0.75	_feet feet/second		
	Ti, Initial time of Concentration: Urban Basin Ti = 1.8*(1.1-C5)*(Lo^0.5)/(S^0.333) (intial design pt.) Ti minimum for Non-Urban Basins = 5 min. Greater of Calculated Ti and 5 minutes		Ti =_ Ti =_	-	min. min.	
	Urban Basin Ti = (Lo/180) +	- 10 min. (initial desi	gn pt.)	Ti =	14.3	min.
		f Flow: n -Urban Basins ⁻t = Lc/V(fps)*60 see	c./min.	Tt =	14.2	min.
	Tc, Time of Cond		+ Tt) Ion-Urban Jrban	Tc = Tc =	-	min. min.

Intensity (I)

From Intensity - Duration - Frequency Curve Town of Erie Standards and Specifications

2 year	5 year	10 year	100 year
2.00	2.80	3.40	5.35

2 year	5 year	10 year	100 year
4.72	6.60	8.11	12.90

APPENDIX B

HYDRAULIC CALCULATIONS

Culvert Calculator Report 24" Discharge Pipe into Pond

Solve For: Section Size

Culvert Summary				
Allowable HW Elevation	15.50 ft	Headwater Depth/Height	1.49	
Computed Headwater Eleva	15.18 ft		14.17	cfs
Inlet Control HW Elev.	14.55 ft	5	14.55	
Outlet Control HW Elev.	15.18 ft	Control Type	Outlet Control	
Grades				
Upstream Invert	12.20 ft	Downstream Invert	10.70	ft
Length	75.00 ft	Constructed Slope	0.020000	ft/ft
Hydraulic Profile				
Profile Press	ureProfile	Depth, Downstream	3.85	ft
Slope Type	N/A	Normal Depth	0.89	ft
Flow Regime	N/A	Critical Depth	1.36	ft
Velocity Downstream	4.51 ft	/s Critical Slope	0.005195	ft/ft
Section				
Section Shape	Circular	Mannings Coefficient	0.012	
Sectionrly geteria HDPE (Smoot	h Interior)	Span	2.00	ft
Section Size	24 inch	Rise	2.00	ft
Number Sections	1			
Outlet Control Properties				
Outlet Control HW Elev.	15.18 ft	Upstream Velocity Head	0.32	ft
Ke	0.20	Entrance Loss	0.06	ft
Inlet Control Properties				
Inlet Control HW Elev.	14.55 ft	Flow Control	N/A	
Inlet Type Beveled ring, 33.	.7° bevels	Area Full	3.1	ft²
К	0.00180	HDS 5 Chart	3	
Μ	2.50000	HDS 5 Scale	В	
С	0.02430	Equation Form	1	
Y	0.83000			

Culvert Calculator Report 30" Oulet Pipe

Solve For: Section Size

Culvert Summary					
Allowable HW Elevation	15.00	ft	Headwater Depth/Height	2.46	
Computed Headwater Elev	a 14.03	ft	Discharge	44.10	cfs
Inlet Control HW Elev.	13.35	ft	Tailwater Elevation	0.00	ft
Outlet Control HW Elev.	14.03	ft	Control Type	Outlet Control	
Grades					
Upstream Invert	8.50	ft	Downstream Invert	7.50	ft
Length	100.00	ft	Constructed Slope	0.010000	ft/ft
Hydraulic Profile					
Profile CompositeM2Pre	essureProfile		Depth, Downstream	2.14	ft
Slope Type	Mild		Normal Depth	N/A	ft
Flow Regime	Subcritical		Critical Depth	2.14	ft
Velocity Downstream	11.30	ft/s	Critical Slope	0.017562	ft/ft
Section					
Section Shape	Circular		Mannings Coefficient	0.013	
Sectionril/graterida HDPE (Sm	ooth Interior)		Span	2.25	ft
Section Size	27 inch		Rise	2.25	ft
Number Sections	1				
Outlet Control Properties					
Outlet Control HW Elev.	14.03	ft	Upstream Velocity Head	1.91	ft
Ke	0.20		Entrance Loss	0.38	ft
Inlet Control Properties					
Inlet Control HW Elev.	13.35	ft	Flow Control	N/A	
Inlet Type Beveled ring,	33.7° bevels		Area Full	4.0	ft²
К	0.00180		HDS 5 Chart	3	
Μ	2.50000		HDS 5 Scale	В	
С	0.02430		Equation Form	1	
Y	0.83000				

consulting engineers - surveyors

PROJECT # 06535F DATE 3/19/09 BY WMK

RIPRAP 'A' SIZING

Per Urban Drainage & Flood Control District Volume 1 Major Drainage - Section 7.3

%

Outfall into WQ Pond Pipe Size = 24" PVC Q(5-yr) = 14.17 cfs

(V*(S**0.17))/((Ss-1)**0.66)

5.6 to 6.4

VELOCITY SLOPE Ss	0.02	fps ft/ft (fixed)	2.00
RESULT	2.32	2	
	1.4 to 3.2 3.3 to 3.9 4.0 to 4.5 4.6 to 5.5	TYPE VL L M H	-

VH

USE TYPE 'L' RIPRAP L = 3D = 5.25' (USE 6' LENGTH) W = 21" MIN (USE 3' WIDTH) D = 18" DEPTH

consulting engineers - surveyors

PROJECT # 06535D DATE 3/19/09 BY WMK

RIPRAP 'B' SIZING

Per Urban Drainage & Flood Control District Volume 1 Major Drainage - Section 7.3

1 %

Outfall into Drainageway Pipe Size = 30" PVC Q(5-yr) = 44.10 cfs

(V*(S**0.17))/((Ss-1)**0.66)

VELOCITY SLOPE Ss	9.61 fps (max) 0.01 ft/ft 2.5 (fixed)	
RESULT	3.36	
	TYPF	

	ITPE
1.4 to 3.2	VL
3.3 to 3.9	L
4.0 to 4.5	М
4.6 to 5.5	Н
5.6 to 6.4	VH

USE TYPE 'L' RIPRAP L = 3D = 8.5' (USE 10' LENGTH) W = 30" MIN (USE 5' WIDTH) D = 18" DEPTH

consulting engineers - surveyors

PROJECT # 06535F DATE 3/19/09 BY WMK

RIPRAP 'C' SIZING

Per Urban Drainage & Flood Control District Volume 1 Major Drainage - Section 7.3

Pond Overflow Width = 34' Q(100-yr) = 86.54 cfs

(V*(S**0.17))/((Ss-1)**0.66)

VELOCITY SLOPE Ss		2 fps 02 ft/ft 2.5 (fixed)	2.00 %
	0.1	79	
		TYPE	
	1.4 to 3.2	VL	
	3.3 to 3.9	L	
	4.0 to 4.5	М	
	4.6 to 5.5	Н	
	5.6 to 6.4	VH	

USE TYPE 'L' RIPRAP L = 8' LENGTH W = 34' WIDTH D = 18" DEPTH

Project No.: 06535F Date: 3/19/09

GRATE FLOW CALCULATIONS

RE: Outlet Structure, Type 'D' Inlet Standard Grate

Q=Cd*A*(2gH)**0.5	
-------------------	--

45.53 CFS 0.60 **12.8** Sq. Ft. 0.55 FT 32.20 FT/s² Q= CALCULATED FLOW Cd= ORIFICE COEF. A= OPEN AREA H=HEAD IN FEET g=gravitation force 32.2 ft/sec2

5-yr flow = 44.10 cfs

Therefore grate is sufficient to convey 5-yr event.

W.S.E.	14.55
RIM	14.00
H=HEIGHT FROM BOTTOM OF THE OPENING	0.55

APPENDIX C

WATER QUALITY POND CALCULATIONS

consulting engineers - surveyors

PROJECT #: 06535D DATE: 3/19/09 BY: WMK

Calculate Water Quality Capture Volume

Reference UDFCD Manual - Volume 3

Calculate the required Water Quality Capture Volume using the Imperviousness Ratio from the Town of Erie Standards for Business - Commercial Areas and the total developed conditions for the two lots.

1. Basin Storage Volume		
A. Imperviousness Ratio (I = I _a / 100)	I _A =	95.00%
(From Town of Erie Design Standards	i =	0.950
for Business - Neighborhood Area)		
B. Contributing Watershed	A =	18.81 Acres
C. Water Quality Capture Volume (WQCV) WQCV = 1.0 x (0.91 * i ³ - 1.19 * i ² + 0.78 * i)		
	WQCV =	0.447 in / acre
D. Design Volume		
Volume = (WQCV / 12) * Area * 1.2	Volume =	0.8413 acre - feet 36,645 cubic feet
	WQCV =	36,645 cubic feet

consulting engineers - surveyors

PROPOSED W.S.E.:

114.00

POND VOLUME CALCULATION

		AREA	AREA	WEIGHTED AVG AREA	INCREMENTAL VOLUME	CUMMULATIVE VOLUME
ELEVATION 108.5	DEPTH	S.I.	S.F. 0	S.F.	C.F.	C.F.
	0.5			1,956	978	978
109.0			3,912			/ .
110.0	1.0		5,160	4,536	4,536	5,514
110.0	1.0		5,100	5,865	5,865	11,379
111.0			6,570	-,	-,	,
	1.0			7,358	7,358	18,737
112.0			8,145			
112.0	1.0		0.000	9,013	9,013	27,749
113.0	1.0		9,880	10,828	10,828	38,577
114.0	1.0		11,775	10,020	10,020	00,011
	5.5	Т	OTAL (CUBIC FEE	ET)	38,577	

ОΚ

Volume Provided=38,577 cubic feet > Volume Required = 36,645 cubic feet

	STAGE/STORAGE	
STAGE(SF)	VOL(CF)±	CUM VOL(CF)
108.5	0	0
109.0	1,956	978
110.0	4,536	5,514
111.0	5,865	11,379
112.0	7,358	18,737
113.0	9,013	27,749
113.8		36,645
114.0	10,828	38,577

PROJECT #:

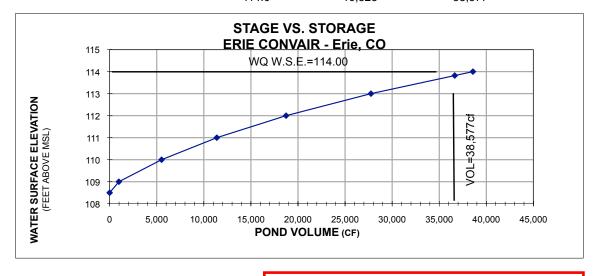
DATE:

BY:

06535D

3/19/09

WMK



20' different in datum. 5114 = 5094' NAVD 88

06535D Pona voi-Ena Area uz-zu-us.xis

Design Procedure Form: Extended Detention Basin (EDB) - Sedimentation Facility

Designer:	WMK		Sheet 1 0
Company:	Scott, Cox & Associates, Inc., 1530 55th Street, Boulder, CO 80303	3	
Date:	October 6, 2008		
Project:	Erie Convair		
Location:	Lot 2 - Replat A - Erie Air Park, 2865 Airport Drive, Erie, CO		
1. Basin Stor	age Volume		
A) Tributar	ry Area's Imperviousness Ratio (i = I _a / 100)	$l_a = 95.00 \%$ i = 0.95	
B) Contrib	outing Watershed Area (Area)	Area = <u>18.82</u> acres	
	Quality Capture Volume (WQCV)	WQCV = 0.45 watershed inches	
	V =1.0 * (0.91 * I ³ - 1.19 * I ² + 0.78 * I)) a Volume: Vol = (WQCV / 12) * Area * 1.2	Vol = 0.842 acre-feet	
2. Outlet Wo	rks		
A) Outlet Type (Check One)		X Orifice Plate Perforated Riser Pipe	
		Other:	
B) Depth	at Outlet Above Lowest Perforation (H)	H = <u>5.30</u> feet	
C) Requir	ed Maximum Outlet Area per Row, (A_0)	$A_o = $ 0.49 square inches	
	ation Dimensions (enter one only) :		
,	cular Perforation Diameter OR leight Rectangular Perforation Width	D = <u>0.770</u> inches, OR W = inches	
E) Numbe	er of Columns (nc, See Table 6a-1 For Maximum)	nc = <u>1</u> number	
F) Actual	Design Outlet Area per Row (A _o)	$A_o = $ 0.47 square inches	
G) Numbe	er of Rows (nr)	nr = <u>16</u> number	
H) Total C	Dutlet Area (A _{ot})	A _{ot} = 7.40 square inches	
3. Trash Rac	k		
A) Neede	d Open Area: $A_t = 0.5 *$ (Figure 7 Value) * A_{ot}	$A_t = 259$ square inches	
В) Туре о	f Outlet Opening (Check One)	X ≤ 2" Diameter <u>Round</u> 2" High <u>Rectangular</u>	
C) For 2",	or Smaller, Round Opening (Ref.: Figure 6a):	Other:	
	h of Trash Rack and Concrete Opening (W _{conc}) n Table 6a-1	W _{conc} = <u>6</u> inches	
ii) Heig	ht of Trash Rack Screen (Η _{τR})	H _{TR} = 66 inches	

Sheet 1 of 3

Design Procedure Form: Extended Detention Basin (EDB) - Sedimentation Facility

Designer:	WMK	Sneet 2 0
Company:	Scott, Cox & Associates, Inc., 1530 55th Street, Boulder, CO 80303	
Date:	October 6, 2008	
Project:	Erie Convair	
Location:	Lot 2 - Replat A - Erie Air Park, 2865 Airport Drive, Erie, CO	
ііі) Туре	e of Screen (Based on Depth H), Describe if "Other"	X S.S. #93 VEE Wire (US Filter) Other:
iv) Scre	en Opening Slot Dimension, Describe if "Other"	X 0.139" (US Filter) Other:
	cing of Support Rod (O.C.) be and Size of Support Rod (Ref.: Table 6a-2)	0.75 inches #156 VEE
vi) Typ	be and Size of Holding Frame (Ref.: Table 6a-2)	<u>3/8 in. x 1.0 in. flat bar</u>
D) For 2"	High Rectangular Opening (Refer to Figure 6b):	
I) Widt	th of Rectangular Opening (W)	W = inches
ii) Widt	h of Perforated Plate Opening (W _{conc} = W + 12")	W _{conc} = inches
iii) Widtl	h of Trashrack Opening (W _{opening}) from Table 6b-1	W _{opening} = inches
iv) Heig	ght of Trash Rack Screen (H_{TR})	H _{TR} = inches
v) Туре	e of Screen (based on depth H) (Describe if "Other")	Klemp [™] KPP Series Aluminum Other:
	oss-bar Spacing (Based on Table 6b-1, Klemp [™] KPP ating). Describe if "Other"	inches Other:
vii) Min	nimum Bearing Bar Size (Klemp [™] Series, Table 6b-2) (Based on depth of WQCV surcharge)	
4. Detention	Basin length to width ratio	(L/W)
5 Pre-sedim	nentation Forebay Basin - Enter design values	
A) Volum	e (no less than 5% of Design Volume from 1D)	acre-feet
B) Surfac	e Area	acres
	ector Pipe Diameter to drain this volume in 5-minutes under inlet control)	inches
D) Paved	/Hard Bottom and Sides	yes/no

Sheet 2 of 3

Design Procedure Form: Extended Detention Basin (EDB) - Sedimentation Facility

			Sheet 3 of 3
Designer:	<u>ММК</u>		
Company:	Scott, Cox & Associates, Inc., 1530 55th Street, Boulder, CO 80303		
Date:	October 6, 2008		
Project:	Erie Convair		
Location:	Lot 2 - Replat A - Erie Air Park, 2865 Airport Drive, Erie, CO		
6. Two-Stage	Design - See Figure EDB-1		
		5	
A) Top Sta	age (Depth $D_{WQ} = 2'$ Minimum)	D _{WQ} =feet Storage= acre-feet	
,	Stage Depth (D _{BS} = 1.0' Minimum, 2.0' Maximum)	D _{BS} =feet	
Bottom	n Stage Storage (no less than 3% of Design Volume (0.025250958675 acre-feet.)	Storage= acre-feet Surf. Area= acres	
		u	
	bool (Minimum Depth = the Larger of	Depth=feet	
0.5 1	op Stage Depth or 2.5 Feet)	Storage= acre-feet Surf. Area= acres	
	/olume: Vol _{tot} = Storage from 5A + 6A + 6B be > Design Volume in 1D, or 0.8416986225 acre-feet.)	Vol _{tot} =acre-feet	
(Musi			
7 Basin Sido	Slopes (Z, horizontal distance per unit vertical)	Z = 4.00 (horizontal/ve	rtical)
	= 4, Flatter Preferred		nical)
8. Dam Emba	nkment Side Slopes (Z, horizontal distance)	Z = 4.00 (horizontal/ve	rtical)
	tical) Minimum Z = 3, Flatter Preferred		,
9. Vegetation	(Check the method or describe "Other")	X Native Grass	
		Irrigated Turf Grass Other:	
		Outer.	
Nataa			
Notes:			

consulting engineers - surveyors

POND

Rectangular Weir Flow Calculations "Emergency Overflow Capacity"

Enter starting C, L, H to calculate Q.

Q=C*L*(H**1.5)	Q=Flow= C=Weir Coef.= L=Weir Length= H=Height= Inv. of Overflow Weir=Pond W.S.E.=	88.40 CFS 2.6 34 FT 1.000 FT 5115.00	(<u>12.00</u> IN.)
	Top of Wall=	5116.00	

Qallow = 88.40 CFS >> Q100-yr,A,B = 86.54 CFS(Design Flow), ∴ O.K.

Date: 3/19/2009



Weir Calcs Rectang .XLS

SITE IMPROVEMENT PLAN (INCLUDES AMENDMENT NO. 2) ERIE CONVAIR LLC

LOT 2 AND OUTLOT A. ERIE AIR PARK SUBDIVISION, REPLAT A. AND A PART OF TRACT D. ERIE AIR PARK SUBDIVISION. ALL LOCATED IN THE SW1/4 OF SEC. 31, T1N, R68W OF THE 6TH P.M. TOWN OF ERIE, COUNTY OF WELD, STATE OF COLORADO

EASEMENTS

THERE IS AN AVIATION EASEMENT ABOVE THE SURFACE OF SUBJECT PROPERTY RECORDED MAY 11, 1978, IN BOOK 831 AT RECEPTION NO. 1753139.

THERE IS A SOLAR EASEMENT APPURTENANT TO EACH LOT AND TRACT IN ERIE AIR PARK SUBDIVISION RECORDED MAY 11, 1978, AS DEFINED IN BOOK 831 AT RECEPTION NO, 1753143. PLAN DOES COMPLY WITH SOLAR EASEMENT.

THERE IS A MINERAL / COLL EASEWEIT OWNED BY NORTH AMERICAN RESOURCES CO. COVERING THE ENTRE PROPERTY AS RECORDED IN THE WELD COUNTY DEED IN BK. 158, PG. 604 AND DESCRIED AS: PARCEL 1; LOT 2 AND OUTLOT A OF ERIE AIR PARK SUBDIVISION REPLAT A. PARCEL 2; THAT PART OF TRACT D, ERIE AIR PARK SUBDIVISION REPLAT A. DARCEL 1; LOT 2 AND OUTLOT A OF ERIE AIR PARK SUBDIVISION REPLAT A. NORTH, RANGE 68 WEST THAT OF THE SOUTHWEST 1/4 OF SECTION 31, TOWNSHIP 1 NORTH, RANGE 68 WEST OF THE SOUTHWEST 1/4 OF SECTION 31, TOWNSHIP 1 NORTH, RANGE 68 WEST OF THE SOUTHWEST 1/4 OF SECTION 31, TOWNSHIP 1 ACREEVENT FOR COUNTY OF WELD, STATE OF COLORADO AS RECORDED IN AN ACREEVENT FOR COMPATIBLE DEVELOPMENT, RECEIPT NO. 265309, WELD COUNTY, DATED 11–16–1998.

THERE IS A 50' TAXIWAY EASEMENT ALONG THE WEST PROPERTY LINE, CONSISTING OF A 30' EASEMENT AND 20' SETBACK. RECP # 3442230.

THERE IS A WATER EASEMENT CONSISTING OF A NORTH BOUNDARY SETBACK LINE SETBACK FROM FURTHEST EXISTING WATERLINE SOUTH IN ARPORT RD. LINE SETBACK FROM FURTHEST EXISTING WATERLINE SOUTH IN ARPORT RD. RECP # 3442230.

THERE IS AN EXISTING 40-FOOT UTILITY EASEMENT CENTERED ON AIRPORT DRIVE BOOK 1598 RECP #1366570

ANY OFF-SITE AND ON-SITE EASEMENTS FOR UTILITIES, ACCESS, TAXIWAYS AND LANDSCAPING NEED TO BE IN PLACE PRIOR TO CONSTRUCTION. SUCH EASEMENTS SHALL BE DEDICATED BY SEPARATE INSTRUMENT WHERE APPLICABLE.

THERE IS A 30' EASEMENT FOR WATER UTILITIES AT 951.85' DUE SOUTH OF THE NW 1/16 COR. SEC. 31 TIN R68W OF THE 6TH PM. WELD COUNTY, COLORADO FOR A DISTANCE WEST OF 370.02'. WELD COUNTY 3411156 DATED 8-11-06.

THERE IS A DRAINAGE EASEMENT FOR THE PROPOSED WATER QUALITY POND CURRENTLY BEING RECORDED.

THERE IS A POND EASEMENT FOR THE PROPOSED WATER QUALITY POND CURRENTLY BEING RECORDED.

THERE IS A UTILITY EASEMENT FOR THE FIRE HYDRANT CURRENTLY BEING

SITE IMPROVEMENT PLAN CERTIFICATE OF APPROVAL

SITE PLAN APPROVAL CERTIFICATE - PLANNING COMMISSION

THIS SITE PLAN HAS BEEN REVIEWED AND FOUND TO BE COMPLETED AND IN ACCORDANCE WITH APPLICABLE TOWN OF ERIE REGULATIONS.

DATE

PLANNING COMMISSION-CHAIR DATE

DIRECTOR OF COMMUNITY DEVELOPMENT

THE UNDERSIGNED AS THE OWNER OR OWNER'S REPRESENTATIVE OF THE LANDS DESCRIBED HEREIN, HEREBY ACREES ON BEHALF OF HIMSELF/HERSEF, THEIR HEIRS, SUCCESSORS, AND ASSIGNS TO DEVELOP AND MAINTAIN THE PROPERTY DESCRIBED HEREON IN ACCORDANCE WITH THIS APPROVED SITE PLAN AND IN COMPLIANCE WITH THE TOWN OF ERE UNIFIED DEVELOPMENT CODE AND MUNICIPAL CODE:

(SEAL)

ACKNOWLEDGED BEFORE ME THIS ____ DAY OF _____ __, 200__ BY ____ ____ AS ___ WITNESS MY HAND AND OFFICIAL SEAL

NOTARY PUBLIC

MY COMMISSION EXPIRES: _____

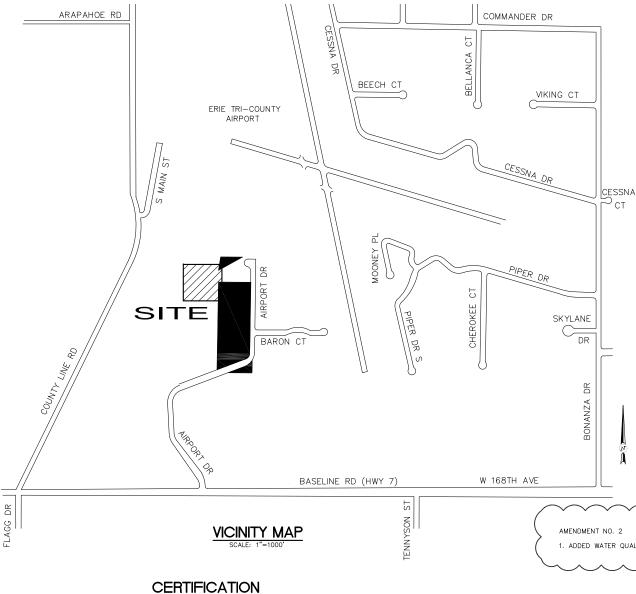
LEGAL DESCRIPTION

OUTLOT A AND LOT 2, ERIE AIR PARK SUBDIVISION REPLAT A, AS PER PLAT RECORDED SEPTEMBER 4, 1992 IN BOOK 1350 AT RECEPTION NO. 2302520, COUNTY OF WELD, STATE OF COLORADO.

AND

THAT PART OF TRACT D, ERIE AIR PARK SUBDIVISION, WHICH IS LOCATED IN THE NORTH 1/2 OF THE SOUTHWEST 1/4 OF SECTION 31, TOWNSHIP 1 NORTH, RANGE 68 WEST OF THE 6TH PRINCIPAL MERIDIAN, LYING SOUTH AND EAST OF AIRPORT DRIVE, COUNTY OF WELD, STATE OF COLORADO TOGETHER WITH ALL ITS APPURTENANCES.

A.K.A. 3000 AIRPORT DRIVE



I A. JOHN BURI, A PROFESSIONAL LAND SURVEYOR REGISTERED IN THE STATE OF COLORADO, HEREBY CERTIFY TO ERIE CONVAIR, LLC., THAT A BOUNDARY SURVEY AND A TOPOGRAPHIC SURVEY OF THE PROPERTY DESCRIBED HEREON WAS CONDUCTED UNDER MY SUPERVISION ON DECEMBER 13, 2006.

AND FURTHER CERTIFY THAT THE PROPERTY DESCRIBED HEREON IS NOT IN A 100-YEAR FLOOD PLAIN PER FEMA FLOOD INSURANCE RATE MAP COMMUNITY PANEL NO. 080180018 E, DATED SEPTEMBER 2, 2004.

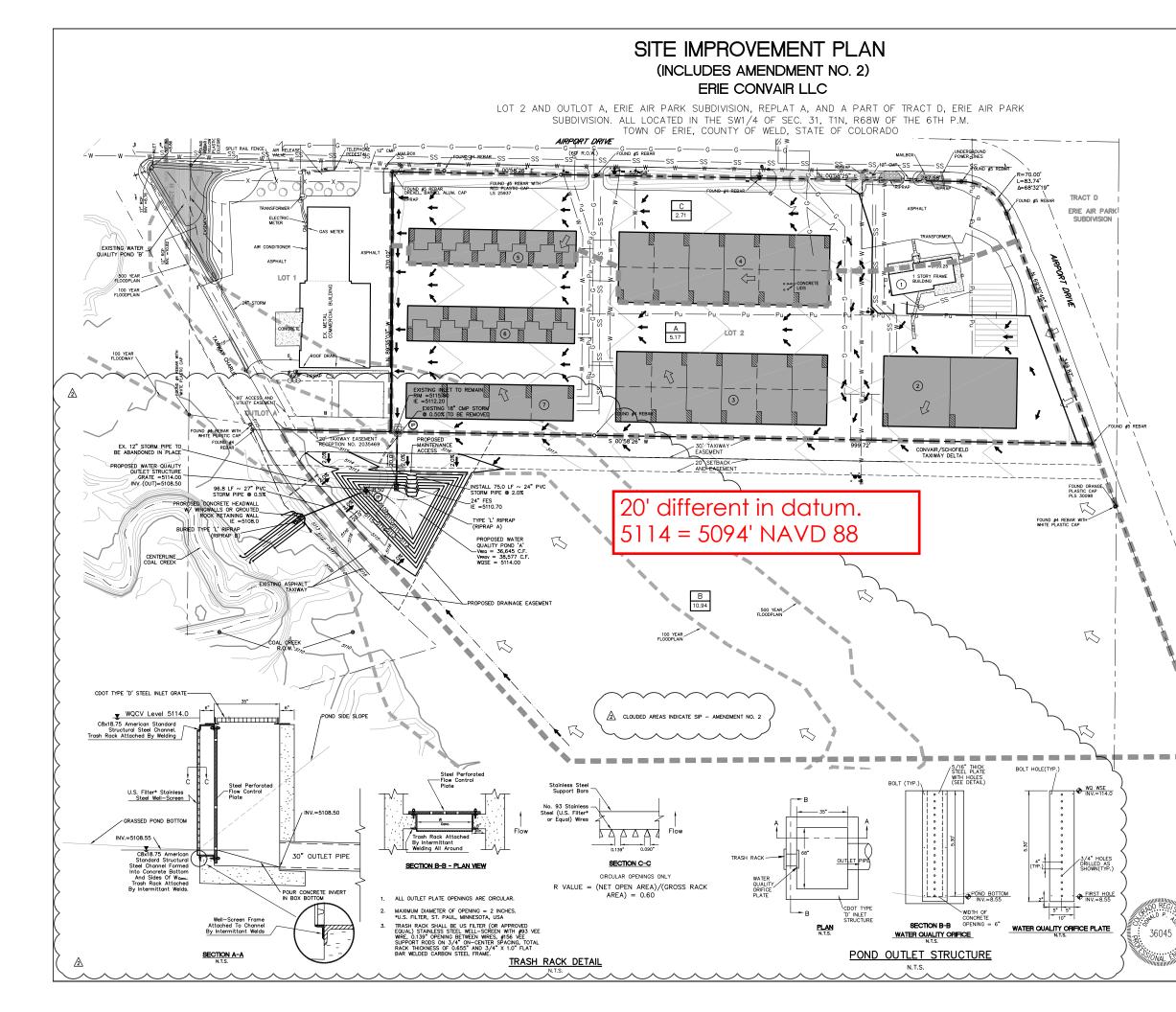
FOR SCOTT, COX, & ASSOCIATES, INC.

COLORADO PLIS No. 24302

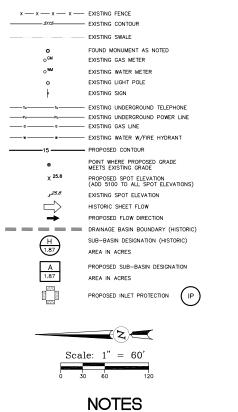
NOTICE: According to Colorado law, you must commence any legal action based upon any defect in this survey within 3 years after you first discover such defect. In no event, may any action based upon any defect in this survey be commenced more than ten year from the date of this survey certification shown hereon.

SHT NO DESCR	RIPTION
C1.0 COVER SHEET	
C1.1 GRADING AND DRAINAG	E PLAN
C2.1 CIVIL DETAILS	









ORIGIN BENCH MARK: NGS DESIGNATION-ERIE AIR PARK, PIO- AI5917. ALUMINUM DISK. SET INTO THE TOP G A ROUND CONCRETE POST FLUSH WITH THE GROUND. 122.4 FEE SW FROM CENTER OF RUWWAY 15-33, TOB.9 FEET WEST FROM THE WESTERN MOST OND OF FOUR RED-ELUE LIGHTS AT THE END OF RUWWAY 33, 931 FEET SE FROM THE TOP CENTER OF SIGN A/33, 197 FEET SE FROM THE SOUTH EDDE TAXIMAY TA STOP BAR.

CENTER OF SIGN A/SS, 19.7 FEET SE FROM THE SOUTH EDUE TAXIWAT AT STOP BAR AT. ELEVATION =5117.70 (NAVO 88). PROJECT BENCH MARK: FOUND YELLOW FIN&CAP MARKING THE NORTHWEST CORNER C LOT 3, BLOCK 6, ERIE JAR PARK SUBDIVISION. LOCATED ON EAST ROW AIRPORT DRIVE ELEVATION =5116.77 (NAVO 88).

- 2. THE LOCATION OF THE ABOVE GROUND UTILITIES SHOWN HEREON ARE BASED ON THE FIELD SURVEY BY SCOTT, COX & ASSOCIATES, INC. THE LOCATIONS OF THE UNDERGROUND UTILITIES SHOWN HEREON ARE BASED ON SAID SURVEY AND INFORMATION PROVIDED BY OTHERS (WHICH MAY INCLUDE THE UTILITY OWNER OR UTILITY LOCATING SERVICES). SCOTT, COX & ASSOCIATES, INC. IS NOT RESPONSIBLE FOR UTILITY. INFORMATION PROVIDED BY OTHERS. SCOTT, COX & ASSOCIATES, INC. RECOMMENDS THAT THE LOCATION OF THE UTILITIES EF FIELD VERIFIED PRIOR TO ANY DIGGING ON, OR ADJACENT TO THE SUBJECT PROPERTY.
- 3. THIS DRAWING IS BASED ON A FIELD SURVEY COMPLETED ON 01/15/08.
- 4. THE WATER QUALITY POND HAS BEEN DESIGNED TO ACCEPT DEVELOPED RUNOFF FROM BOTH THE 7.88 ACRE BASIN ON LOT 2 AND THE 10.94 ACRE BASIN ON A PORTION OF LOT E.
- 5. ACCORDING TO THE NATIONAL FLOOD INSURANCE PROGRAM FLOOD INSURANCE RATE MAP, FRM PANEL 0801810018E DATED DECEMBER 2, 2004, A PORTION OF THE SITE I LOCATED IN ZONE AE, INDICATING THAT IT IS IN AN AREA DETERMINED TO BE INSIDE OF THE 100-YEAR FLOODFLAIN.
- 6. THE CONTOURS SHOWN WITHIN THE COAL CREEK DRAINAGE WAY ARE PER THE AERIAL CONTOURS PROVIDED BY THE TOWN OF ERIE AND WERE NOT SURVEYED AS A PART OF THIS PROJECT.

BASIN SUMMARY

BASIN	Q2 (CFS)	Q5 (CFS)	Q10 (CFS)	OUTFALL
А	5.17	14.17	27.15	PROPOSED
В	10.97	30.93	59.39	POND 'A'
С	2.71	6.60	12.90	EX. POND 'B'

GRADING, DRAINAGE, AND **EROSION CONTROL PLAN** SITE IMPROVEMENT PLAN ERIE CONVAIR HANGAR COMPLEX 3000 AIRPORT DRIVE ERIE, COLORADO

SCOTT, COX & ASSOCIATES, INC. consulting engineers • Surveyors 1530 55th Street • Boulder, Colorado 80303 (303) 444 - 3051							
Designed byWMK	Date	Scale	Drawing no.		Sheet		
Name and WMK	10/09/08	1"=60'	0653	5D-3	C1.1		
Drawn by	Revision	Descr	iption	Date	Project no.		
Checked by DPA	1	TOWN CO	MMENTS	04/02/09	06535D		
CHECKED By	2	TOWN COMMENTS		04/22/09	000000		

GENERAL NOTES - CONSTRUCTION

ALL CONSTRUCTION SHALL CONFORM TO THE LATEST "STANDARDS AND SPECIFICATIONS FOR DESIGN AND CONSTRUCTION OF PUBLIC INPROVEMENTS" BY THE TOWN OF ERIE. COPIES OF THE TOWN OF ERIE STANDARDS AND SPECIFICATIONS MAY BE OBTAINED FROM THE TOWN OF ERIE. THE OWNER SHALL SCHEDULE A PRE-CONSTRUCTION MEETING WITH THE TOWN OF ERIE ENGINEERING STAFF AT LEAST 48 HOURS PRIOR TO THE START O CONSTRUCTION. THOSE IN ATTENDANCE SHALL INCLUDE THE OWNER, HIS ENGINEER. THE TOWN OF ERIE ENGINEERING STAFF, REPRESENTATIVES OF TH CONTRACTORS AND OTHER AFFECTED AGENCIES. PLANS WITH THE TOWN OF ERIE REVIEW STAMP WILL BE DISTRIBUTED AT THE PRE-CONSTRUCTION MEETING.

. EXCEPT WHERE OTHERWISE PROVIDED FOR IN THESE PLANS AND SPECIFICATIONS, THE COLORADO DEPARTMENT OF TRANSPORTATION STANDARD SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION, AND THE COLORADO DEPARTMENT OF TRANSPORTATION M & S STANDARDS, LATEST EDITION, SHALL APPLY.

PRIOR TO BEGINNING THE WORK, THE CONTRACTOR SHALL OBTAIN ANY/ALL WRITTEN AGREEMENTS FOR INGRESS AND EGRESS TO THE WORK SITE FROM ADJACENT PRIVATE PROPERTY OWNERS. ACCESS TO ANY ADJACENT PRIVATE PROPERTY SHALL BE MAINTAINED THROUGHOUT THE CONSTRUCTION PERIOD.

ALL MATERIALS AND WORKMANSHIP SHALL BE SUBJECT TO INSPECTION BY THE TOWN OF ERIE ENGINEERING STAFF. THE TOWN RESERVES THE RIGHT TO ACCEPT OR REJECT ANY SUCH MATERIALS AND WORKMANSHIP THAT DOES NOT CONFORM TO TOWN STANDARDS AND SPECIFICATIONS. APPLICATION FOR INSPECTION BY THE TOWN OF ERIE SHALL BE MADE BY THE CONTRACTOR AT LEAST TWENTY-FOUR (24) HOURS BEFORE THE SERVICE THEREOF WILL BE REQUIRED. IF A TOWN OF ERIE SHALL BE MADE BY THE CONTRACTOR AT LEAST TWENTY-FOUR (24) HOURS BEFORE THE SERVICE THEREOF WILL BE REQUIRED. IF A TOWN OF ERIE SHALL BY ADSECTOR IS NOT AVAILABLE AFTER PROPER NOTICE OF CONSTRUCTION ACTIVITY HAS BEEN PROVIDED, THE PERMITTEE MAY COMMENCE WORK IN THE INSPECTOR'S ABSENCE. HOWEVER, THE TOWN OF ERIE RESERVES THE RIGHT TO REJECT THE IMPROVEMENT IF SUBSEQUENT TESTING REVEALS AN IMPROPEN INSTALLATION.

UNDERGROUND UTUITIES IN THE AREA OF CONSTRUCTION ARE APPROXIMATE ONLY. THEY HAVE BEEN LOCATED FROM FIELD INVESTIGATION AND THE BEST AVAILABLE UTUITY RECORDS. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE LOCATION, PROTECTION AND REPAR OF ALL UTUITES ENCOUNTERED DURING CONSTRUCTION WHETHER SHOWN ON THESE PLANS OR NOT. THE CONTRACTOR SHALL CONTACT ALL RESPECTIVE UTUITES AND HAVE ALL UTUITES FIELD-LOCATED PRIOR TO CONSTRUCTION, IT SHALL BE THE CONTRACTOR'S RESPONSIBILITY TO VERIFY THE LOCATION OF ALL EXISTING STRUCTURES AND UTUITES SHOWN ON THE DAMMOS, TO ASCERTAIN WHETHER ANY STRUCTURES AND UTUITES MAY EMST, AND TO REPAR FOR REPLACE ANY STRUCTURES AND UTUITES AND HAVE ALL UNTURED BE DAMAGED. IN SACH AND HAVE ALL UNTURES AND FOR ADDITION OF ALL EXISTING STRUCTURES AND UTUITES SHOWN ON THE DAMAGED. THE AND STRUCTURES AND UTUITES MAY EMST, AND TO REPAR FOR REPLACE ANY STRUCTURES AND UTUITES AND HAVE ALL DENDRIFY AND DESIGN CIVIL ENGINEER PRIOR TO PROCEEDING.

THE CONTRACTOR SHALL COORDINATE HIS ACTIVITIES WITH THE AFFECTED UTILITY COMPANIES AND SHALL NOTIFY THE UTILITY NOTIFICATION CENTER, PHONE NUMBER 1-800-922-1987, FORTY-EIGHT (96) HOURS PRIOR TO THE START OF CONSTRUCTION.

CONTRACTOR SHALL HAVE IN HIS POSSESSION AT ALL TIMES ONE (1) SIGNED AND STAMPED BY THE DESIGN ENGINEER, COPY OF PLANS ACCEPTED BY THE TOWN OF ERIE. THE TOWN OF ERIE, THROUGH ACCEPTANCE OF THIS DOCUMENT, ASSUMES NO RESPONSIBILITY FOR THE COMPLETENESS AND/OR ACCURACY OF THIS DOCUMENT. THE OWNER AND ENGINEER UNDERSTAND THAT THE RESPONSIBILITY FOR THE ENGINEERING ADEQUACY OF THE FACULTES DEPICTED IN THIS DOCUMENT LIES SOLELY WITH THE REGISTERED PROFESSIONAL ENGINEER WHOSE STAMP AND SIGNATURE ARE AFFIXED TO THIS DOCUMENT. REPORT ALL DISCREPANCIES TO THE DESIGN ENGINEER IMMEDIATELY.

CONTRACTOR SHALL OBTAIN, AT HIS OWN EXPENSE, ALL APPLICABLE SPECIFICATIONS AND PERMITS NECESSARY TO PERFORM THE PROPOSED WORK.

. AS-BUILT DRAWINGS AND AN AUTOCAD CD, AS REQUIRED IN THE SPECIFICATIONS, ARE TO BE SUBMITTED BY THE CONTRACTOR PRIOR TO SUBSTANTIAL COMPLETION/CONSTRUCTION ACCEPTANCE OF THE CONSTRUCTION.

THE CONTRACTOR SHALL BE RESPONSIBLE FOR REMOVING AND REPLACING ANY EXISTING SIGNS, STRUCTURES, FENCES, ETC., ENCOUNTERED ON THE JOB AND RESTORING THEM TO THEIR ORIGINAL CONDITION. . THE CONTRACTOR IS RESPONSIBLE FOR:

A. NOTIFYING THE TOWN OF ERIE UTILITY CUSTOWERS OF POTENTIAL SERVICE OUTAGES, AND COORDINATE WITH THE TOWN OF ERIE FOR DETERMINATION OF MINIMUM TIME REQUIREMENT.

B. NOTIFYING THE TOWN OF ERIE TWENTY-FOUR (24) HOURS IN ADVANCE FOR OBSERVATIONS OF WORK IN PROGRESS. OBSERVATION AND ON-SITE VISITS ARE NOT TO BE CONSTRUED AS A GUARANTEE BY THE TOWN ENGINEERING STAFF OF THE CONTRACTORS' CONTRACTUAL COMMITMENT. IF WORK IS SUSPENDED FOR ANY PERIOD OF TIME AFTER INITIAL START-UP, THE CONTRACTOR SHALL NOTIFY THE TOWN OF ERIE FORTY-EIGHT (48) HOURS PRIOR TO RESTART.

C. IN THE EVENT OF AN AFTER HOURS EMERGENCY, CALL 303-441-4444.

D. NOTIFYING THE MOUNTAIN VIEW FIRE PROTECTION DISTRICT OF ALL STREET CLOSURES AND EXISTING FIRE HYDRANTS TAKEN OUT OF SERVICE FOR AT LEAST FORTY-EIGHT (48) HOURS PRIOR TO THE START OF CONSTRUCTION.

PRIOR TO INSTALLATION OF UTILITY MAINS, ROAD CONSTRUCTION MUST HAVE PROGRESSED TO AT LEAST THE "SUB-GRADE" STAGE. THE CONTRACTOR WILL ADJUST ALL VALVE BOXES AND FIRE HYDRANTS TO THE FINAL FINISHED GRADE.

THE CONTRACTOR SHALL BE RESPONSIBLE FOR REMOVING ANY GROUNDWATER ENCOUNTERED DURING THE CONSTRUCTION OF ANY PORTION OF THIS . THE CONTRACTOR SHALL BE RESPONSIBLE FOR REMOVING ANY GROUNDWATER ENCOUNTERED DURING THE CONSTRUCTION OF ANY PORTION OF THIS PROJECT. A CONSTRUCTION DEWATERING PERMIT MUST BE OBTAINLE FROM THE COLORADO DEPARTMENT OF PUBLIC HEALTH AND ENVROMENT (COPHE). GROUNDWATER SHALL BE PUMPED, PIPED, REMOVED AND DISPOSED OF IN A MANNER WHICH DOES NOT CAUSE FLOODING OF NEITHER EXISTING STREET NOR ERSION OF ADUTING PROPERTIES IN ORDER TO CONSTRUCTION UNT ANY SEVENT TO DISPOSE OF TRENCH WATER WILL NOT BE PERMITAD. STREET NOR THE DISPOSE OF FRENCH WATER WILL NOT BE PERMITAD. STREET NOR THE PLACED WHERE GROUNDWATER IS VISIBLE OR UNTIL THE GROUNDWATER SHALL BE FLACED WHERE GROUNDWATER, STABLE ON UNTIL THE GROUNDWATER, ENCOUNTERED DURING THE CONSTRUCTION OF THE PROPOSED IMPROVEMENTS. ANY UNSTABLE AREAS, AS A RESULT OF GROUNDWATER, ENCOUNTERED DURING THE CONSTRUCTION OF THE PROPOSED IMPROVEMENTS. ANY UNISTABLE AREAS, AS A RESULT OF GROUNDWATER, ENCOUNTERED DURING THE CONSTRUCTION OF THE PROPOSED IMPROVEMENTS. ANY UNISTABLE AREAS, AS A RESULT OF GROUNDWATER, ENCOUNTERED DURING THE CONSTRUCTION OF THE PROPOSED IMPROVEMENTS. ANY UNISTABLE AREAS, AS A RESULT OF GROUNDWATER, BOUND THEED DURING THE CONSTRUCTION OF THE PROPOSED IMPROVEMENTS. ANY UNISTABLE AREAS, AS A RESULT OF GROUNDWATER, ENCOUNTERED DURING THE CONSTRUCTION OF THE COURTRACTOR, THE TOWN OF ERIE, AND THE DESIGN AT ALL TIMES WITHIN THE CONSTRUCTION AREAS.

. IT SHALL BE THE RESPONSIBILITY OF THE DESIGN ENGINEER TO RESOLVE CONSTRUCTION PROBLEMS WITH THE TOWN OF ERIE DUE TO CHANGED CONDITIONS ENCOUNTERED BY THE CONTRACTOR DURING THE PRORESS OF ANY PORTION OF THE PROPOSED WORK. IF, IN THE OPINION OF THE TOWN OF ERIE PROPOSED ALTERATIONS TO THE SIGNED CONSTRUCTION PLANS INVOLVES SIGNIFICANT CHANGES TO THE CHARACTER OF THE WORK, OR TO THE FUTURE CONTIQUOUS PUBLIC OR PRIVATE IMPROVEMENTS, THE DESIGN ENGINEER SHALL BE RESPONSIBLE FOR SUBMITTING REVISED PLANS TO THE TOWN OF ERIE FOR REVEM, PRIOR TO ANY FUTURER CONSTRUCTION RELATED TO THAT PORTION OF THE WORK.

JURING THE COURSE OF CONSTRUCTION OF THE PROJECT. THE CONTRACTOR SHALL BE SOLELY AND COMPLETELY RESPONSIBLE FOR CONDITIONS AT AND ADJACENT TO THE JOB INCLUDING SAFETY OF ALL PERSONS AND PROPERTY DURING PERFORMANCE OF THE WORK. THE CONTRACTOR SHALL PROVIDE ALL LIGHTS, SIGNS, BARRICADES, FLAGMEN, OR OTHER DEVICES NECESSARY TO PROVIDE FOR PUBLIC SAFETY. THIS REQUIREMENT SHALL APPROVIDE ALL LIGHTS, SIGNS, BARRICADES, FLAGMEN, OR OTHER DEVICES NECESSARY TO PROVIDE FOR PUBLIC SAFETY. THIS REQUIREMENT SHALL APPLY CONTINUOUSLY AND IS NOT LIMITED TO NORMAL WORKING HOURS. THE TOWN OF ERIE OR THE ENGINEER EXERCISE NO CONTROLS OVER THE SAFETY OR ADEQUACY OF THE SAME. THE CONTRACTOR SHALL DEFEND, INDENNIFY AND HOLD HARNLESS FROM ANY AND ALL LIABULTY. GRIN THE PROVECT ON THE PROVICE, EXCEPTING FOR LIABURANCE OF WORK ON THIS PROVIDE. THE OFFICIENT WORK AND SALL LIABULTY. RELAND ALLEGED, IN CONNECTION WITH HE PERFORMANCE OF WORK ON THIS PROVICE, EXCEPTING FOR LIABURG FROM ANY AND ALL LIABULTY. RELAND ALLEGED, IN CONNECTION WITH HE PERFORMANCE OF WORK ON THIS PROVICE, EXCEPTING FOR LIABULTY ARISING FROM THE SOLE NEGURIESE OF THE ADD ALLEGED, IN CONNECTION WITH HE PERFORMANCE OF WORK ON THIS PROVICE, EXCEPTING FOR LIABULTY ARISING FROM THE SOLE NEGUREOR OF THE MOWER, THE DESION EDING FOR THE SOLE NEGURE OF THE POWER, THE DESION EDINEER OR THE TOWN. THE TOWN OF ERIE ENGINEERING FOR ALL ADDILIDABLE FOR SAFETY IN, ON OR ABOUT THE PROVERTIONS OF

WORK IN PUBLIC STREETS, ONCE BEGUN, SHALL BE PROSECUTED TO COMPLETION WITHOUT DELAY SO AS TO PROVIDE MINIMUM INCONVENIENCE TO ADJACENT PROPERTY OWNERS AND TO THE TRAVELING PUBLIC.

8. THE CONTRACTOR SHALL TAKE ALL NECESSARY AND PROPER PRECAUTIONS TO PROTECT ADJACENT PROPERTIES FROM ANY AND ALL DAMAGE THAT MAY OCCUF FROM STORM WATER RUNOFF AND/OR DEPOSITION OF DEBRIS RESULTING FROM ANY AND ALL WORK.
9. EACH TYPE OF CONSTRUCTION SHALL BE COMPLETED BY A CONTRACTOR THAT HAS DEMONSTRATED ACCEPTABLE QUALIFICATIONS TO THE TOWN AND IS A LICENSED CONTRACTOR IN THE TOWN OF ERE.

. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL TRAFFIC CONTROL DURING CONSTRUCTION. ALL TRAFFIC CONTROLS SHALL CONFORM TO THE MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES. (MUTCD) LATEST EDITION.

ALL BACKFILL SHALL CONFORM TO THE TRENCH DETAIL LOCATED IN THE TOWN OF ERIE STANDARDS & SPECIFICATIONS.

2. THE CONTRACTOR SHALL IMMEDIATELY REMOVE ANY CONSTRUCTION DEBRIS OR MUD TRACKED ONTO EXISTING ROADWAYS. THE CONTRACTOR SHALL REPAIR ANY EXCAVATION OR PAVEMENT FAILURES CAUSED BY HIS CONSTRUCTION.

5. THE CONTRACTOR SHALL RENEW OR REPLACE ANY EXISTING TRAFFIC STRIPING AND/OR PAVEMENT MARKINGS, WHICH HAVE BEEN EITHER REMOVED OR THE EFFECTIVENESS OF WHICH HAS BEEN REDUCED DURING HIS OPERATION. RENEWAL OF PAVEMENT STRIPING AND MARKING SHALL BE DONE IN CONFORMANCE WITH THE TOWN OF ERIE STRUADARD SPECIFICATIONS.

4. IT SHALL BE THE CONTRACTOR'S RESPONSIBILITY TO TAKE EVERY MEASURE NECESSARY TO COMPLY WITH ANY STATE, COUNTY OR TOWN DUST CONTROL ORDINANCE. CONSTRUCTION VEHICLES SHALL USE TRUCK ROUTES DESIGNATED BY THE TOWN.

5. THE CONTRACTOR WILL BE HELD RESPONSIBLE FOR THE PROPER FUNCTIONING OF THE IMPROVEMENTS FOR A MINIMUM OF TWO (2) YEARS FROM THE DATE OF SUBSTANTIAL COMPLETION/ CONSTRUCTION ACCEPTANCE OF THE IMPROVEMENTS BY THE TOWN OF ERIE. ANY FAILURE DURING THIS PERIOD OF GUARANTEE SHALL BE REMEDIED BY THE CONTRACTOR TO THE SATISFACTION OF THE TOWN OF ERIE AT NO EXPENSE TO THE TOWN.

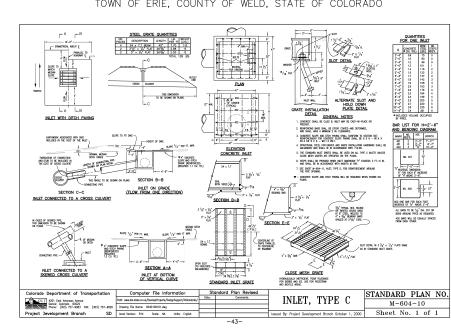
. THE DESIGN CIVIL ENGINEER SHALL PERFORM SUFFICIENT INSPECTIONS AND SURVEYS DURING GRADING AND CONSTRUCTION SO THAT HE MAY RENDER AN OPINION VERIFIED IN WRITING AS TO COMPLIANCE WITH THE PLANS AND CODES WITHIN HIS PURVIEW.

THE SOLS ENGINEER SHALL PERFORM SUFFICIENT INSPECTIONS DURING GRADING AND CONSTRUCTION SO THAT HE MAY RENDER AN OPINION VERIFIED IN WRITING AS TO COMPLIANCE WITH THE PLANS AND CODES WITHIN HIS PLRWEW

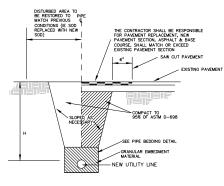




LOT 2 AND OUTLOT A, ERIE AIR PARK SUBDIVISION, REPLAT A, AND A PART OF TRACT D, ERIE AIR PARK SUBDIVISION. ALL LOCATED IN THE SW1/4 OF SEC. 31, T1N, R68W OF THE 6TH P.M. TOWN OF ERIE, COUNTY OF WELD, STATE OF COLORADO



TRENCH EXCAVATION STRAW BALE INSTALLATION -2"x2" STAKE ______50 LB. STRAW BAL - FLOW SECTION NOTE: EROSION CONTROL MEASURES SHALL BE MAINTAINED UNTIL LANDSCAPING IS COMPLETED. STRAW BALE EROSION BARRIER ERIE ER STM5 N BY: D. JENKINS PPROVED BY: G. BEHLEN DATE: 06/200



UTILITY TRENCH DETAIL N.T.S.



D.MAINTAIN INSPECTION AND MAINTENANCE RECORDS OF BMPS ONSITE WITH THE SWMP. E.BASED ON INSPECTIONS PERFORMED BY THE OWNER OR BY TOWN PERSONNEL, MODIFICATIONS TO THE SWMP WILL BE NECESSARY IF AT ANY TIME THE SPECIFIED BMPS DO NOT MEET THE OBJECTIVES OF THIS CHAPTER. IN THIS CASE, THE OWNER SHALL MEET WITH TOWN PERSONNEL TO DETERMINE THE APPRORPHATE MODIFICATIONS ALL MODIFICATIONS SHALL BE COMPLETED WITHIN SEVEN (7) DAYS OF THE REFERENCED INSPECTION, AND SHALL BE RECORDED ON THE OWNER'S COPY OF THE SWMP.

3. ALL SITE GRADING (EXCAVATION, EMBANKMENT, AND COMPACTION) SHALL CONFORM TO THE RECOMMENDATIONS OF THE LATEST SOILS INVESTIGATION FOR THIS PROPERTY AND SHALL FURTHER BE IN CONFORMANCE WITH THE TOWN OF ERIE "STANDARDS AND SPECIFICATIONS FOR THE DESIGN AND CONSTRUCTION OF PUBLIC IMPROVEMENTS", LATEST EDITION.

6. NATURAL VEGETATION SHALL BE RETAINED AND PROTECTED WHEREVER POSSIBLE. EXPOSURE OF SOIL TO EROSION BY REMOVAL OR DISTURBANCE OF VEGETATION SHALL BE LIMITED TO THE AREA REQUIRED FOR IMMEDIATE CONSTRUCTION OPERATION AND FOR THE SHORTEST PRACTICAL PERIOD OF TIME. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO AVDID ANY DAMAGE TO EXISTING FOLIAGE THAT LIES IN THE PROJECT AREA UNLESS DESIGNATED FOR REMOVAL AND SHALL BE LIABLE FOR SUCH DAMAGE AT HIS/HER EXPENSE.

11. THE OWNER/DEVELOPER SHALL PROVIDE ANY ADDITIONAL DUST ABATEMENT AND EROSION CONTROL MEASURES DEEMED NECESSARY BY SHOULD CONDITIONS MERIT THEM. 12. DURING CONSTRUCTION THE FILL AREAS WILL BE WETTED FOR COMPACTION AND THE HAUL ROUTES AND CUT AREAS WILL BE MAINTAINED WITH WATER TO REDUCE WIND FROSION

13. FILL SLOPES SHALL BE COMPACTED BY MEANS OF SHEEPSFOOT COMPACTOR OR OTHER SUITABLE EQUIPMENT. COMPACTING SHALL CONTINUE UNTIL SLOPES ARE STABLE AND THERE IS NOT AN APPRECIABLE AMOUNT OF LOOSE SOLL ON THE SLOPES.

14. TEMPORARY CUT/FILL SLOPES SHALL NOT BE STEEPER THAN 2:1 (2H:1V). PERMANENT SLOPES SHALL NOT BE STEEOER THAN 4:1 (4H:1V) IN AREAS TO BE SEFEDED OR SODDED.

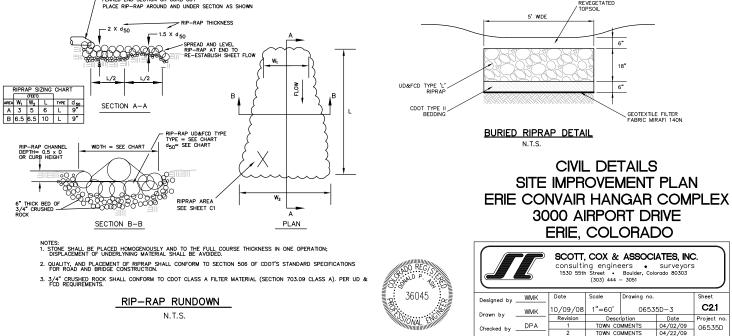
15. DEPTH OF MOISTURE-DENSITY CONTROL SHALL BE FULL DEPTH ON ALL EMBANKMENT AND SIX (6) INCHES ON THE BASE OF CUTS AND FILLS

16. OUTLET SIDES OF ALL PIPES SHALL BE GRADED TO DRAIN AND SHALL HAVE SUFFICIENT EROSION PROTECTION. 17. THE PERMITTEE OR HIS AGENT SHALL NOTIFY THE TOWN OF ERIE ENGINEERING STAFF WHEN THE GRADING OPERATION IS READY FOR EACH OF THE

E.DRAINAGE DEVICE INSPECTION AFTER FORMING OF TERRACE DRAINS, DOWNDRAINS, OR AFTER PLACEMENT OF PIPE BUT BEFORE ANY CONCRETE OR FILL MATERIAL IS PLACED. F.FINAL INSPECTION WHEN ALL WORK INCLUDING INSTALLATION OF ALL DRAINAGE STRUCTURES AND OTHER PROTECTIVE DEVICES HAS BEEN COMPLETED AND THE AS-GRADED PLAN, PROFESSIONAL VERIFICATIONS AND REQUIRED REPORTS HAVE BEEN SUBMITTED.

18. SOILS IN THE AREA OF THE PROPOSED STRUCTURE SHALL BE CUT TO THE PROPOSED GRADE, AND THE SURFACE SHALL BE SCARIFIED TO A MINIMUM DEPTH OF ONE (1) FOOT, MOISTURE CONDITIONED AND PROOF ROLLED TO A MINIMUM OF 95% RELATIVE COMPACTION, UNLESS OTHERWISE PROVIDED FOR IN THE SOLLS REPORT.

19. AREAS OF CONTINUOUS FOOTINGS SHALL BE UNDERCUT AND COMPACTED TO 95% RELATIVE COMPACTION AT A DEPTH EQUAL TO THE WIDTH OF THE FOOTING, UNLESS OTHERWISE PROVIDED FOR IN THE SOILS REPORT. REVEGETATED



DIAMETER CULVERT WITH

GENERAL NOTES - GRADING

1. NO GRADING SHALL COMMENCE WITHOUT OBTAINING A GRADING AND STORWWATER QUALITY PERMIT FROM THE TOWN OF ERLE. A PRE-GRADE MEETING AT THE SITE IS REQUIRED BEFORE THE START OF GRADING WITH THE FOLLOWING PEOPLE PRESENT: OWNER, GRADING CONTRACTOR, DESIGN CIVIL ENGINEER, SOLIS ENGNEER, TOWN OF ERLE ENGINEERING STAFF, AND UTILITY COMPANY REPRESENTATIVES. A TWENTY-FOUR (24) HOUR NOTCE IS REQUIRED.

2. ALL CONSTRUCTION ACTIVITIES THAT DISTURBS ONE OR MORE ACRES OF LAND, AS WELL AS ACTIVITIES THAT DISTURB LESS THAN ONE ACRE OF LAND, BUT IS PART OF A LARGER COMMON PLAN OF DEVELOPMENT, MUST COMPLY WITH BOTH LOCAL AND STATE REGULATIONS REGARDING STORMWATER DRAINAGE ON CONSTRUCTION SITES. OWNERS OR CONTRACTORS MUST OBTINN A COLORADO STORMWATER DISCHARGE PERMIT FOR CONSTRUCTION ACTIVITIES, FROM THE COLORADO DEPARTMENT OF PUBLIC HEALTH AND ENVIRONMENT (CDPHE).

A. MAINTAIN A COPY OF THE SWMP ONSITE AT ALL TIMES. THE APPROVED SWMP MUST BE MAINTAINED AND MADE AVAILABLE TO MUNICIPAL INSPECTORS UPON REQUEST.

B.INSTALL AND MAINTAIN EROSION, SEDIMENT, AND MATERIALS MANAGEMENT CONTROL BMPS AS SPECIFIED IN THE SWMP

CINSPECT ALL BMPS AT LEAST EVERY FOURTEEN (14) DAYS AND WITHIN TWENTY FOUR (24) HOURS AFTER ANY PRECIPITATION OR SNOWMELT EVENT THAT CAUSES SURFACE RUNOFF.

F.THE OPERATOR SHALL AMEND THE PLAN WHENEVER THERE IS A SIGNIFICANT CHANGE IN DESIGN, CONSTRUCTION, OPERATION, OR MAINTENANCE, WHICH HAS A SIGNIFICANT EFFECT ON THE POTENTIAL FOR DISCHARGE OF POLLUTANTS TO THE RECEIVING WATERS, OR IF THE SMMP PROVES TO BE INEFFECTIVE IN ACHIEVING THE GENERAL OBJECTIVES OF CONTROLLING POLLUTANTS IN STORM WATER DISCHARGES ASSOCIATED WITH CONSTRUCTION ACTIVITIES.

G. INSTALLATION AND MAINTENANCE OF BMPS SHALL BE SUPERVISED BY PERSONNEL CERTIFIED IN EROSION AND SEDIMENT CONTROL.

ALL GRADING AND FILLING OPERATIONS SHALL BE OBSERVED, INSPECTED AND TESTED BY A LICENSED SOILS ENGINEER, ALL TEST RESULT SHALL BE SUBMITTED TO THE TOWN OF ERIE ENGINEERING STAFF.

5. CONTOURS AND SPOT ELEVATIONS SHOWN ARE ONLY CONTROLS AND THE PROFILES THEY FORM SHALL BE SMOOTH AND CONTINUOUS

TOPSOIL SHALL BE STOCKPILED TO THE EXTENT PRACTICABLE ON THE SITE FOR USE ON AREAS TO BE REVEGATATED. ANY AND ALL STOCKPILES SHALL BE LOCATED AND PROTECTED FROM ERGSIVE ELEMENTS.

8. TEMPORARY VEGETATION SHALL BE INSTALLED ON ALL DISTURBED AREAS WHERE PERMANENT SURFACE IMPROVEMENTS ARE NOT SCHEDULED FOR IMMEDIATE INSTALLATION. SEEDING WILL BE DONE ACROSS THE SLOPE FOLLOWING THE CONTOURS. VEGETATION SHALL BE A VIGOROUS, DROUGHT TOLERANT NATIVE SPECIES MIX, PROJECT SCHEDULING SHOULD TAKE ADVANTAGE OF SPRING OR FALL PLANTING SEASONS FOR NATURAL GERMINATION. SEEDED AREAS SHALL BE IRRIGATED IF CONDITIONS SO MERIT.

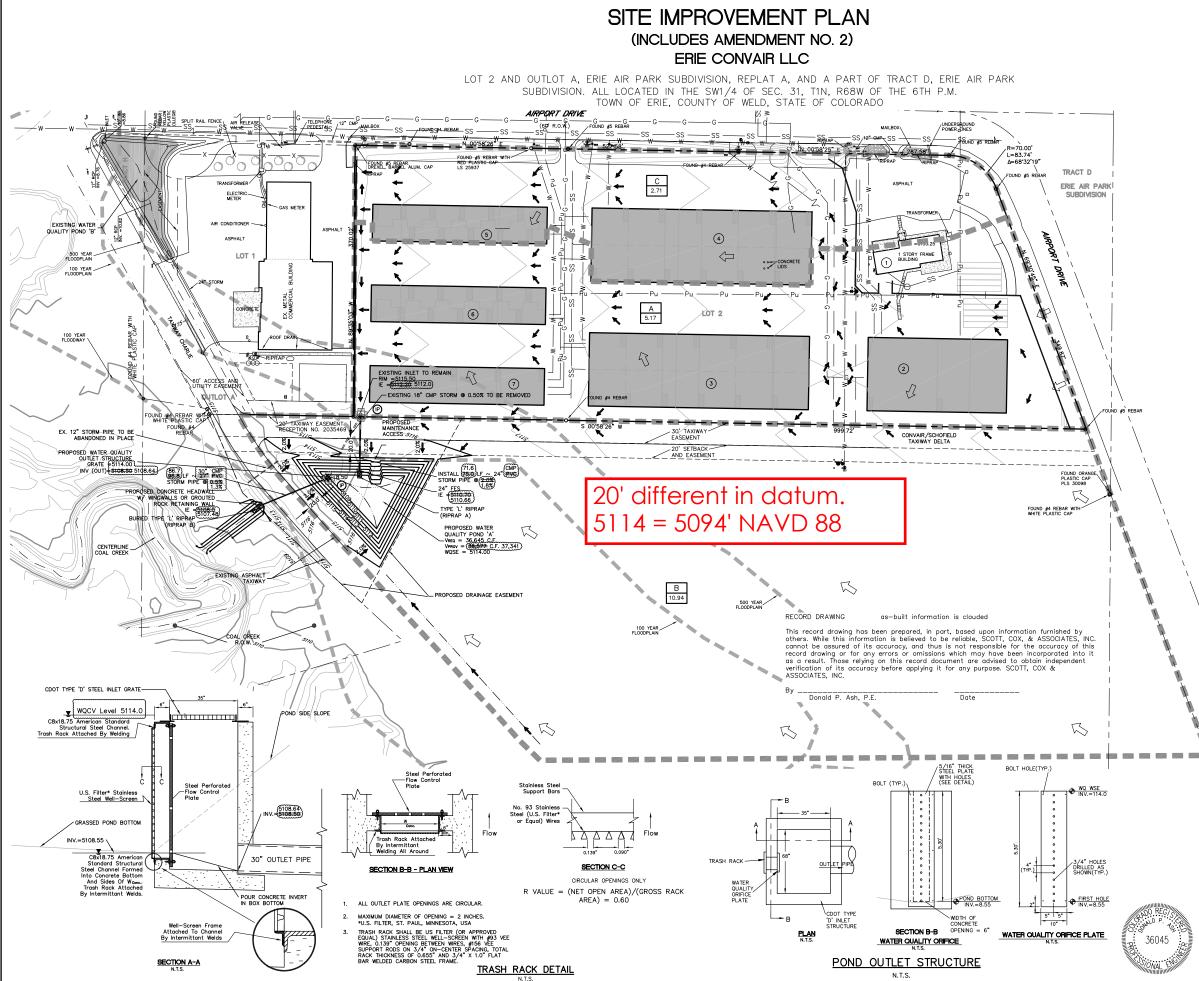
9. AT ALL TIMES, THE PROPERTY SHALL BE MAINTAINED AND/OR WATERED TO PREVENT WIND-CAUSED EROSION. EARTHWORK OPERATIONS SHALL BE DISCONTINUED WHEN FUGITIVE DUST SIGNIFICANTLY IMPACTS ADJACENT PROPERTY. IF EARTHWORK IS COMPLETE OR DISCONTINUED AND DUST FROM THE SITE CONTINUES TO CREATE PROBLEMS, THE OWNER/DEVELOPER SHALL IMMEDIATELY INSTITUTE MITIGATIVE MEASURES AND SHALL CORRECT DAMAGE TO ADJACENT PROPERTY.

10. TEMPORARY SILT FENCES SHALL BE INSTALLED ALONG ALL BOUNDARIES OF THE CONSTRUCTION LIMITS AS SHOWN ON THE APPROVED EROSION CONTROL PLAN. IN ADDITION, THE TOWN OF ERIE MAY REQUIRE AN ADDITIONAL TEMPORARY SILT FENCE IF FIELD CONDITIONS SO MERIT THEM.

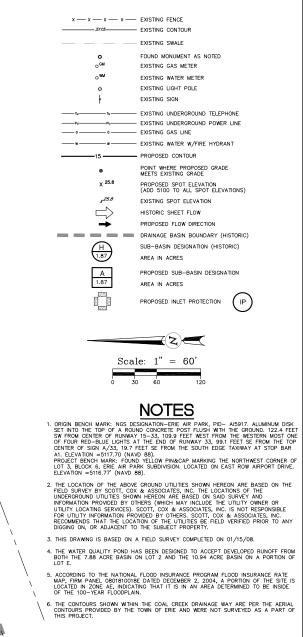
A. INITIAL INSPECTION WHEN THE PERMITTEE IS READY TO BEGIN WORK, BUT NOT LESS THAN TWO (2) DAYS BEFORE ANY GRADING OR GRUBBING IS STARTED.

B.TOWN OF ERIE INSPECTION AFTER THE NATURAL GROUND OR BEDROCK IS EXPOSED AND PREPARED TO RECEIVE FILL, BUT BEFORE FILL IS PLACED. C.EXCAVATION INSPECTION AFTER THE EXCAVATION IS STARTED BUT BEFORE THE VERTICAL DEPTH OF THE EXCAVATION EXCEEDS TEN (10) FEET.

D.FILL INSPECTION AFTER THE FILL PLACEMENT IS STARTED, BUT BEFORE THE FILL EXCEEDS TEN (10) FEET.







BASIN SUMMARY

BASIN	Q2 (CFS)	Q5 (CFS)	Q10 (CFS)	OUTFALL
А	5.17	14.17	27.15	PROPOSED
В	10.97	30.93	59.39	POND 'A'
С	2.71	6.60	12.90	EX. POND 'B'

AS-BUILT POND GRADING, DRAINAGE, AND **EROSION CONTROL PLAN** SITE IMPROVEMENT PLAN ERIE CONVAIR HANGAR COMPLEX 3000 AIRPORT DRIVE ERIE, COLORADO

SCOTT, COX & ASSOCIATES, INC. consulting engineers • Surveyors 1530 55th Street • Boulder, Colorado 80303 (303) 444 - 3051							
Designed by	WMK	Date	Scale	Drawing no.		Sheet	
	WMK	10/09/08	1"=60'	0653	5D-3	C1.1	
Drawn by _		Revision	Description Date		Date	Project no.	
Checked by _	DPA	1	TOWN CO	MMENTS	04/02/09	06535D	
onecked by		2	TOWN COMMENTS 04/22/09		04/22/09	000000	
		3	POND AS	-BUILT	05/19/09		



United States Department of Agriculture

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Weld County, Colorado, Southern Part

Lot 2 Erie Air Park Tract E Minor Subdivision Replat A



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

The U.S. Department of Agriculture (USDA) prohibits discrimination in all its programs and activities on the basis of race, color, national origin, age, disability, and where applicable, sex, marital status, familial status, parental status, religion, sexual orientation, genetic information, political beliefs, reprisal, or because all or a part of an individual's income is derived from any public assistance program. (Not all prohibited bases apply to all programs.) Persons with disabilities who require

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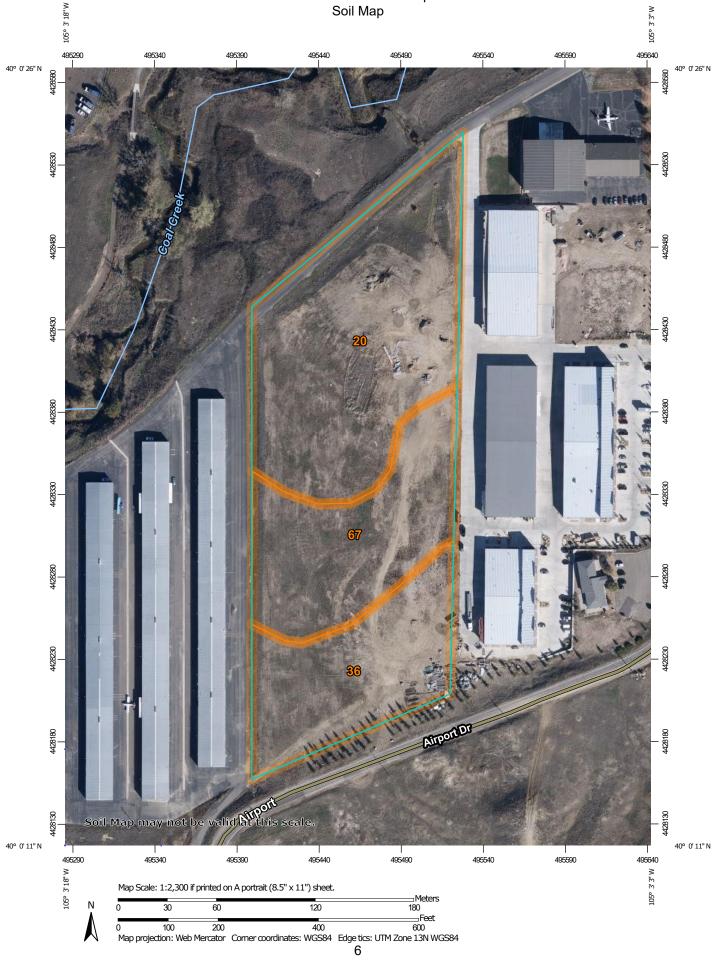
Contents

Preface	2
Soil Map	
Soil Map	
Legend	7
Map Unit Legend	
Map Unit Descriptions	
Weld County, Colorado, Southern Part	
20—Colombo clay loam, 1 to 3 percent slopes	
36—Midway-Shingle complex, 5 to 20 percent slopes	11
67—Ulm clay loam, 3 to 5 percent slopes	13
References	15

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

Custom Soil Resource Report Soil Map



	MAP L	EGEND		MAP INFORMATION		
Area of Int	terest (AOI) Area of Interest (AOI)	8	Spoil Area Stony Spot	The soil surveys that comprise your AOI were mapped at 1:24,000.		
Soils	Soil Map Unit Polygons Soil Map Unit Lines Soil Map Unit Points	00 ☆ ∽	Very Stony Spot Wet Spot Other Special Line Features	Warning: Soil Map may not be valid at this scale. Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of		
() ()	Borrow Pit		tures Streams and Canals ation	contrasting soils that could have been shown at a more detailed scale. Please rely on the bar scale on each map sheet for map		
× ×	Clay Spot Closed Depression Gravel Pit Gravelly Spot	∷	Rails Interstate Highways US Routes Major Roads	measurements. Source of Map: Natural Resources Conservation Service Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857)		
0 A 4	Landfill Lava Flow Marsh or swamp	Backgrou	Local Roads	Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more		
* 0 0	Mine or Quarry Miscellaneous Water Perennial Water			accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.		
* + ::	Rock Outcrop Saline Spot Sandy Spot			Soil Survey Area: Weld County, Colorado, Southern Part Survey Area Data: Version 17, Sep 10, 2018 Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.		
♦ ◇ ◇	Severely Eroded Spot Sinkhole Slide or Slip			Date(s) aerial images were photographed: Oct 1, 2018—Oct 31, 2018		
ø	Sodic Spot			The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.		

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
20	Colombo clay loam, 1 to 3 percent slopes	4.7	48.4%
36	Midway-Shingle complex, 5 to 20 percent slopes	2.3	24.3%
67	Ulm clay loam, 3 to 5 percent slopes	2.6	27.3%
Totals for Area of Interest	·	9.6	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or

landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Weld County, Colorado, Southern Part

20—Colombo clay loam, 1 to 3 percent slopes

Map Unit Setting

National map unit symbol: 361x Elevation: 4,600 to 4,780 feet Mean annual precipitation: 12 to 16 inches Mean annual air temperature: 48 to 52 degrees F Frost-free period: 130 to 160 days Farmland classification: Prime farmland if irrigated

Map Unit Composition

Colombo and similar soils: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Colombo

Setting

Landform: Terraces, flood plains Down-slope shape: Linear Across-slope shape: Linear Parent material: Stratified, calcareous alluvium

Typical profile

H1 - 0 to 14 inches: clay loam
H2 - 14 to 21 inches: stratified loam to clay loam
H3 - 21 to 60 inches: stratified sand to loam to clay loam

Properties and qualities

Slope: 1 to 3 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20 to 0.60 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 10 percent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water storage in profile: High (about 9.4 inches)

Interpretive groups

Land capability classification (irrigated): 2e Land capability classification (nonirrigated): 3e Hydrologic Soil Group: C Ecological site: Clayey Plains (R067BY042CO) Hydric soil rating: No

Minor Components

Dacono

Percent of map unit: 5 percent

Hydric soil rating: No

Heldt

Percent of map unit: 5 percent Hydric soil rating: No

Nunn

Percent of map unit: 5 percent Hydric soil rating: No

36—Midway-Shingle complex, 5 to 20 percent slopes

Map Unit Setting

National map unit symbol: 362g Elevation: 5,050 to 5,250 feet Mean annual precipitation: 10 to 17 inches Mean annual air temperature: 46 to 52 degrees F Frost-free period: 100 to 180 days Farmland classification: Not prime farmland

Map Unit Composition

Midway and similar soils: 50 percent Shingle and similar soils: 35 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Midway

Setting

Landform: Ridges, hills Down-slope shape: Linear Across-slope shape: Linear Parent material: Calcareous residuum weathered from shale

Typical profile

H1 - 0 to 7 inches: clay H2 - 7 to 13 inches: clay H3 - 13 to 17 inches: weathered bedrock

Properties and qualities

Slope: 5 to 20 percent
Depth to restrictive feature: 6 to 20 inches to paralithic bedrock
Natural drainage class: Well drained
Runoff class: Medium
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 15 percent
Gypsum, maximum in profile: 15 percent

Salinity, maximum in profile: Very slightly saline to moderately saline (2.0 to 8.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 15.0
Available water storage in profile: Very low (about 2.0 inches)

Interpretive groups

Land capability classification (irrigated): 6e Land capability classification (nonirrigated): 6e Hydrologic Soil Group: D Ecological site: Shaly Plains (R067BY045CO) Hydric soil rating: No

Description of Shingle

Setting

Landform: Hills, ridges Down-slope shape: Linear Across-slope shape: Linear Parent material: Residuum weathered from calcareous shale

Typical profile

H1 - 0 to 6 inches: loam H2 - 6 to 18 inches: clay loam H3 - 18 to 22 inches: unweathered bedrock

Properties and qualities

Slope: 5 to 20 percent
Depth to restrictive feature: 10 to 20 inches to paralithic bedrock
Natural drainage class: Well drained
Runoff class: Medium
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 15 percent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water storage in profile: 1 ow (about 3.3 inches)

Available water storage in profile: Low (about 3.3 inches)

Interpretive groups

Land capability classification (irrigated): 6s Land capability classification (nonirrigated): 6s Hydrologic Soil Group: D Ecological site: Shaly Plains (R067BY045CO) Hydric soil rating: No

Minor Components

Renohill

Percent of map unit: 8 percent *Hydric soil rating:* No

Tassel

Percent of map unit: 7 percent Hydric soil rating: No

67—Ulm clay loam, 3 to 5 percent slopes

Map Unit Setting

National map unit symbol: 363k Elevation: 5,070 to 5,200 feet Mean annual precipitation: 13 to 15 inches Mean annual air temperature: 46 to 48 degrees F Frost-free period: 105 to 120 days Farmland classification: Farmland of statewide importance

Map Unit Composition

Ulm and similar soils: 85 percent *Minor components:* 15 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Ulm

Setting

Landform: Plains Down-slope shape: Linear Across-slope shape: Linear Parent material: Alluvium and/or eolian deposits derived from shale

Typical profile

H1 - 0 to 5 inches: clay loam *H2 - 5 to 17 inches:* clay *H3 - 17 to 60 inches:* clay loam

Properties and qualities

Slope: 3 to 5 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 15 percent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water storage in profile: High (about 10.5 inches)

Interpretive groups

Land capability classification (irrigated): 4e Land capability classification (nonirrigated): 4e Hydrologic Soil Group: C Ecological site: Clayey Plains (R067BY042CO) Hydric soil rating: No

Minor Components

Renohill

Percent of map unit: 11 percent *Hydric soil rating:* No

Heldt

Percent of map unit: 4 percent Hydric soil rating: No

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